## A critical review of power generation using geothermal-driven organic Rankine cycle

# Reyhaneh Loni<sup>a,\*</sup>, Omid Mahian<sup>b</sup>, Gholamhassan Najafi<sup>a</sup>, Ahmet Z. Sahin<sup>c,\*</sup>, Fatemeh Rajaee<sup>d</sup>, Alibakhsh Kasaeian<sup>d</sup>, Mehdi Mehrpoya<sup>d</sup>, Evangelos Bellos<sup>e</sup>, Willem G. le Roux<sup>f</sup>

<sup>a</sup> Department of Biosystem Engineering, Tarbiat Modares University, Tehran, Iran.

<sup>b</sup> School of Chemical Engineering and Technology, Xiá n Jiaotong University, Xiá n, China

<sup>c</sup> Mechanical Engineering Department, King Fahd University of Petroleum & Minerals, Dhahran, Saudi Arabia

<sup>d</sup> Department of Renewable Energies, Faculty of New Sciences and Technologies, University of Tehran, Tehran, Iran

<sup>e</sup> Thermal Department, School of Mechanical Engineering, National Technical University of Athens, Athens, Greece

<sup>f</sup> Department of Mechanical and Aeronautical Engineering, University of Pretoria, South Africa

\*Corresponding authors: loni@modares.ac.ir, azsahin@kfupm.edu.sa, Tel.: +966 13 860 2548

#### Highlights

•The geothermal-driven ORC systems for power generation are reviewed.

•Both experimental and numerical investigations are included.

•The geothermal-driven ORC systems are viable investments.

•A 20% to 30% increase in the performance of geothermal-fed ORC systems is possible.

•The polygeneration systems that include geothermal-driven ORCs are promising units.

#### Abstract

Organic Rankine Cycle (ORC) is a promising electricity production technology that exploits low and medium heat sources. Usually, renewable and alternative heat sources can be used in order to feed an ORC with heat. The exploitation of geothermal energy is a usual and sustainable way to feed an ORC because it is a sustainable, abundant, economical and environmentally-friendly choice. The main objective of this study is to review and to discuss the geothermal-driven ORC systems for power generation in a detailed way. Both experimental and numerical investigations are included in the present work. It is found that the geothermal-driven ORC systems are viable investments with relatively low payback periods, as well as these systems lead to high energy efficiency. Moreover, it is concluded that a 20% to 30% increase in the performance of geothermal-fed ORC systems is possible by optimization. Lastly, it is useful to state that the polygeneration systems that include geothermal-driven ORCs are promising units that present high exergy efficiency values.

## Keywords

Renewable energy, Organic Rankine cycle, Power generation, Geothermal ORC, Geothermal energy

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## 1 Introduction

## 1.1 Geothermal energy

The use of fossil fuels for producing electricity has very important drawbacks such as high levels of greenhouse gas emissions, acid rain, global warming, and depletion of the ozone layer [1]. Renewable resources can be regarded as reliable and clean energy resources for meeting the required electricity and heat duties [2]. Geothermal energy is a clean energy source that can be converted into heating of various temperature levels and so it is able to produce many useful outputs like electricity [3].

Geothermal plants are found in tectonically active locations such as Iceland, Italy, Turkey and New Zealand. The organic Rankine cycle market has experienced substantial growth since the early 2000s (Tartière and Astolfi [4]). In the world, geothermal installed capacity has increased from approximately 9992 MW in 2010 to around 13,931 MW in 2019 (Haghighi et al. [5]). Hydrothermal plants provide the heat stored in natural aquifers with high values of enthalpy to generate electrical power by dry steam, single flash and double flash cycles [6, 7]. Deep and improved geothermal plants are of the more recent technologies that aim at heat stored in reserves deeper than natural aquifers [8]. A hydrothermal reservoir can be formed by trapping steam in permeable and porous rocks under an impermeable layer.

In order to produce electrical power from the geothermal (or hydrothermal) resources, wells are drilled into a geothermal reservoir and geothermal fluid is brought to the surface. By employing a geothermal power plant, the heat is converted into power through turbines. There are four kinds of geothermal power plants are employed for power generation [9]:

(a) Dry steam systems: In dry steam systems, the temperature of the reservoir is about 370°C, and high-pressure steam is produced. Dry steam (or supercritical) systems supply the highest amount of energy per fluid mass. In this case, steam is generated directly from the geothermal reservoir. Because the wells generate only steam to run the turbines, no separation system is needed.

(b) Single-double or triple flash systems: In flash systems, the liquid flashes while still in the well. The steam enters the turbine and then the liquid is sent back to the reservoir. A double-flash steam plant is a modified version of the single-flash configuration, which can generate 15-20% more electricity for the same conditions. The capital, operating and maintenance costs of a double-flash system are more than single-flash systems, but the extra electricity produced often justifies the installation of these systems.

(c) Binary-cycle systems: When low-grade geothermal energy is available, binary-cycle (indirect) systems are used. Generally, isobutane and pentafluoropropane are utilized as working fluids in these systems. The Kalina and organic Rankine cycles are commonly employed in binary systems. The thermal efficiency of binary systems is in the 10-13% range.

(d) Flash/binary combined systems: In flash/binary combined configurations, a hybrid form of binary and flash systems are employed. Figure 1 illustrates the different configurations of geothermal power units [10].



Figure 1: Diagram of different geothermal power plants including: a) a dry steam plant b) a single-flash plant c) a basic binary geothermal power plant d) a hybrid steam-binary geothermal power plant [10].

#### **1.2** The organic Rankine cycle

The organic Rankine cycle (ORC) is a power cycle that is ideal for low or medium temperature heat sources. It is a usual technology for applications of lower capacity and thus it is commonly selected for applications with geothermal energy, solar energy, or waste heat recovery. ORC utilizes organic fluids as working fluids and thus it is able to choose the suitable working fluid which is suitable for every energy source. Practically, there is a need for achieving compatibility between the heat source temperature level and the saturation curve shape of the selected working medium. The critical temperature of the organic fluid is an important parameter and it has to be close to the temperature level of the heat source. In many cases, the regenerative ORC is used in order to utilize the waste heat at the exit of the turbine and to enhance the thermodynamic efficiency of the system.

The basic non-regenerative ORC is illustrated in Figure 2. The system shown includes the heat recovery system (HRS) for inserting heat in the cycle, the expansion device (turbine) for work production, the condenser for rejecting heat to the ambient and the organic fluid pump. The minimum temperature approach between the geothermal source and the organic medium, the pinch point, is usually chosen to be between 5°C and 20°C [11, 12].



Figure 2: The basic organic Rankine cycle.

Working fluid selection is important in designing the geothermal-driven ORC systems for high efficiency [13, 14]. For a series circuit ORC system, organic working fluids with high critical temperatures like iso-pentane result in high efficiency, while for parallel circuits, fluids with low critical temperatures like R227ea are superior [15]. The traditional classification of the organic working fluids is according to the slope of the saturation vapor curve and so the fluids are separated into wet, dry and isentropic [16]. According to the Reference [16], the most suitable working fluids are the following:

#### Subcritical working fluids: R236ea, R600a, R600 and R245fa.

#### Superheated working fluids: R142b, R152a, R236ea, R600 and R600a.

#### Supercritical working fluids: R134a, R600a, R32 and R22.

On the other hand, a novel classification has also been suggested on the basis of the primary and secondary characteristic points on the same diagram. As many as 57 types of organic working fluids have been reported in [17]. Molecular degrees of freedom and the isochoric heat capacity has been used to pick out between the wet and dry type of organic working medium. It is shown that when the degree of freedom of molecules increases, the transition occurs from wet to dry type of organic fluid. [18] Zeotropic fluid mixtures are also widely used as working fluids in power generation systems. [19] Selecting an ORC working fluid is done by considering the system performance, chemical/physical properties of the fluid, like toxicity, flammability and environmental indexes like ozone depletion and global warming potentials. [20, 21] Some of the hydrofluoroolefins such as R1234yf, R1225yeE and R245fa showed potential for low-temperature geothermal power applications as ORC fluids at geothermal heat source temperatures in the range 120°C to 180°C. [22]

#### 1.3 Objectives of the present study

The current paper presents a detailed review in relation to the geothermal-fed ORC for electricity production. The review started by considering the performance analyses of geothermal-driven ORC systems. Both subcritical and supercritical ORC units are reviewed. Coupling the ORC systems with Kalina cycle, absorption cycle and coal-fired gasification combined cycle are discussed. Both the energy and exergy analyses with different working fluids are reviewed. Also, experimental and numerical studies are considered in this review paper. Additionally, this review paper includes the techno-economic analyses of the geothermal-driven ORC systems. In this regard, the application of vapor absorption chiller, thermal energy storage and integration with natural gas expansion plant are discussed. In addition, optimization techniques of the ORC cycles are presented that included subcritical and supercritical ORC systems with and without regeneration and various types of working fluids using both the energy and exergy aspects. Furthermore, solar-geothermal hybrid ORC systems were considered. Various approaches for the optimization of such hybrid systems that included artificial intelligence are considered from the energy, exergy and power generation perspective. Moreover, it has to be said that studies about cogeneration, trigeneration and polygeneration systems that include ORC and geothermal energy are included in this review paper. The reviewed works are examined and discussed properly in order to determine the most effective choices. Tables are used in order to summarize the basic conclusions of all the studies. In the last part of this work, the most important conclusion is highlighted, the future steps in the field and given, as well as the challenges of the examined technology, are presented.

