

6 REFERENCES

1. Von Bogdandy, L.; Engell, H.J.; 1971; The Reduction of Iron Ores; *SPRINGER-VERLAG*; Berlin
2. Keplinger, W., Maschlanka, W., Wallner, F.; 1990; The Corex Process – Development And Further Plans; *COREX SYMPOSIUM, SAIMM SP4*; pp 5-20.
3. Biswas, A.K.; Principles Of Blast Furnace Ironmaking; *COOTHA PUBLISHING HOUSE*, Australia; pp 1-13.
4. Hauk, R.; 1990; Raw Materials For The Corex Process; *COREX SYMPOSIUM, SAIMM SP4*; pp 21-34
5. <http://www.mindat.org/min-1856.html>; Oktober 2007
6. Taylor,D.; 1984; Thermal Expansion Data: III Sesquioxides, M_2O_3 , With The Corundum And The A-, B- and C- M_2O_3 Structures; *BRIT CERAM SOC*; J and Trans; Vol. 83; p92
7. Megaw, H.D.; 1973; Crystal Structures: A Working Approach; *SAUNDERS*; Philadelphia
8. Deer, W.A., Howie, R.A., Zussman, J.; 1971; In Introduction To The Rock-Forming Minerals; *LONGMAN*, London
9. Taylor,D.; 1985; Thermal Expansion Data VI: Complex Oxides, AB_2O_4 , The Spinels; *BRIT CERAM SOC*; J and Trans; Vol 84; p121
10. Bernal, J.D., Dasgupta, D.R., Mackay, A.L.; 1957; Nature; Vol. 180; pp645-647.

11. Roller, P.W.; 1986; Letter to the editor: The Theoretical Volume Decrease On Reduction Of Hematite To Magnetite; *ISIJ*; pp834-835
12. Loo, C.E., Bristow, N.J.;1998; Properties Of Iron Bearing Materials Under Simulated Blast Furnace Indirect Reduction Conditions Part 2 Reduction Degradation, RDI; *IRONMAKING AND STEELMAKING*; Vol. 25; No. 4; pp287-295
13. Yang, J., Cheng, G.; 1998; A Process For Minimizing Reduction Degradation Of Iron Ore Agglomerates Has Been Put In Practice; *ICSTI/IRONMAKING CONFERENCE PROCEEDINGS*; p1687
14. Brill-Edwards, H., Daniell, B.L., Samuel, R.L.; 1965; Structural Changes Accompanying The Reduction Of Polycrystalline Hematite; *J ISI*; pp361-368.
15. Loo, C.E.; Bristow, N.J.; 1994; Mechanism Of Low Temperature Reduction Degradation Of Iron Ore Sinters; *TRANS. INSTN MIN. METALL.* (sect C: Mineral Process. Extr Metall.); p103
16. Hayes, P.C., Grieveson, P.; 1981; Microstructural Changes On The Reduction Of Hematite To Magnetite; *METALLURGICAL TRANSACTIONS B*; American Society for Metals and The Metallurgical Society of AIME; Vol. 12B; pp579-587
17. Husslage, W.M., Bakker, T., Kock, M.E.m Heerema, R.H.; 1999; Influence Of Reduction Conditions On The Expansion And Microstexture Of Sintered Hematite Compacts During The Transition To Magnetite; *MINERALS AND METALLURGICAL PROCESSING*; Vol. 16; No. 3; pp23-33
18. Pimenta, H.P.; 2002; Influence Of Al_2O_3 And TiO_2 On The Reduction Degradation Behaviour Of Sinter And Hematite At Low Temperatures; *IRONMAKING AND STEELMAKING*; Vol 29; No 3; pp175-179

- 19 El-Geassy, A.A., Nasr, M.I., Hessien, M.M.; 1996; Effect Of Reducing Gas On The Volume Change During Reduction Of Iron Oxide Compacts; *ISIJ INTERNATIONAL*; Vol 36; No. 6; pp640-649
20. Theron, J.A.; 2002; Effect Of The Heating Rate And Other Parameters On Breakdown Of Iron Ore In The Saldanha Steel Corex Shaft – A Laboratory Scale Study
21. Bapat, S.P., Chakravarty, A.K., Mitra, A.N., Mukherjee, T.;1977; Assessment Of The Low-Temperature Breakdown And Swelling Characteristics Of Noamundi Ore, Joda Ore And Sinter; *TISCO*
22. Gudenau, H.W., Burchard, W.G., Rupp, H.; 1979; Direct Observation Of Reduction And Disintegration Processes In The Scanning Electron Microscope, *IRONMAKING PROCEEDINGS*; Vol 38; pp230-234
23. Adam, F., Dupre, B., and Gleitzer, C.; 1988; Cracking Of Hematite Crystals During Low Temperature Reduction Into Magnetite; *REACTIVITY OF SOLIDS*; Vol. 5; pp101-114
24. Porter, J, Swann, P; 1977; High-Voltage Microscopy Of Reduction Of Hematite To Magnetite; *IRONMAKING AND STEELMAKING*; p300.
25. Martens, R., Rausch, H., Serbent, H., Westenberger, H.; 1985; Investigation Of The Interrelation Of Microstructure And Disintegration Behaviour Of Hematite Lump Ores In The Reduction Process; *STEEL RESEARCH* 56, No.3; pp147-152
26. Vreugdenburg, J.C., Van der Vyver, W.F., Kleyenstuber, A.; 2004; Iron Ore Characterization; Kumba Research and Development
27. ISO 4696

APPENDIX 1

ALPHABETICAL LISTING OF THE MINERALS MENTIONED IN THIS REPORT, THEIR IDEAL CHEMICAL FORMULAE AND THE THEORETICAL IRON CONTENT OF THE MINERALS AND DEFINITIONS



Alphabetical listing of the minerals mentioned in this report, their ideal chemical formulae and the theoretical iron content of the minerals and definitions

Mineral	Ideal chemical formula	Theoretical iron content in mass %
Anatase	TiO ₂	
Ankerite	Ca(Fe,Mg,Mn)(CO ₃) ₂	16.24
Apatite	Ca ₅ (PO ₄) ₃ (OH)	
Barite	BaSO ₄	
Calcite	CaCO ₃	
Celestite	SrSO ₄	
Diaspore	AlO(OH)	
Dolomite	CaMg(CO ₃) ₂	
Goethite	α-FeOOH	62.85
Greenalite	(Fe ²⁺ ,Fe ³⁺) ₂₋₃ Si ₂ O ₅ (OH) ₄	44.14
Hematite	Fe ₂ O ₃	69.94
Illite	(K,H ₃ O)(Al,Mg,Fe) ₂ (Si,Al) ₄ O ₁₀ [(OH) ₂ ,H ₂ O]	
Jacobsite	MnFe ₂ O ₄	48.43
Kaolinite	Al ₂ Si ₂ O ₅ (OH) ₄	
Lithiophorite	(Al,Li)MnO ₂ (OH) ₂	
Magnetite	Fe ₃ O ₄	72.36
Muscovite	KAl ₃ Si ₃ O ₁₀ (OH) ₂	
Pyrophyllite	Al ₂ Si ₄ O ₁₀ (OH) ₂	
Quartz	SiO ₂	
Rhodochrosite	MnCO ₃	
Rutile	TiO ₂	
Siderite	FeCO ₃	48.20
Stilpnomelane	K(Fe ²⁺ ,Mg,Fe ³⁺) ₈ (Si,Al) ₁₂ (O,OH) ₂₇	30.40

Specularite	A platy, metallic variety of hematite
Acicular	Slender and pointed, needle-like
Brecciated	A textural term used to describe a rock comprised of angular clasts.
Relict	Term used to describe a mineral that is a remnant or fragment that remains from what was more widely distributed
Earthy	The non-metallic mineral lustre of porous mineral aggregates such as clays.
Microlaminae	Rock layers less than 1cm thick are referred to as laminae, microlaminae are less than 3mm in thickness
Texture	The general character of a rock, shown by its component particles



in terms of grain size and shape, degree of crystallinity and arrangement.