The novelty of this study is based on the detailed examination of the geothermal-driven ORC including different aspects such as experimental studies, numerical studies, energy, exergy and economical approaches. Moreover, the special novelty is the emphasis that is given in the use of geothermal ORC systems inside cogeneration, trigeneration and polygeneration units. This fact makes this review to be a novel one and to be different compared to the other published reviews in the existing literature.

## 2 Thermodynamic investigation of the geothermal-driven ORC systems

The performance analysis of geothermal-driven ORC systems has been considered by many researchers. The energy analysis and the performance investigation are essential for the proper evaluation of ORC systems. Various design and operational aspects of ORC systems together with different options of coupling them with other cycles have been considered to improve the efficiency of the geothermal-driven ORC units [23]. In this regard, Paloso and Mohanty [24] suggested the idea of coupling an absorption cycle to a geothermal-driven ORC system. They numerically investigated the application of an absorption heat-transformer (AHT) and a vaporabsorption chiller (VAC) to increase the temperature of the fluid fed to the ORC evaporator. The performance of three power generation cycles was compared including conventional ORC, AHT-ORC and VAC-ORC systems. They found the VAC-ORC system resulted in having the highest performance. Guzović et al. [25] investigated the potential of a geothermal-driven system such as an ORC or a Kalina cycle (KC) for power production in the Republic of Croatia. They assessed the suggested systems based on thermodynamic laws. They found that the ORC systems can be recommended because of high efficiencies. More specifically, the thermal performance of the ORC is 14.1% compared to 10.6% with Kalina cycle, while the exergetic performance of the ORC is 52% compared to 44% with the Kalina cycle. Vetter et al. [11] compared the performance of a geothermal-driven ORC in subcritical and supercritical conditions for electricity generation. Ten different refrigerants were considered in the organic Rankine cycle and it is concluded that propane or R143a can be suggested as an appropriate ORC working fluid at a geothermal temperature level of 150°C. Sauret et al. [26] examined the performance of radial-inflow turbines in a geothermal-driven ORC system. Various ORC working fluids were evaluated including R134a, R143a, R236fa, R245fa and n-Pentane. They reported that the application of R134a and n-pentane resulted in the highest, and lowest performance of the system for power generation, respectively. Franco [27] investigated a geothermal-driven ORC unit for power production based on energy and exergy aspects. A regenerative ORC was investigated with water as the working medium between 100°C and 130°C. The performance of different organic Rankine cycle schemes was evaluated by testing different organic fluids including n-pentane, R134a, isobutane and R245fa. It was found that the regenerative configuration of the ORC decreased the brine-specific consumption of the unit. A typical geothermal-driven ORC system where CO<sub>2</sub> at supercritical conditions was used as the heat transfer MEDIUM of the geothermal energy is depicted in Figure 3 [16].



Figure 3: Depiction of the investigated power system with geothermal reservoir [16].

A performance comparison for the geothermal-driven ORC and KC was done by Guzović et al. [28] based on the energy efficiency analysis. This study was conducted for a medium temperature geothermal source in Lunjkovec-Kutnjak at 140°C, as a case study in the Republic of Croatia. The ORC system showed higher thermal efficiency of 13.5% compared to the KC with a thermal efficiency of 12.8%. Gabbrielli et al. [29] conducted an investigation of the determination of the optimum operating conditions in the off-design operation for a geothermal-driven ORC by trying to maximize the cash flow. They found that the application of geothermal energy with the lowest temperature resulted in the best performance for a power generation unit. Li et al. [30] suggested an ORC combined with geothermal energy, gathering heat tracing and oil recovery systems. The depiction of the examined combined system is illustrated in Figure 4. The suggested unit was combined with three subsystems. Different working fluids were studied for the ORC such as R245fa, R601a, R601, R141b, R123 and R600. It was calculated that the net power production was enhanced by 40% with the application of the optimized plant and R601a in the ORC.



Figure 4: Depiction of the electricity production unit with three subsystems and geothermal energy [30].

Zhang and Jiang [31] thermodynamically investigated a geothermal-drive ORC system for power generation using different geothermal working fluid temperatures which are illustrated in figure 5. The impact of different ORC fluids was considered including isopentane, R134a, isobutane and R245fa. Also, three different types of power generation cycles were studied including subcritical, superheated and transcritical. It was reported that the transcritical cycle was determined as the best choice for reaching the highest performance. Fu et al. [32] compared the use of an organic Rankine cycle and a Kalina cycle coupled with a geothermal power unit in an oilfield and they studied different working fluids. The studied system is illustrated in Figure 6 and the results showed that the application of R236fa leads in the highest performance of the ORC unit. Moreover, they clearly reported that the KC performed better than the ORC.



Figure 5: Depiction of the investigated power generation system with a non-regenerative ORC [31].



Figure 6: Depiction of a system with ORC and oil production subsystem [32].

The performance of a geothermal-driven ORC unit using CO<sub>2</sub> as the HTF of the geothermal system was studied by Mohan et al. [33]. Figure 7 depicts the examined system of this work with details. Four working fluids were investigated in the ORC including R134A, ammonia, n-Butane and neopentane. Among the investigated working fluids, ammonia showed the maximum power production of 49 MW<sub>el</sub> with an efficiency of 23%. AlZaharani et al. [34] studied the energy and exergy performance of a Rankine cycle with CO<sub>2</sub> and R600. The system was assumed as a multi-generation system for electricity, heat and hydrogen production. The suggested systems were driven using geothermal energy as a medium-high temperature heat source and Figure 8 shows the investigated system. The energetic efficiency and exergetic efficiency of the overall unit were reported at 13.67% and 32.27% respectively.



Figure 7: A schematic view of an indirect geothermal power system [33].



Figure 8: A schematic view of a double stage power generation system [34].

Configurations of the geothermal-driven ORC system for combined heating and power (CHP) were investigated by Habka and Ajib [35] based on energetic and exergetic aspects. The CHP system was investigated in parallel connection, series connection, and connection according to the Glewe-plant integration. R134a was applied as the ORC working medium. Their comparison concluded that the parallel connection is the best choice financially, while the optimum energy choice is the series connection. Li et al. [36] compared the performance of series and parallel circuits for heating, electricity and oil recovery for geothermal-driven ORC units. The studied series and parallel circuits of the investigated configuration are presented in Figure 9. It was found that the series circuit is appropriate for high geothermal water inlet temperatures and low heat source inlet temperatures of the oil gathering and transportation heat tracing (OGTHT), while the parallel circuit is appropriate for low geothermal inlet temperatures and high heat source inlet temperatures of the OGTHT. Habka and Ajib [37] investigated a geothermal-driven ORC system based on power generation, heating, and cooling. R134a was selected as the ORC medium. According to the results, the power of the system reduced when there was an increase in the return temperature or in the heating demand. Also, they found improved energy and exergy efficiency of the unit when reducing the return temperature. Hsieh et al. [38] investigated the performance of a geothermal-driven ORC using a co-axial multi-tube heat exchanger. R-245fa was used as the organic fluid.



Figure 9: A diagram view of the investigated systems by Ref. [36].

Fiaschi et al. [39] suggested a new geothermal-driven ORC unit for the production of electricity and heat. The cross parallel CHP system was proposed for the production of higher temperature heat for industrial applications. A depiction of the studied system is exhibited in Figure 10. The system was developed for reducing the exergetic destruction in the heat exchanging surfaces and heat loss due to re-injection, to increase the energetic and exergetic efficiencies of the system. They found a 55% improvement in power generation of the suggested system compared to a conventional one. Habka and Ajib [40] evaluated a geothermal-driven ORC using zeotropic mixtures as the working mediums. The unit was investigated based on parallel and series configurations for single power generation or CHP generation. Finally, it was concluded that the working fluids R22M, R422A and R438A were more efficient choices than the pure-fluids for the single electricity generation system.



Figure 10: A schematic view of the investigated system by Ref. [39] with details about the heat transfer devices.

A geothermal-driven ORC system for power generation coupled with an integrated coal-fired gasification combined cycle (IGCC) for providing the required CO<sub>2</sub> as geothermal heat transfer fluid was studied by Mohan et al. [41]. They reported that the combination of a high-pressure turbine and an ORC was advantageous for power generation from the suggested system. Also, it was found that isobutene and isopentane were the ORC working fluids that generated the highest and lowest net EGS power over a period of 25 years. Malik et al. [42] energetically and exergetically investigated a geothermal/biomass-driven ORC system for electricity, cool production, heat production, gas liquefaction and air drying which is given in Figure 11. They reported that the energy efficiency and the exergy efficiency of the unit were 56.5% and 20.3% respectively. Proctor et al. [43] dynamically simulated a geothermal-driven ORC for electricity production which is given in Figure 12 and they validated their model with existing experimental data.