Mesolaminae

Layers less than 1cm thick are referred to as laminae, mesolaminae are thicker than 3mm but less than 1cm.



APPENDIX 2

TEST METHODS



Iron ores for blast furnace feedstocks — Determination of low-temperature reduction-disintegration indices by static method —

Part 1: Reduction with CO, CO₂, H₂ and N₂

Minerais de fer pour l'alimentation des hauts-fourneaux — Détermination des indices de désagrégation par réduction à basse température par méthode statique —

Partie 1: Réduction avec CO, CO₂, H₂ et N₂

[Revision of first edition (ISO 4696-1:1996)]

ICS 73.060.10

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Contents

	Page
1	Scope 1
2	Normative references 1
3	Definitions 1
4	Principle 1
5	Sampling, sample preparation and preparation of test portions 2
6	Apparatus 2
7	Test conditions 3
8	Procedure 4
9	Expression of results 5
10	Test Report 6
11	Verification 6
	Annex A (normative) Flowsheet of the procedure for the acceptance of test results 11

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 4696-1 was prepared by Technical Committee ISO/TC 102, *Iron Ore and Direct Reduced Iron*, Subcommittee SC 3, *Physical Testing*.

This second edition cancels and replaces the first edition (ISO 4696-1:1996), which has been revised to homogenise with other physical test standards.

ISO 4696 consists of the following parts, under the general title *Iron ores for blast furnace feedstocks — Determination of low-temperature reduction-disintegration indices (RDI) by static method*:

- Part 1: Reduction with CO, CO₂, H₂ and N₂
- Part 2: Reduction with CO and N₂

Introduction

This is one of a number of physical test methods that have been developed to measure various physical parameters and to evaluate the behaviour of iron ores including reducibility, disintegration, crushing strength, apparent density, etc. This method was developed to provide a uniform procedure, validated by collaborative testing, to facilitate comparisons of tests made in different laboratories.

Results of this test should be considered in conjunction with other tests used to evaluate the quality of iron ores as feedstocks for blast furnace and direct reduction processes.

This International Standard may be used to provide test results as part of a production quality control system, as a basis of a contract, or as part of a research project.

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2005

Iron ores for blast furnace feedstocks — Determination of low-temperature reduction-disintegration indices by static method — Part 1: Reduction with CO, CO₂, H₂ and N₂

CAUTION This standard may involve hazardous materials, operations and equipment. This standard does not purport to address all of the safety issues associated with its use. It is the responsibility of the user of this International Standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to its use.

1 Scope

Part 1 of this International Standard specifies a method to provide a relative measure for evaluating the degree of size degradation of iron ores when reduced under conditions resembling those prevailing in the low-temperature reduction zone of a blast furnace.

This International Standard is applicable to lump ores, sinters and hot bonded pellets.

2 Normative references

The following referenced documents are indispensable for the application of this International Standard. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3082:2000¹⁾, *Iron ores — Sampling and sample preparation procedures.*

ISO 3310-1:2000, *Test sieves — Technical requirements and testing — Part 1: Test sieves of metal wire cloth.*

ISO 3310-2:1999, *Test sieves — Technical requirements and testing — Part 2: Test sieves of perforated metal plate.*

ISO 4701:1999, *Iron ores - Determination of size distribution by sieving.*

ISO 11323:2002, *Iron ore and direct reduced iron — Vocabulary.*

3 Definitions

For the purpose of this International Standard the definitions given in ISO 11323 apply.

4 Principle

The test portion is isothermally reduced in a fixed bed, at 500 °C, using a reducing gas consisting of CO, CO₂, H₂ and N₂, for 60 min. The reduced test portion is tumbled in a specific tumble drum for 300 revolutions and then sieved with sieves having square openings of 6,3 mm, 3,15 mm and 500 µm. Three reduction-

¹⁾ Under revision to incorporate ISO 10836 – *Iron ores – Method for sampling and sample preparation for physical testing.*

disintegration indices (*RDI*) are calculated as the mass percentage of material greater than 6,30 mm, less than 3,15 mm and less than 500 μm .

5 Sampling, sample preparation and preparation of test portions

5.1 Sampling and sample preparation

Sampling of a lot and preparation of a test sample shall be in accordance with ISO 3082.

The size range for pellets, sinters and lump ores shall be $- 12,5 \text{ mm} + 10,0 \text{ mm}$.

A test sample of at least 2 kg, on dry basis, of the sized material shall be obtained.

Oven-dry the test sample to constant mass at $105 \text{ }^\circ\text{C} \pm 5 \text{ }^\circ\text{C}$ and cool it to room temperature before preparation of the test portions.

NOTE Constant mass is achieved when the difference in mass between two subsequent measurements becomes less than 0,05% of the initial mass of the test sample.

5.2 Preparation of test portions

Collect each test portion by taking ore particles at random.

At least 4 test portions, each of approximately 500 g (\pm the mass of 1 particle) shall be prepared from the test sample.

Weigh the test portions to the nearest 0,1 g and register the mass of each test portion on its recipient label.

6 Apparatus

6.1 General

Test apparatus shall comprise

- a) ordinary laboratory equipment, such as oven, hand tools, time control device and safety equipment;
- b) a reduction tube assembly;
- c) a furnace;
- d) a system to supply the gases and regulate the flow rates;
- e) a tumble drum;
- f) test sieves;
- g) a weighing device.

Figure 1 shows an example of the test apparatus.

6.2 Reduction tube, made of non-scaling, heat-resistant metal to withstand temperatures higher than $600 \text{ }^\circ\text{C}$ and resistant to deformation. The internal diameter shall be $75 \text{ mm} \pm 1 \text{ mm}$. A removable perforated plate made of non-scaling, heat-resistant metal to withstand temperatures higher than $600 \text{ }^\circ\text{C}$ shall be mounted in the reduction tube to support the test portion and to ensure uniform gas flow through it. The perforated plate shall be 4 mm thick, with a diameter 1 mm less than the tube internal diameter. The holes in the plate shall be 2 mm to 3 mm in diameter and shall be separated from each other by 4 mm to 5 mm.

Figure 2 shows an example of reduction tube.

6.3 Furnace, having a heating capacity and temperature control able to maintain the entire test portion as well as gas entering the bed at $500\text{ }^{\circ}\text{C} \pm 5\text{ }^{\circ}\text{C}$.

6.4 Porcelain balls, having a size range between 10,0 mm and 12,5 mm and enough amount to form a double-layer bed on the perforated plate.

6.5 Gas supply system, capable of supplying the gases and regulating gas flow rates.

6.6 Tumble drum, made of steel, at least 5 mm thick, having an internal diameter of 130 mm and an inside length of 200 mm. Two equally spaced steel lifters 200 mm long, 20 mm high and 2 mm thick shall be mounted longitudinally inside the drum. These may be mounted on a frame that can be inserted inside the vessel from one end. One end of the drum shall be closed and the other open. A close-fitting lid shall be held in place on the opening to ensure a dust-tight seal. The drum shall be replaced in any case when the thickness of the plate is reduced to 3 mm in any area, and the lifters when their height is reduced to less than 18 mm.

Figure 3 shows an example of tumble drum.

6.7 Rotation equipment, capable to ensure that the drum attains full speed in one revolution, rotates at a constant speed of $30\text{ rpm} \pm 1\text{ rpm}$ and stops within one revolution. The equipment shall be fitted with a revolution counter and with an automatic device for stopping the drum after a predetermined number of revolutions.