Figure 11: A schematic view of a polygeneration system that uses geothermal energy for feeding two power cycles [42].



Figure 12: A schematic of a regenerative ORC that exploits geothermal energy [43].

Performance optimization for the subcritical and supercritical ORC systems with single-stage axial flow turbines was done by Manente et al. [44]. The ORC unit was coupled with geothermal energy with a geothermal working fluid of 150°C. They reported that the application of R1234yf, R134a, and R1234ze(E) was recommended as the optimum working fluids in the supercritical ORC system with the exergy efficiency in the range of 45.4% to 46.5%. Zare et al. [45] thermodynamically investigated geothermal-driven KC and ORC systems as multi-generation systems. The systems' performance was optimized according to the exergy efficiency criterion. A depiction of the investigated ORC unit is depicted in Figure 13. According to the results, it is found that the KC system resulted in higher exergy efficiency compared to other investigated systems. It was found that the KC system with a heat source temperature at 120°C, can generate 12.2% more electricity than the ORC system. An et al. [46] reviewed the application of geothermal energy for space heating and domestic hot water in Tianjin, China. Also, they presented a study for power generation with a geothermal-driven ORC system based on existing geothermal energy in Tianjin, China.

The performance of a two-stage serial ORC (TSORC) coupled with geothermal energy and absorption refrigeration (AR) is shown in Figure 14 [47]. The integrated TSORC-AR system increases the net power compared to the TSORC system while decreasing the thermal efficiency of the generated power. Yuksel and Ozturk [48] suggested geothermal energy-driven multi-generation system for electricity production using an ORC, domestic hot water, cooling using a quadruple effect absorption cooling system, and hydrogen using proton exchange-membrane electrolysis. They investigated the system based on energy and exergy analyses and reported energy and exergy efficiencies as 47% and 32.2% respectively. They found increasing power generation from 4 MW to 8.5 MW, and increasing hydrogen production from 0.030 kg s<sup>-1</sup> to 0.075 kg s<sup>-1</sup> with the increase of geothermal fluid temperature from 130°C to 200°C.



Figure 13: A schematic view of a system with ORC and absorption chiller which is fed by a geothermal heat source [45].



Figure 14: Diagram of the studied power generation system by Ref. [47].

Erdeweghe et al. [49] compared the exergy performance of the parallel and series configurations of a CHP plant coupled to 3<sup>rd</sup> and 4<sup>th</sup> generation thermal networks and Figure 15 shows the examined configurations. The investigated systems were driven by geothermal energy and an ORC system was used for generating power. They found that the parallel and series configurations can be recommended for the high and low-temperature thermal networks, respectively. Exergy efficiency of the parallel configuration with a nominal heat demand of 6 MW was calculated as 41.25%. Sadaghiani et al. [50] suggested a combined electricity

production plant including KC and ORC systems. Geothermal energy and liquid natural gas streams were used for converting heat to useful power. A block flow chart of the proposed power generation unit is presented in Figure 16. The combined system was investigated based on energy and exergy aspects. The highest exergy efficiency of the system and the net power output of each unit were found at 32.15 kW and 2485 kW respectively. Li et al. [51] investigated a geothermal energy-based multi-generation system as shown in Figure 17. The suggested system was including ORC units for electricity production. The impact of heat source and evaporator temperatures on the performance of the system was evaluated. The total energetic efficiency was reported as 75%.



Figure 15: Depiction of the investigated series and parallel CHP cases by Ref. [49].



Figure 16: Block-flow diagram of the power generation system by Ref. [50] which includes ORCs, Kalina cycle, geothermal reservoir and liquid natural gas.



Figure 17: A schematic view of the trigeneration system of Ref. [51].

The use of abandoned oil and gas wells with high temperatures as geothermal energy that can be used for electricity production was discussed by Nian and Cheng [52]. They presented different methods for utilizing geothermal energy for power generation including coupling with ORC systems. Also, a review was conducted on different methods for simulation of the heat transfer models of abandoned oil and gas wells geothermal systems. Akrami et al. [53] investigated a polygeneration unit based on a geothermal-driven ORC for power, heating, cooling and hydrogen production. The suggested configuration was analyzed according to energy and exergy aspects (Figure 18). They found that the total energy efficiency and exergy efficiencies were 33.9% and 43.6%, respectively. Also, the net electricity production, hot water flow rate, cooling load and hydrogen production were calculated as 817 kW, 7.1 kg/s, 1900 kW and 0.05 g/s respectively.

The influence of accurate working fluid properties on predicting the optimum design of an ORC system was studied by Huster et al. [54]. They assumed a geothermal-driven ORC system. An artificial neural networks (ANNs) method was used for optimization. They found that the application of an accurate thermodynamic model results in different design decisions in comparison to a simplified model. Karakilcik et al. [55] investigated a polygeneration system for electricity and hydrogen generation using geothermal energy. An ORC system and a chlor-alkali cell were used for power, and hydrogen generation, respectively. A view of the investigated system is presented in Figure 19. They found the electrical power generation improved from 2.5 to 3.9 MW and H<sub>2</sub> production increased from 10.5 to 21.1 kg/h, with increasing geothermal temperature between 140°C to 155°C. Also, the energy and exergy efficiency of the system was reported as 6.2%, and 22.4%, respectively, with a geothermal temperature of 155°C. Ebadollahi et al. [56] suggested a new geothermal energy-based polygeneration system for cooling, heating,

electricity and hydrogen production which includes an ORC and it is illustrated in Figure 20. It is found that the energy efficiency to be 38.33% and the exergy efficiency to be 28.91%.



Figure 18: A schematic view of a polygeneration system driven by geothermal energy [53].



Figure 19: A schematic view of a power generation system with direct and indirect cycle driven by geothermal reservoir [55].



Figure 20: A schematic view of a polygeneration unit driven by geothermal energy and LNG [56].

Performance investigation of a geothermal-driven ORC for electricity production was also considered in Refs. [57, 58]. Bronicki [59] conducted a review associated with different existing geothermal cites for power generation with the ORC system up until 1988. Vonsée et al. [60] presented an assessment framework of technology dependence for geothermal power based on the ORC system in the European Union. Bonalumi et al. [61] investigated geothermal-driven ORC and flash technologies for power generation. They reported that higher performance could be obtained with the application of supercritical plants with a recuperative layout for the ORC system is presented in Table 1.

Study	Brief title	Highlights	Ref.	
Paloso and	Geothermal OPC and	The result of the numerical study showed that the system		
Mohanty (1003)	absorption shiller	including VAC and ORC had the highest performance	[24]	
Monanty (1995)	absorption chiller	regarding the lower heat exchange area.		
Guzović et al.	Electricity generation by	The ORC yielded 33.01% higher thermal efficiency and	[25]	
(2010)	geothermal energy	18% higher exergy efficiency than the KC.	[25]	
Sauret et al.	Radial-inflow turbines and	R134a was the most appropriate working fluid for the		
(2011)	high-density working fluids	described system.	[26]	
( )		The author found that the regenerative configuration of		
Franco (2011)	A moderate temperature	the ORC system diminished the brine-specific	[27]	
1141100 (2011)	geothermal resource and ORCs	consumption	[= ']	
	Electricity generation from	consumption.		
Guzović et al.	medium temperature	For a medium-temperature geothermal source, the ORC	1201	
(2012)	medium-temperature	system showed better performance than the KC.	[20]	
	geothermal sources			
Gabbrielli et al.	A design approach for	The use of geothermal energy with the lowest	[29]	
(2012)	geothermal power plants	temperature resulted in the best operation.		
	Low-temperature geothermal	By optimizing the plant and using R601a as the ORC		
Li et al. (2012)	water in oilfield power	working fluid, a 40% enhancement in power output was	[30]	
	generation	achieved.		
	Binary power cycle for	The working fluids with critical temperatures close to the		
Zhang and	different EGS geofluid	geofluid temperature present high efficiencies.	[31]	
<b>Jiang (2012)</b>	temperature levels	8	[]	
<b>TT T</b>	Sub- and supercritical ORC	To determine the working fluid for the geothermal power		
Vetter et al.	from low-temperature	plant, the local geothermal fluid temperature and	[11]	
(2013)	geothermal wells	associated optimum critical temperature should be taken		
	8	into consideration.		
	A KC and ORC system based			
Fu et al. (2013)	on coupling with geothermal	The KC performed better than the ORC system.		
. ,	power system			
		Although ammonia yielded the highest performance $n_{-}$		
Mahan at al	Carbon dioxide as a heat	hutane and neopentane could be considered as notantial		
(2013)	transfer fluid	working fluids, considering the correspondence of	[33]	
(2013)	uansier nulu	working nutus, considering the corrosive nature of		
	A geothermal system for	i ne impact of various operational conditions, such as		
AlZaharani et	power, hydrogen and heat	geothermal source temperature, ambient temperature and	[34]	
al. (2013)	generation	cooling water temperature, on the exergy and energy		
	0	efficiency of each cycle, was considered.		
Hahka and Aiih	Operation characteristics for	The parallel connection of ORC had a better economic		
(2013)	two configurations of heat and	performance while the series connection was more	[35]	
(2010)	power systems	energy efficiency.		
		The parallel circuit was preferred for high geothermal		
I: at al (2012)	Series and parallel geothermal	water inlet temperatures and low heat source inlet	120	
Li et al. (2013)	systems in an oilfield	temperatures of the OGTHT, while the opposite was	[30]	
		preferred for the series circuit.		
<b></b>	Heating plant parameters and	Dropping the return temperature by 5 °C increased the		
Habka and Ajib	geothermal plant based on	energy performance by 52% and the exergy performance	[37]	
(2014)	ORC	by 9%	[• ']	
Hsieh at al	A heat exchanger for a	<i>oy y v</i> .		
(2014)	anothermal OPC	R-245fa was selected in the ORC.	[38]	
(4014) Fierebi et el		The areas marghal CIID		
riaschi et al.	An OKC power plant for neat	incross parallel CHP system showed a 51%	[39]	
(2014)	and power generation	improvement in power generation compared to the		