6.8 Test sieves, conforming to ISO 3310-1 or ISO 3310-2 and having square apertures of the following nominal sizes: 6,30 mm; 3,15 mm and 500 μm .

6.9 Weighing device, capable of weighing the test sample and test portions to an accuracy of 0,1 g.

7 Test conditions

7.1 General

Volumes and flow rates of gases are as measured at a reference temperature of 0°C and at a reference atmospheric pressure of 101,325 kPa (1,01325 bar).

7.2 Reducing gas

7.2.1 Composition

The reducing gas shall consist of:

CO	20,0 % (V/V) \pm 0,5 % (V/V)
CO ₂	20,0 % (V/V) \pm 0,5 % (V/V)
H ₂	2,0 % (V/V) \pm 0,5 % (V/V)
N ₂	58,0 % (V/V) \pm 0,5 % (V/V)

7.2.2 Purity

Impurities in the reducing gas shall not exceed:

O ₂	0,1 % (V/V)
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H₂O 0,2 % (V/V)

7.2.3 Flow rate

The flow rate of the reducing gas, during the entire reducing period, shall be maintained at 20 L/min \pm 1 L/min.

7.3 Heating and cooling gas

Nitrogen (N₂) shall be used as the heating and cooling gas. Impurities shall not exceed 0,1% (V/V).

The flow rate of N₂ shall be maintained at 5 L/min until the test portion reaches 500 °C and at 20 L/min during temperature equilibration period. During cooling it shall be maintained at 5 L/min.

7.4 Temperature of the test portion

The temperature of the entire test portion shall be maintained at 500 °C \pm 10 °C during the entire reducing period and, as such, the reducing gas shall be preheated before entering the test portion.

8 Procedure

8.1 Number of determinations for the test

Carry out the test as many times as required by Annex A.

8.2 Reduction

Place a double-layer bed of porcelain balls (6.4) in the reduction tube (6.2) on the perforated plate.

Take at random one of the test portions prepared in Clause 5.2. Place it in the reduction tube (6.2) and level its surface.

Close the top of the reduction tube. Connect the thermocouple, ensuring that its tip is in the centre of the test portion.

Insert the reduction tube into the furnace (6.3).

Connect the gas supply system (6.5).

Pass a flow of N₂ through the test portion at a rate of 5 L/min and commence heating. When the temperature of the test portion approaches 500 °C increase the flow rate to 20 L/min. Continue heating while maintaining the flow of N₂ until the test portion reaches 500 °C \pm 5 °C. Allow a period of 15 min for temperature equilibration at 500 °C.

DANGER Carbon monoxide and the reducing gas, which contains carbon monoxide, are toxic and therefore hazardous. Testing shall be carried out in a well ventilated area or under a hood. Precautions should be taken for the safety of the operator, in accordance with the safety codes of each country.

Introduce the reducing gas at a flow rate of 20 L/min \pm 1 L/min to replace the N₂. After 60 min of reduction turn off the power. Replace the reducing gas with N₂ at a flow rate of 5 L/min and cool the test portion to a temperature below 100 °C.

8.3 Tumbling

Remove the test portion carefully from the reduction tube. Determine its mass (m_0) and place it in the tumble drum (6.6). Fasten the lid tightly and rotate the drum for a total of 300 revolutions at a rate of 30 rpm \pm 1 rpm.

8.4 Sieving

Remove all material from the drum, determine and record the mass and hand sieve with care on 6,30 mm, 3,15 mm and 500 µm sieves, in accordance with ISO 4701. Determine and record the mass of each fraction retained on the 6,30 mm (m_1), 3,15 mm (m_2) and 500 µm (m_3) sieve. Material lost during tumbling and sieving shall be considered to be part of the - 500 µm fraction.