Table 1: Summary of	performance investigations	s of the geothermal-driven	<b>ORC</b> system.
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conventional one.				
Habka and Ajib (2015)	An ORC with and without cogeneration	The zeotropic mixtures, R438A, R422A and R22M performed more efficiently in a single power generation system than pure working fluids.	[40]	
Mohan et al. (2015)	CO <sub>2</sub> -based EGS paired with IGCC for symbiotic integration of CO <sub>2</sub> sequestration	The integration of a high-pressure turbine and an ORC was recommended for power generation.	[41]	
Malik et al. (2015)	An energy-based multi- generation system	The energy and exergy efficiencies of the geothermal cycle were reported as 64.2% and 50.9%, respectively.	[42]	
Proctor et al. A commercial-scale The difference in   (2016) geothermal ORC model   Manente et al. Influence of the ORC turbine The exergy efficient		The difference in power output between the dynamic model and the plant was 0.24%.	[43]	
Manente et al.Influence of the ORC turbine efficiencyThe exergy efficiency of the supercritical OR highest and ranges from 45.4% to 46.5%A tri-generation system		The exergy efficiency of the supercritical ORC is the highest and ranges from 45.4% to 46.5%.	[44]	
Zare et al. (2016)	A tri-generation system utilizing low-grade geothermal energy	The KC yielded higher exergy efficiency than other investigated systems.	[45]	
An et al. (2016)   A hydrothermal geothermal resource in China   Flash and ORC are typically used in Tianjin to mal most of geothermal resources.		Flash and ORC are typically used in Tianjin to make the most of geothermal resources.	[46]	
Sun et al. (2017)	TSORC integrated with AR for geothermal power generation	The geothermal heat source could be used more efficiently with the TSORC-AR compared to the solo TSORC.		
Yuksel and Ozturk (2017)	A geothermal energy-based system for hydrogen production	The hydrogen production surged by 150% when the geothermal water temperature rose from 130°C to 200°C.	[48]	
Erdeweghe et al. (2017)	Series and parallel configurations for a low- temperature CHP plant	The authors found that parallel configurations were more appropriate for high-temperature thermal networks, while series configurations were more appropriate for low-temperature networks.	[49]	
Sadaghiani et al. (2018)	A geothermal-based plant with liquefied natural gas	The numerical study showed the potential of recovering energy from low-temperature heat sources like geothermal hot water.	[50]	
Li et al. (2018)	Poly-generation system driven by geothermal water for oilfield	The output power of the ORC increased by about $300\%$ when heat source temperature increased from 110 to 115 °C.	[51]	
Nian and Cheng (2018)	Geothermal utilization of abandoned oil and gas wells	ORC systems were identified as a promising method to exploit oil and gas wells with high temperatures as geothermal energy.	[52]	
Akrami et al. (2018)	An analysis of a multi- generation energy system	The parametric analysis indicated that a rise in absorber operating temperature, turbine inlet temperature and pressure improved the total exergy efficiency.	[53]	
Huster et al. (2019)	Impact of accurate working fluid properties on an ORC	ANNs method indicated the importance of the accuracy of the thermodynamic model on design decisions.	[54]	
Karakilcik et al. (2019)	A chlor-alkali cell integrated into a geothermal resource	A positive effect on hydrogen production was observed for an increase in the geothermal resource temperature.	[55]	
Ebadollahi et al. (2019)	A geothermal-based multigeneration system using energy recovery	The prices of the heating capacity, cooling capacity, net output power, and hydrogen were estimated to be 480.1 \$/GJ, 441.8 \$/GJ, 292.4 \$/GJ, and 409.4 \$/GJ, respectively.	[56]	

#### **3** Techno-economic analyses of geothermal-driven ORC systems

The financial aspects are very important in order to determine the viability of the ORC systems. Mohanty and Paloso Jr [62] economically examined a geothermal-driven ORC configuration with the application of a vapor absorption chiller (VAC) for increasing power generation compared to the conventional ORC system. They found that the ORC-VAC system can be recommended as a more economical system for power generation. Guo et al. [63] techno-economically evaluated a geothermal-driven ORC system as a cogeneration system which is given in Figure 21. They investigated different ORC working fluids and cycle parameters for the optimization performance of the system. They reported that E170, R600 and R141b showed better performances comprehensively. Vélez et al. [64] studied the low to medium-temperature heat sources that were connected to the organic Rankine cycle for power generation. They reviewed ORC systems based on technical and financial aspects as well as market evolution. Eyidogan et al. [65] performed a techno-economic analysis on ORC power cycles coupled with low-temperature heat sources. It was reported that the investment payback period of an ORC with a biomass-driven system was calculated as 2.7 years for the generation of 1 MW power.



Figure 21: Depiction of the investigated cogeneration system by Ref. [63].

The application of thermal energy storage in an ORC unit coupled with a low-temperature heat source such as geothermal based on techno-economic aspects were investigated by Rodríguez et al. [66]. A transient model was developed for a 1 MW ORC power plant using energy storage technology. Numerical results were validated with experimental results. Fiaschi et al. [67] numerically compared the performance between two power generation cycles including ORC and KC based on geothermal-driven systems. Two different geothermal sites including Mount Amiata, Italy with a heat source of 212°C, and Pomarance, Italy with a heat reservoir of 120°C were investigated. The suggested systems were assessed based on energy, and exergoeconomic aspects. They found that the KC can be recommended as the most efficient cycle, producing 22% to 42% more net power than ORC systems for the low-temperature heat source. Also, the

cost of the electricity was estimated at 12.5 c€/kWh. On the other hand, the ORC with R1233zd(E) had resulted in the best exergoeconomic performance for the medium-temperature heat source. Akrami et al. [68] developed a geothermal-driven system in which an ORC system was used for the generation of electricity which is depicted in Figure 22. The system was analyzed in energy, exergy, and exergoeconomic aspects. The impact of different parameters on the system's performance were investigated. It was found that the energy efficiency and the exergetic efficiency of the suggested system were found at 35.0% and 49.2% respectively. Furthermore, the highest and the lowest total unit costs of the products were reported as 23.18 \$/GJ and 22.73 \$/GJ for the geothermal water temperatures of 185°C, and 215°C respectively.



Figure 22: A schematic view of a polygeneration system driven by geothermal energy [68].

A geothermal-driven power generation system was optimized by Aali et al. [69] using single and multi-objective optimization using the existing data from the Sabalan geothermal field, Iran. The system was analyzed using energy, exergy, and exergo-economic analyses as shown in Figure 23. They found that exergy efficiency and specific cost of output power were found at 52.56% and 4.901 \$/GJ, based on single-objective optimization, and 54.87% and 5.068 \$/GJ based on multi-objective optimization, respectively. Yao et al. [70] economically and thermodynamically investigated a novel integration of a natural gas expansion plant with a geothermal-driven ORC technology as Figure 24 indicates. The fluid in the ORC was R600 and they conducted a multi-objective optimization using the TOPSIS decision-making method for finding the optimal evaporator temperature. The energetic and exergetic efficiencies of the optimized configuration were calculated at 89.8% and 84.13% respectively, with the optimum evaporator temperature of

45.5°C. Furthermore, they expected a net profit of 3.97 M\$ during the lifetime of the plant and a payback period of 2 years for the optimized power generation system.



Figure 23: A schematic view a power system with direct and indirect cycles driven by geothermal energy [69].



Figure 24: A schematic diagram of a power system with geothermal sink coupled to the condenser [70].