9 Expression of results

9.1 Calculation of the reduction-disintegration indices ($RDI-1_{+6,3}$, $RDI-1_{-3,15}$, $RDI-1_{-0,5}$)

The reduction-disintegration indices, $RDI-1_{+6,3}$, $RDI-1_{-3,15}$, $RDI-1_{-0,5}$, expressed as percentages by mass, are calculated from the following equations:

$$RDI - I_{+6,3} = \frac{m_1}{m_0} \times 100$$

$$RDI - I_{-3,15} = \frac{m_0 - (m_1 + m_2)}{m_0} \times 100$$

$$RDI - I_{-0,5} = \frac{m_0 - (m_1 + m_2 + m_3)}{m_0} \times 100$$

where

m_0 is the mass, in grams, of the test portion after reduction and before tumbling;

m_1 is the mass, in grams, of the fraction retained on the 6,30 mm sieve;

m_2 is the mass, in grams, of the fraction retained on the 3,15 mm sieve;

m_3 is the mass, in grams, of the fraction retained on the 500 µm sieve.

Record each result to one decimal place.

9.2 Repeatability and acceptance of test results

Follow Annex A, for each of the $RDI-1$ indices, by using the repeatability value given in Table 1. Results shall be reported to one decimal place.

Table 1 — Repeatability (*r*)

Mean value of <i>RDI-1</i> %	<i>r</i> (%, absolute)
0	0
5	1,0
10	2,0
15	3,0
20	4,0
25	4,0
50	4,0
75	4,0
80	4,0
85	3,0
90	2,0
95	1,0
100	0

10 Test Report

The test report shall include the following information:

- a) reference to this part of ISO 4696, i.e. ISO 4696-1;
- b) all details necessary for the identification of the sample;
- c) the name and address of the test laboratory;
- d) the date of the test;
- e) the date of the test report;
- f) the signature of the person responsible for the test;
- g) details of any operation and any test conditions not specified in this part of ISO 4696 or regarded as optional, as well as any incident which may have had an influence on the results;
- h) the reduction-disintegration indices, *RDI-1_{+6,3}*, *RDI-1_{-3,15}*, *RDI-1_{-0,5}*;
- i) the sieving conditions, e.g. the method of sieving and the sieving time;
- j) the total mass of the material inserted into the tumble drum and taken from the tumble drum;
- k) the types of sieves used.

11 Verification

Regular checking of apparatus is essential to assure test result reliability. The frequency of checking is a matter for each laboratory to determine.