A polygeneration system for generating electricity, hot water, and pure water based on a geothermal-driven unit was suggested by Behnam et al. [71] and it is shown in Figure 25. The system was investigated based on energetic, exergetic and thermo-economical aspects and geothermal water at 100 °C. The freshwater production capacity was calculated at 0.662 kg/s. They obtained 161.5 kW electricity and 246 kW heating. Kahraman et al. [72] numerically investigated a geothermal-driven ORC system based on thermodynamic and economic aspects. They investigated the influence of ambient temperature on the energy and exergy performance of the ORC system. They concluded that the power generation reduced to about 6.8 MW as the ambient temperature increases from 5°C to 35°C, whereas first thermodynamic law efficiency and the thermodynamic law efficiency are decreased from 13.7% to 9.2% and 54.9% to 36.7% respectively, with increasing ambient temperature from 5°C to 35°C respectively.

![](_page_25_Figure_1.jpeg)

Figure 25: A schematic view of a power system which exploits geothermal energy and the sea water reservoir [71].

Fraia et al. [73] presented a novel geothermal-driven ORC system for providing electricity and heat by wastewater and sludge treatment. They investigated the suggested system of Figure 26 according to energetic, exergetic and economical points of view. They reported a reduction in

sludge disposal by 70%. Also, they found a payback period of around 5 years and CO<sub>2</sub> equivalent emissions savings of 628 tons per year. Meng et al. [74] studied the techno-economic performance of four different configurations of a geothermal-driven ORC system for the generation of power and heat. Four suggested systems were optimized based on the evaporation temperature and flash temperature. They found that the double-flash ORC yielded a levelized cost of electricity of 0.0831 \$/kWh and a payback period of 9.43 years. Figure 27 shows the examined configuration of the geothermal-driven power unit. Tartiere et al. [75] considered the coupling of a novel cooling system to a geothermal ORC, which showed a noticeable increase in power generation and profit. Most recently, Li et al. [76] showed that a multi-generation system for oilfields, which includes ORC power generation, heating, refrigeration, as well as other oilfield processes, can have a payback period of about 3 years. A summary in relation to the techno-economic analyses of the geothermal-driven ORC systems is presented in Table 2.

![](_page_26_Figure_1.jpeg)

Figure 26: Depiction of a cogeneration system driven by geothermal energy [73].

![](_page_27_Figure_0.jpeg)

Figure 27: A schematic view of a power system with primary and secondary cycle driven by geothermal well [74].

	Table 2: Summary for techno-economic analyses of the geothermal-driven ORC system.				
Study	Brief title	Highlights	Ref.		
Mohanty and Paloso Jr (1992)	Power generation using ORC and geothermal-driven ORC system for power generation	The ORC-VAC system was a more cost-effective system than the solo system.	[62]		
Guo et al. (2011)	A cogeneration system driven by low-temperature geothermal sources	E170, R600 and R141b were introduced as suitable working fluids resulting in a promising performance of the unit.	[63]		
Vélez et al. (2012)	A review of ORCs for the conversion of low-grade heat	ORCs supplied output power ranging from 0.2 MWe to 2 MWe with a cost of 1000 €/kW <sub>el</sub> to 4000 €/kW <sub>el</sub> .	[64]		
Eyidogan et al. (2016)	ORC technologies in Turkey	The potential of low-temperature heat sources such as geothermal, solar energy, biomass and waste heat for feeding an ORC were considered.	[65]		
Rodríguez et al. (2016)	Thermal energy storage solutions for a CSP-ORC plant	The possibility of the usage of thermal energy storage in an ORC unit joined with a low-temperature heat source was considered.	[66]		
Fiaschi et al. (2017)	An ORC and KC to exploit low and medium-high temperature geothermal sites	The KC was found to be a better system than the ORC to exploit low-temperature geothermal heat sources.	[67]		
Akrami et al. (2017)	A polygeneration energy system based on geothermal energy	The highest and lowest cost of the products was calculated as 23.18 \$/GJ and 22.73 \$/GJ for geothermal water temperature of 185 °C and 215 °C, respectively.	[68]		

`able 2: Summar	y for techno-o	economic analyses	s of the geothern	nal-driven ORC s	vstem.
	•/	•/	<b>a</b>		

Aali et al. (2017)	Optimization of a flash-binary cycle	A 3.4% difference between the specific cost of the output power achieved by single and multi-objective optimization methods was observed.	[69]	
Yao et al. (2018)	A geothermal system integrating a natural gas expansion plant	Energy and exergy efficiencies of the optimized system were calculated as 89.8% and 84.13% by the TOPSIS decision-making method.	[70]	
Behnam et al. (2018)A tri-generation system driven by low-temperature geothermal sources		The system produced 0.662 kg/s of fresh water, 161.5 kW of power, and 246 kW of heat.		
Kahraman et al. (2019)	A 21 MW geothermal plant and the effect of ambient temperature	It was observed that the ambient temperature had a considerable impact on the energy and exergy efficiencies of the system.	[72]	
Fraia et al. (2019)	A geothermal based unit for wastewater and sludge treatment	The unit contributed to saving CO <sub>2</sub> equivalent emissions of 628 tons per year.	[73]	
Meng et al. (2020)	Enhanced geothermal system	The levelized cost of electricity generated by the optimized double-flash ORC was 0.0831 \$/kWh.	[74]	

## 4 Experimental studies of geothermal-driven ORC systems

The experimental investigations were done to study the performance of the geothermal-driven ORC and to determine the limitations and the difficulties of this technology. Tang et al. [77] investigated the impact of twin-screw expander application in geothermal-driven ORC systems for electricity experimentally, as it is shown in Figure 28. The influence of various parameters was considered on the performance of the expander. The numerical model they developed was also validated from the experimental tests. They reported the energy efficiency of the ORC system at 7.5%. Yang et al. [78] designed a geothermal-driven ORC system for power generation from abandoned oil wells in the Huabei oilfield of China. The fluid R245fa was selected in the ORC and Figure 29 illustrates the studied configuration. The final results showed an efficiency of 78.52 % for the suggested turbine and an ORC efficiency of 5.33% based on experimental investigations.

![](_page_28_Picture_3.jpeg)

Figure 28: A photograph of the examined experimental setup by Ref. [77].

![](_page_29_Figure_0.jpeg)

Figure 29: Depiction of the suggested geothermal ORC system by Ref. [78].

Hu et al. [79] designed and experimentally tested a geothermal-driven ORC system under partial load conditions. A 500 kW ORC with R245fa was investigated. The analyses were conducted for a case study at the Huabei oilfield, China. They found that the geothermal water flow rate had an impact on the performance of the ORC. Wang et al. [80] experimentally investigated a new variable electricity capacity based on a geothermal-driven flash-ORC system. They proposed this system due to the variable temperature of the geothermal energy during a typical day, as well as in different seasons. The system was evaluated at both steady and dynamic conditions. The maximum net electricity production of the ORC subsystem was 0.74 kW in steady-state conditions. Also, it was reported that power generation increased with decreasing the load.

An experimental investigation for an ORC unit for power generation was done by Song et al. [81]. A photograph of their experimental setup is illustrated in Figure 30. Two scenarios were considered for coupling the ORC system: geothermal energy only or hybrid system with solar irradiation and geothermal energy. Thermodynamic modeling was conducted using MATLAB software. Variation of solar radiation and ambient temperature was investigated. They found 11.21% higher energy efficiency of the hybrid-driven ORC unit compared to the single geothermal-driven ORC system for power generation. Lin et al. [82] experimentally investigated the energetic behavior of a 10 kW ORC that was driven with a low-temperature heat source such as geothermal. The fluid R245fa was used in the ORC and the total configuration is given in Figure 31. They concluded that the net thermal efficiency was 8.9%, while the net electricity efficiency was 7.9%.

![](_page_30_Picture_0.jpeg)

Figure 30: A photograph of the examined experimental setup by Ref. [81].

![](_page_30_Figure_2.jpeg)

Figure 31: Depiction of the investigated power generation unit by Ref. [82].

Chao et al. [83] experimentally investigated a geothermal-driven flash-ORC for electricity and they gave the emphasis on the optimization of the working fluid (R245fa) mass flow rate. Chaiyat et al. [84] studied the CCHP of Figure 32 based on levelized energy and exergy costs in a life cycle evaluation. The suggested unit was driven by geothermal energy. Also, an ORC system with R-245fa was used for electricity production. They concluded that the energetic and exergetic outputs of the CCHP unit were equal to 32.62 kWh and 6.98 kWh with mean efficiencies of 11.6% and 11.2% respectively. Also, it was stated that the levelized energy and exergy and exergy costs were calculated as 0.069 \$/kWh and 0.323 \$/kWh, respectively. Welzl et al. [85] conducted some experimental tests of nucleate pool boiling heat transfer coefficients in an evaporator of a geothermal-driven ORC system for power generation. Two organic fluids were

investigated including R245fa, and R1233zd(E). They concluded that R245fa had higher heat transfer characteristics of up to 43.2% compared to R1233zd(E). Also, the electricity production of the ORC system with R245fa resulted in higher power output compared to the application of R1233zd(E). Experimental investigations on a geothermal-driven ORC system were also conducted in Ref. [86]. A summary of experimental works related to performance investigation of geothermal-driven ORC systems based is presented in Table 3.