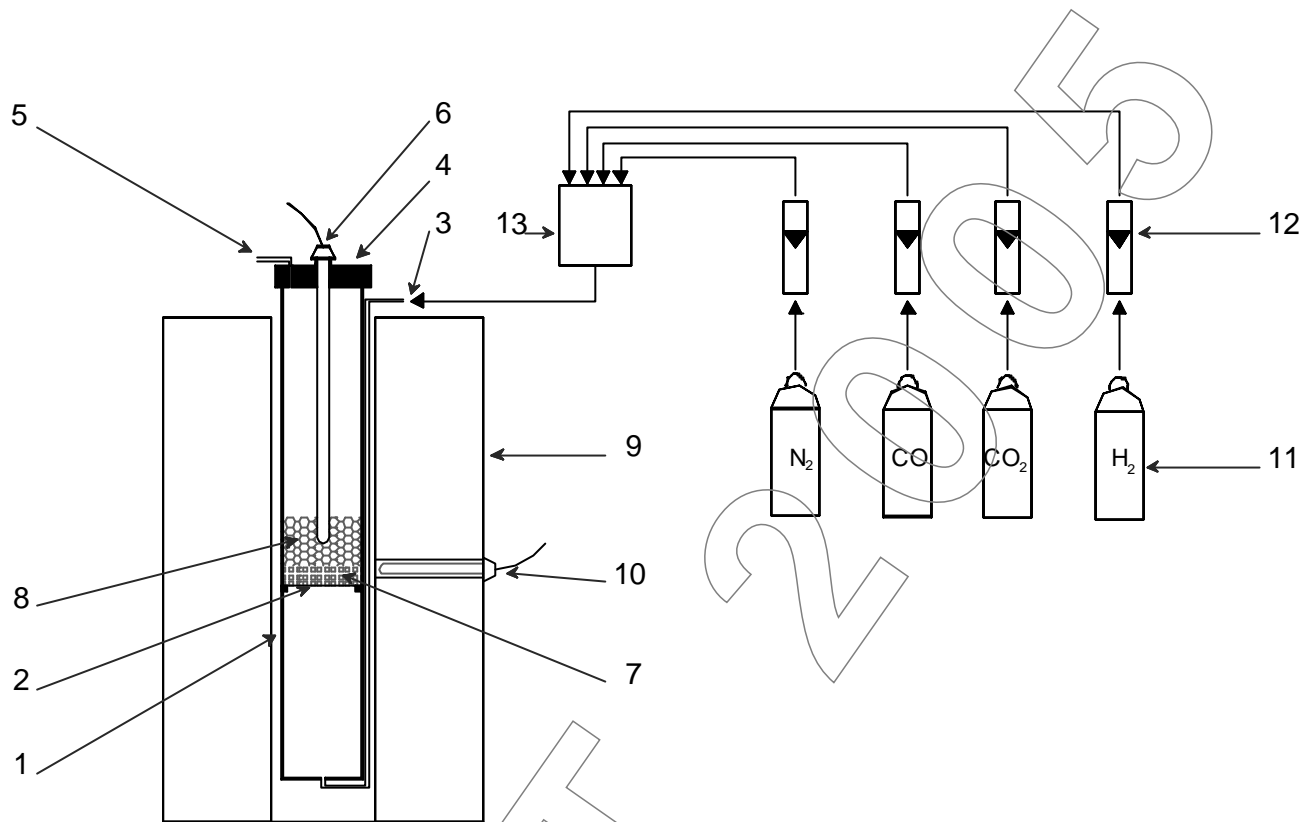
The conditions of the following items shall be checked:

- sieves
- weighing device
- reduction tube
- temperature control and measurement devices
- gas flow meters
- purity of gases
- time control device
- tumble drum
- drum rotation equipment

It is recommended that internal reference material be prepared and used periodically to check test repeatability.

Appropriate records of verification activities shall be maintained.

DRAFT



Key:

Reduction tube

- 1 Reduction tube wall
- 2 Perforated plate
- 3 Gas inlet
- 4 Lid
- 5 Gas outlet
- 6 Thermocouple for measuring the reduction temperature
- 7 Porcelain ball layer
- 8 Test portion