![](_page_31_Figure_1.jpeg)

Figure 32: A schematic view of the suggested power production system by Ref. [86].

Table 3: Summary	, for ex	nerimental	nerformance	investigations	of the	geothermal-driven	<b>ORC</b> system
rabic 5. Summary	101 CA	permentai	per for manee	mvesugations	or the	geother mai-ut iven	One system

Study	Brief title	Highlights		
Tang et al.	Twin-screw expander in a	Twin-screw expanders can be effectively coupled with heat	[77]	
(2015)	geothermal ORC	sources over a wide range of temperatures.	[//]	
Yang et al.	An ORC system using a geothermal resource from	According to the experimental test, the efficiency of the suggested turbine and ORC were 78.52 % and 5.33%.		
(2017)	abandoned oil wells			
	Design and test of a			
Hu ot al. (2017)	geothermal-driven ORC	To have the stability of the system's operation, the stability of	[70]	
110 et al. (2017)	system in Huabei Oilfield,	the geothermal water flow rate was essential.		
	China			
Wang of al	A variable-capacity power	The power generated by the flash OPC system increased by		
(2017)	system driven by geothermal	decreasing the load	[80]	
(2017)	energy	decreasing the load.		

Song et al. (2019)	Solar and geothermal energy coupled power generation system	The efficiency of the hybrid-driven ORC system was 11.21% higher than that of the single geothermal-driven ORC.	[81]
Lin et al. (2019)	The behavior of a 10 kW ORC using a scroll-type expander	Net thermal efficiency of 8.9% and net electricity efficiency of 7.9%.	[82]
Chao et al. (2019)	The stability study of a flash-binary power system	The optimum organic fluid mass flow rate was determined according to the different temperatures of the heat source.	[83]
Chaiyat et al. (2020)	Levelized energy and exergy costs per life cycle assessment of a co- generation system	The CCHP unit generated net output energy and exergy of 32.62 kWh and 6.98 kWh, respectively.	[84]
Welzl et al. (2020)	Experimental evaluation of nucleate pool boiling heat transfer correlations	A higher power output of the ORC unit was achieved with R245fa as the working fluid than with R1233zd(E).	[85]

## 5 Optimization of the geothermal-driven ORC systems

Optimization is important for the proper design of the systems in order to have high energy performance and to be financially viable. Hettiarachchi et al. [87] optimized a geothermal-driven ORC system. They used the steepest descent method for optimization. Different parameters were investigated in the optimization study including the evaporator and condenser temperature levels, and the water velocity. Furthermore, the influence of different organic fluids was investigated including ammonia, R123, n-pentane and PF5050. Based on exergy analysis, they concluded that in the optimization process the efficiency was more compromised for ammonia than for the other working fluids. Shengjun et al. [88] examined the performance of a geothermal-driven ORC system based on a subcritical and transcritical cycle. They reported that the application of R123 in a subcritical ORC system was recommended for reaching the highest energetic and exergetic efficiencies of 11.1% and 54.1% respectively. Also, the application of R125 as the ORC working fluid was reported as the most cost-effective approach in the transcritical power cycle.

Generally, the performance of the geothermal-driven ORC depends on the heat source and the sink temperatures. Consequently, the performance of the ORC system varies with the change of the ambient temperature. Manente et al. [89] created an off-design model for optimum power generation with the variation of ambient temperatures from 0 °C to 30 °C and geo-fluid temperatures from 130°C to 180°C. Garg et al. [90] examined the application of isopentane, R-245fa and their mixtures (in 0.7 / 0.3 mole fraction) as the working medium of an ORC with low-temperature level heat sources such as solar or geothermal (see figure 33). They reported an optimum energy efficiency of about 13% with turbine expansion ratios in the range of 7 to 10.

![](_page_33_Figure_0.jpeg)

Figure 33: Depiction of the evaluated ORC regenerative system by Ref. [90].

The thermodynamic performance optimization of an ORC unit connected to a mediumtemperature heat source such as geothermal energy was carried out Maraver et al. [91]. They presented guidelines for the optimization of subcritical and transcritical ORC units with or without regeneration. Different ORC operating mediums were investigated including Toluene, R245fa, n-Pentane, Solkatherm, R134a and Octamethyltrisiloxane. Liu et al. [92] optimized the performance of a geothermal-driven ORC for isobutane/isopentane (R600a/R601a) mixtures as the ORC organic fluid which is illustrated in Figure 34. The optimization was done for various mole fractions of R600a/R601a mixtures. Also, the influence of geothermal water temperature levels of 110°C, 130°C and 150°C was considered. With the application of an R600a/R601 mixture, an increased power generation of 11% was reported for geothermal water temperature levels of 110°C when compared to using pure R600a. The maximum power generation was found when using R600a at a mole fraction of about 0.9.

![](_page_33_Figure_3.jpeg)

Figure 34: A schematic view of the suggested system driven by geothermal water [92].

A two-stage series ORC (TSORC) coupled with a low-grade heat source such as geothermal energy as shown in Figure 35 was optimized by Li et al. [93]. They found that the TSORC is more preferable than an ORC for electricity production. Sadeghi et al. [94] energetically and exegetically optimized three different cases of geothermal-driven ORC units for electricity production using zeotropic mixtures. The investigated configurations included the ordinary ORC, PTORC and TSORC, as they are presented in Figure 36. They concluded that power generation of the simple ORC, PTORC and TSORC improved with 27.76%, 24.98% and 24.79% with the application of the zeotropic mixtures, respectively.

![](_page_34_Figure_1.jpeg)

Figure 35: Depiction of the investigated system by Ref. [93].

![](_page_34_Figure_3.jpeg)

Figure 36: Configurations and T-s diagrams of the three examined configurations of Ref. [94].

The optimization procedure of a geothermal-fed ORC with the application of a coaxial heat exchanger was studied by Mokhtari et al. [95]. Different working fluids were investigated

including R123, R134a, R245fa, and R22. They reported that the exergy and energy efficiencies increased to 8.7% and 13% respectively when using the optimum configuration of the ORC. Zhao et al. [96] investigated a geothermal-driven system for electricity production and cooling as depicted in Figure 37. An ORC system and an ejector refrigeration cycle were applied for power generation and cooling respectively. The suggested system was evaluated based on thermodynamic and exergo-economic investigations. The system was optimized for maximizing the exergetic efficiency and minimizing the levelized cost per unit exergy of products using two single-objective optimizations. It was reported that the best thermodynamic performance could not obtain the calculated optimal exergo-economic design.

![](_page_35_Figure_1.jpeg)

Figure 37: A schematic view of a system with two turbines and ejectors driven by geothermal energy [96].

Design and optimization for the structural and operational parameters of geothermal-driven ORC for power generation under different environmental conditions were carried out by Huster et al. [97]. They used isobutene as the organic fluid of the ORC. They found higher power generation at lower ambient temperatures, whereas they reported levelized costs of electricity of between 41 US-\$/MWh and 60 US-\$/MWh at an optimum design. Zhu et al. [98] investigated numerical modeling for presenting the optimum power generation map based on geothermal energy. The main goal was performance comparison of DF, FORC, and DFORC cycles with SF cycle for increasing power generation by 20% with R245fa as working fluid. For the best thermodynamic performance, the FORC and DF cycles were recommended for a geofluid temperature of less than 170°C, and greater than 170°C, respectively. Furthermore, Zhao et al. [99] and Lu et al. [100] considered the optimum flash and evaporation temperatures of the SF, DF, FORC and DFORC based on geothermal energy. The generation of maximum net power output was selected as an objective function during the optimization process. Five different organic fluids

were investigated including R123, R152a, isobutane, n-pentane and R245fa. The investigated systems were considered based on techno-economic analyses. The SF system showed the lowest performance compared to the other investigated power generation systems. Zhou et al. [101] optimized a geothermal-driven ORC system as presented in Figure 38. The particle swarm optimizer (PSO) was used for the optimization of the power output. The Sabalan geothermal power plant in Ardabil, Iran, was investigated as a case study for driving the ORC system. The energy and exergy efficiencies were calculated at 18.2% and 62.4% respectively. Also, they reported zeotropic mixtures for generating the highest power output.

![](_page_36_Figure_1.jpeg)

Figure 38: A schematic diagram of a steam power cycle and an ORC fed by geothermal energy [101].

A polygeneration unit based on a geothermal working fluid as the heat source and an LNG regasification process as the heat sink was investigated by Emadi and Mahmoudimehr [102] thermodynamically and economically. Two ORC systems were placed between the heat source and the heat sink for power generation as shown in Figure 39. They conducted a comprehensive parametric analysis and an optimization study based on the coupling Genetic Algorithm (Artificial Neural Network). The optimum design yielded a total cost rate of 424 \$/hr, a hydrogen production capacity of 276.1 kg/hr, and an exergy efficiency of 24.92%. Özkaraca and Keçebaş [103] numerically optimized the thermodynamic efficiency of a geothermal-driven ORC unit for power generation based on a gravitational search algorithm. The exergetic efficiency of the optimized ORC was 31%.

In conclusion, as also shown by Lee et al. [104] and Haghighi et al. [5], many research efforts have gone into modeling and optimization in order to improve geothermal-driven ORC systems. A recent study by Zhi et al. [105] can be highlighted, where a novel transcritical-subcritical ORC with zeotropic mixtures was optimized. They reported that, by adopting a zeotropic mixture, system performance can be significantly enhanced. A summary of optimization works for geothermal-driven ORC systems is presented in Table 4.

![](_page_37_Figure_2.jpeg)

Figure 39: Depiction of a system with double stage ORC and other devices driven by geothermal energy [102].

Study	Brief title	Highlights	Ref.
Hettiarachchi et al. (2007)	Optimum design criteria for a geothermal ORC	Parameters such as evaporation and condensation temperatures, geothermal and cooling water velocities were changed to acquire the optimal design.	[87]
Shengjun et al. (2011)	A subcritical ORC and transcritical power cycle system	R123 and R125 yielded the highest exergy efficiency and the most cost-effective system, respectively.	[88]
Manente et al. (2013)	An ORC design for the control strategy	The authors optimized the system according to the variation of environmental conditions.	[89]
Garg et al. (2013)	Isopentane, R-245fa and their mixtures as working fluids for ORC	The optimum energy efficiency was reported to be around 13% for the mixtures of working fluids.	[90]
Maraver et al. (2014)	Optimization of ORCs constrained by technical parameters	A guideline for optimizing the ORC system with regenerative and non-regenerative cycles was introduced.	[91]
Liu et al. (2015)	Geothermal ORCs using R600a/R601a mixtures	ng To generate the same power with a lower heat transfer area, the geothermal source temperature should rise.	
Li et al. (2015) Optimization of ORC using two-stage evaporation TSORC performed better compared to ORC for power generation.		[93]	
Sadeghi et al. (2016)	Various ORC configurations using zeotropic mixtures	The usage of zeotropic mixtures increased the power generation of a simple ORC by 27.76%.	[94]
Mokhtari et al. (2016)	A geothermal Rankine cycle utilizing a coaxial heat exchanger	The optimum design of the ORC system increased the exergy and energy efficiencies to 8.7% and 13%.	
Zhao et al. (2016)	Optimization of a CCP system driven by the geothermal source	The exergy efficiency and the average levelized costs were optimized by two single-objective optimization methods.	
Huster et al. (2017)	Design of a geothermal ORC	Lower ambient temperatures were more suitable for a geothermal-driven ORC system.	[97]
Zhu et al. (2017)	Optimum flash and evaporation temperatures under different geofluid conditions	To improve the power generation unit by 20%, four different power generation cycles were studied.	[98]
Zhao et al. (2017)	Optimum flash and evaporation temperatures under different geofluid conditions	It was found that the optimum flash and evaporation temperatures rose with an increase in geofluid temperature and dryness.	[99]
Lu et al. (2018)	Compound power cycles for enhanced geothermal systems	The five different systems including SF, DF, FORC and DFORC were compared to each other based on levelized electricity cost and payback period.	[100]
Zhou et al.	Geothermal flash and dual-	Zeotropic mixtures yielding the maximum output power	[101]
(2019) Emadi and Mahmoudimehr (2019)	pressure evaporation ORC A geothermal heat source and LNG heat sink	Consisted of Pentane /Cis-2-butene, and Pentane/Trans-2-butene. The optimized unit produced power with a total cost rate of 424 \$/hr and exergy efficiency of 24.92%.	[102]
Özkaraca and Keçebaş (2019)	Maximum exergy efficiency of a geothermal power plant	The unit was optimized by the gravitational search algorithm.	[103]

Table 4: Summary	v of the on	otimization in	vestigations of tl	he geothermal-driven	<b>ORC</b> system.

#### 6 Hybrid solar/geothermal ORC systems

Hybrid systems are introduced for increasing the performance of geothermal-driven ORC systems. Usually, geothermal energy is combined with solar irradiation to enhance the energy input potential in the system and to exploit two renewable energy sources. Zhou [106] investigated a hybrid geothermal/solar-driven ORC system for power generation based on subcritical and supercritical power cycles as depicted in Figure 40. They reported that the suggested hybrid power configuration could generate 19% more electricity annually as compared with the two stand-alone power plants. Ruzzenenti et al. [107] investigated a combined geothermal-solar system coupled with an organic Rankine cycle for the producing of heat and power based on environmental sustainability aspects as shown in Figure 41. They evaluated the feasibility of exploiting abandoned wells.

![](_page_39_Figure_2.jpeg)

Figure 40: Depiction of the suggested hybrid power generation system by Ref. [106] which exploits both solar and geothermal energy.

![](_page_39_Figure_4.jpeg)

Figure 41: Depiction of the suggested system by Ref. [103].

Islam and Dincer [108] studied a combined solar-geothermal system as a poly-generation system as exhibited in Figure 42. The system was investigated based on energy and exergy investigations for 4 cases including single-generation, co-generation, tri-generation and poly-generation. The influence of many parameters on energy and exergy performance was considered. They found the energy and exergy efficiencies of the polygeneration unit to be 51% and 62% respectively. Ahmadi, Boyaghchi and Nazer [109] suggested a poly-generation system for generating power, producing hydrogen and oxygen, cooling, heating, and drying. Combined geothermal energy and concentrated photovoltaic thermal were coupled to the system as depicted in Figure 43. They found that the cost reduced by 18.3% and the environmental impact criteria improved by 24.9% when the system was optimized. Energy efficiency increased by about 27.4% and the exergy efficiency improved about 2 times. Furthermore, they reported that the power generation improved by 50.3% as compared to the nominal point.

![](_page_40_Figure_1.jpeg)

Figure 42: Depiction of a complex polygeneration system which exploits solar and geothermal energy [108].

![](_page_41_Figure_0.jpeg)

Figure 43: A Depiction of o a polygeneration system driven by geothermal energy and solar concentrating photovoltaics [109].

A model was presented by Li et al. [110] for performance optimization of a hybrid geothermal/solar-driven ORC by applying a compound objective function methodology. They concluded that the performance of the ORC system increased when coupling with hybrid geothermal/solar energy compared to using a single heat source. Khosravi et al. [111] developed an artificial intelligence approach for modeling a hybrid geothermal/solar-driven ORC unit for electricity production as displayed in Figure 44. The method for this modeling was conducted by the ANFIS optimized with PSO (ANFIS-PSO) and MLP-PSO. The modeling was developed based on thermodynamic and financial aspects of the ORC technology. Different design parameters were considered during modeling including solar irradiation, well temperature level, working fluid flow rate, turbine outlet pressure level, collecting area and inlet pressure level in the preheater. They reported better modeling results of the hybrid ORC system with ANFIS-PSO than with MLP-PSO. Atiz et al. [112] numerically considered a hybrid geothermal/solar-driven ORC system for power generation under energy, exergy, and power output aspects as presented in Figure 45. They found that the application of the solar collector had an effective influence on enhancing the performance of the suggested ORC system. The highest energy and exergy efficiency values of the unit were reported as 6.92% and 21.06% using n-butane as the ORC fluid respectively.

![](_page_42_Figure_0.jpeg)

Figure 44: Depiction of an ORC which is driven by solar and geothermal energy [111].

![](_page_42_Figure_2.jpeg)

Low-grade geothermal resource

Figure 45: Depiction of a power system with evacuated tube solar collectors and geothermal reservoir [112].

A new hybrid geothermal-solar ORC system with flash-binary configuration was suggested by Wan et al. [113] as displayed in Figure 46. The energy and exergy efficiency values o were reported at 10.74% and 23.9% respectively. They found that the thermodynamic performance improves with increasing flash pressure. Hybrid geothermal/solar-driven ORC systems have been investigated by many researchers as an effective approach for improving power generation performance [114, 115]. Liu et al. [116] presented a hybrid geothermal/fossil energy-driven ORC unit for power generation. Geothermal energy was used for preheating the feedwater in the coal-fired power system. They developed models for the investigation of two configurations including parallel and serial geothermal preheating configurations. They studied the impact of different geothermal temperatures on the performance. They concluded that the serial configuration

generally generated more power than the parallel configuration. Lastly, Heidarnejad et al. [117] presented a thermodynamic study of a biomass-geothermal power plant combined with a desalination system. It was reported that energetic and exergetic efficiencies of 13.9% and 19.4% could be reached respectively. A summary of the related works to the performance investigations of hybrid solar/geothermal ORC is reported in Table 5.

![](_page_43_Figure_1.jpeg)

Figure 46: A schematic view of a power system with parabolic trough solar collectors and geothermal reservoir [113].

	v i			
Study	Brief title	Highlights	Ref.	
Zhou (2014)	Hybridization of solar and geothermal	The supercritical hybrid unit generated electrical	[106]	
	energy	power more economically than stand-alone systems.	[100]	
Ruzzenenti et	A micro-CHP system fueled by	The feasibility of exploiting abandoned wells was	vells was [107]	
al. (2014)	geothermal and solar energy	investigated in this research.		
Liu et al. (2016)	A hybrid geothermal-fossil power	The role of geothermal energy was the preheating of	[22]	
	generation system	the feed water in the coal-fired power unit.	[22]	
		Four kinds of systems, single generation,		
Islam and	A solar and geothermal energy-based	cogeneration, tri-generation, and multi-generation,	[109]	
Dincer (2017)	integrated system	were investigated regarding exergy and energy	[108]	
		efficiency.		
Ahmadi	Concentrated abotevialtais thermal	An 18.3% reduction in cost and a 24.9% improvement		
Boyaghchi and	concentrated photovoltate thermal-	in environmental impact criteria were attained by	[109]	
Nazer (2017)	geothermal system	optimizing the proposed unit.		
Li et al. (2018)	TSORC is driven by geothermal energy	The hybrid unit performed more efficiently compared	[110]	

Table 5: Summary	for the performance	investigations of hy	brid solar/geothermal	<b>ORC</b> systems
•	1	8 .	8	•

	coupled with solar energy	to the system with a single heat source.	
Khosravi et al. (2019)	A geothermal based-ORC equipped with a solar system	The effect of parameters including solar radiation, well temperature, and surface area of the solar collector on the performance of the hybrid unit was investigated.	
Atiz et al. (2019)	A low-temperature geothermal resource and solar energy	The maximum overall energy and exergy efficiencies were 6.92% and 21.06% respectively when n-butane was the ORC working fluid.	[112]
Wan et al. (2019)	A geothermal-solar flash-binary hybrid system	Energy and exergy efficiencies were evaluated as 10.74% and 23.9%, respectively.	[113]

## 7 Challenges and opportunities

Geothermal energy is a renewable and sustainable energy source and thus it is an attractive choice that concentrates a great amount of interest. The relatively low temperature levels of this energy source make it ideal for coupling with the ORC. Generally, ORC exhibits a better performance as compared with the Kalina cycle when coupled with the geothermal energy sources [25, 28]. On the other hand, natural refrigerants, such as R600a, are promising choices for the ORC from both the environmental and the energy points of view [30]. From the energetic perspective R245fa and R141b appear to be good choices, however, they are not environmentally friendly and thus they should not be preferred.

The parallel configuration is more efficient than the series one in power and heat production systems [35, 36, 39]. An enhancement as high as 51% has been reported with the parallel configuration [39]. The literature search revealed that the highest performance is obtained in the multigeneration system [42] with 64.2% energetic efficiency and 50.9% exergetic efficiency. Moreover, the exergy efficiency of a geothermal-based ORC with supercritical CO<sub>2</sub> is found to be around 45% [44]. On the other hand, the experimental studies indicate relatively lower efficiency values [78, 82]. Thus, more experimental studies are needed to validate the above-mentioned high-performance results in relation to the geothermal-based ORC systems.

An increase in the geothermal temperature level enhances significantly the unit performance. The increase of the geothermal temperature from 130°C to 200°C led to a 150% increase in hydrogen production [48], while the temperature increases from 110°C to 150°C led to 300% increase in the electricity production of the ORC [51]. Using the optimization techniques, further performance improvement in the range of 20% to 30% has been achieved [94, 98].

The levelized cost of electricity with a geothermal ORC system is found to be as low as 0.0831 \$/kWh in [74] with a payback period of about 9 years. Some other studies claim much lower payback periods with geothermal ORC systems, e.g. as low as 2.7 years [65] and around 2 years with a geothermal-natural gas system [70]. These results are encouraging for the viability of the geothermal-driven ORC systems.

Geothermal energy is an important energy source; however, it faces some serious limitations. More specifically, geothermal power plants require a high amount of investment due to the high drilling cost. Moreover, the extraction of geothermal energy is associated with the release of greenhouse gases and this fact leads to possible environmental limitations. The release of gases like CO<sub>2</sub>, NH<sub>3</sub> and H<sub>2</sub>S from the geothermal power generation systems has to be taken into serious consideration for the environmental assessment and in the life cycle analysis.

Another issue that may lead to limitations in geothermal applications, especially in urban areas, is the need for extensive land utilization to obtain high amounts of heat inputs. The use of vertical ground heat exchangers is a solution to this problem. On the other hand, the geothermal heat sink may possibly lead to cooling down the ground gradually. In such a case, the system has to shut down its operation for some period of time and then restart when the ground reaches the proper temperature levels.

The ORC systems, especially the ones with low capacity come with a relatively high cost. Moreover, the working fluids are flammable and toxic in some cases. Thus, there is a need for a suitable selection of the working fluids. When compared with the water/steam cycles, the ORC systems provide restricted performance due to the low and medium operating temperature levels. Therefore, their careful design is needed in order to enhance the thermodynamic efficiency of the ORC devices and especially the expander.

## 8 Future Directions

A significant amount of work is available in the literature on the domain of geothermal-based ORC units. However, more research efforts are needed in order to improve the efficiency of these units and eliminate the limitations mentioned above. It is important to optimize these systems using novel algorithms which use artificial intelligence in order to minimize the computational time during the optimization procedure. In any case, energy, exergy and financial aspects have to be taken into account during the optimization procedures.

Moreover, there is a need for investigating new organic fluids which are ideal for the operating temperature levels of the geothermal-driven units. Natural refrigerants are promising and the binary mixtures have to be tested theoretically and experimentally. Fluids with low global warming potential and zero ozone depletion potential are ideal choices, as well as they have to be safe choices (low flammability and low toxicity). Moreover, the cost of organic fluids has to be reasonable to reduce the overall cost of the systems.

There is a need for conducting experimental studies with different scales. More specifically, investigation of higher capacity systems is needed in order to predict the efficiency of commercial size systems accurately. The computationally optimized models need to be validated through the experimental results in order to have multilateral approximations.

More studies should be conducted to study the simultaneous use of geothermal energy and other heat sources. A combination of geothermal energy and waste heat may be considered in this regard. Finally, the use of geothermal energy in polygeneration systems is another issue worth investigating in order to analyze various heat inputs in highly efficient systems with many useful

outputs. The exploitation of the geothermal potential in the building sector through the use of polygeneration units is an important area to be investigated more in the future.

## 9 Conclusions

Organic Rankine cycles can convert low-grade heat input into work with an acceptable conversion ratio. Geothermal energy is one of the most promising renewable energies that can provide heat input at different temperature levels. The goal of the present review paper is to investigate the different aspects of the geothermal-driven ORC in order to define the cases with the highest performance and the most important parameters that affect the system efficiency. The emphasis in determining the performance is given to the energy efficiency, exergy efficiency, financial indexes, environmental parameters, optimization procedures and experimental studies. Hybrid solar/geothermal ORC systems including geothermal units with different solar collectors were also reviewed. The following conclusions can be derived from the current work:

- Geothermal-driven ORC systems lead to viable investments with relatively low payback periods.
- There are cases with high energy and exergy efficiencies, especially in the cases with more useful outputs (e.g. multigeneration systems). This indicates the need for combining geothermal energy and ORC with additional energy devices.
- The parallel configuration is more efficient than the series configuration in electrical and heat production.
- The natural working fluids are promising choices for achieving high efficiency and environmentally friendly systems. The toxicity and flammability issues need to be taken into account for choosing the proper working mediums.
- The optimization of the system is able to increase the performance by around 20% to 30% that is important in order to have sustainable configurations.
- Especially in polygeneration systems with geothermal energy, there is a possibility to achieve high efficiency. So, the system energy efficiency of 65% and exergy efficiency of 50% can be achieved.
- The exploitation of geothermal energy as the heat source in power systems is a financially promising choice that can lead to a low payback period which is ranges from 2 up to 9 years.
- The increase of the geothermal temperature levels leads to higher exergy input and the possibility for increasing the electricity production (or the other useful products) at a higher level.
- There is a need for further practical and experimental studies about the combination of ORC with geothermal plants especially in hybrid systems with geothermal energy and solar or waste heat inputs.

## Abbreviations

ANFIS	Adaptive neuro-fuzzy inference system
ANNs	Artificial neural networks
AR	Absorption refrigeration
CCHP	Combined cooling, heating and power
CCP	Combined cooling and power
CHP	Combined heating and power
CSP	Concentrated solar power
DF	Double-flash
DFORC	Double-flash organic Rankine cycle
FORC	Flash-organic Rankine cycle
GPP	Geothermal power plant
GWP	Global warming potential
IGCC	Integrated gasification combined cycle
HRS	Heat recovery system
HTF	Heat transfer fluid
KC	Kalina cycle
LNG	Liquefied natural gas
MGS	Multigeneration system
MLP	Multilayer perceptron
ORC	Organic Rankine cycle
OGTHT	Oil gathering and transportation heat tracing
PSO	Particle swarm optimizer
PTORC	Parallel two-stage organic Rankine cycle
SF	Single-flash
TOPSIS	Technique for order preference by similarity to the ideal solution
TSORC	Two stage serial organic Rankine cycle
TU	Thermal utility
VAC	Vapor absorption chiller

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