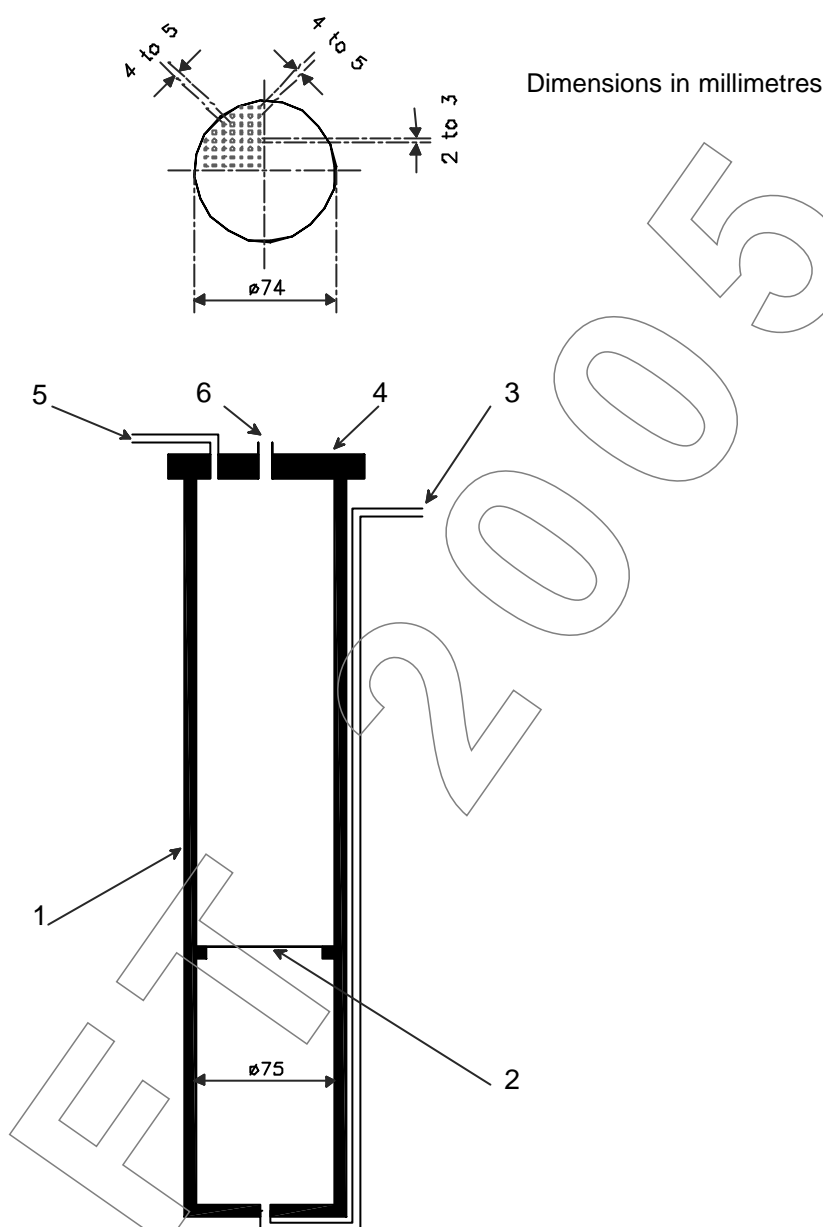
Furnace

- 9 Electrically heated furnace
- 10 Thermocouple for temperature regulation of furnace

Gas supply system

- 11 Gas cylinders
- 12 Gas flowmeters
- 13 Mixing vessel

Figure 1 - Example of test apparatus (schematic diagram)



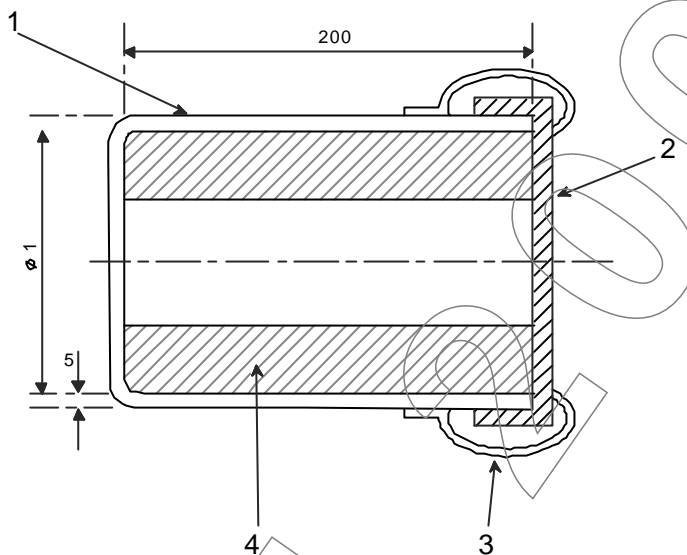
Key:

- 1 Reduction tube wall
- 2 Perforated plate
- 3 Opening for gas inlet
- 4 Lid
- 5 Opening for gas outlet
- 6 Opening for thermocouple insertion

NOTE Dimensions not specified in the apparatus Clause are shown for information only.

Figure 2 - Example of reduction tube (schematic diagram)

Dimensions in millimetres



Key:

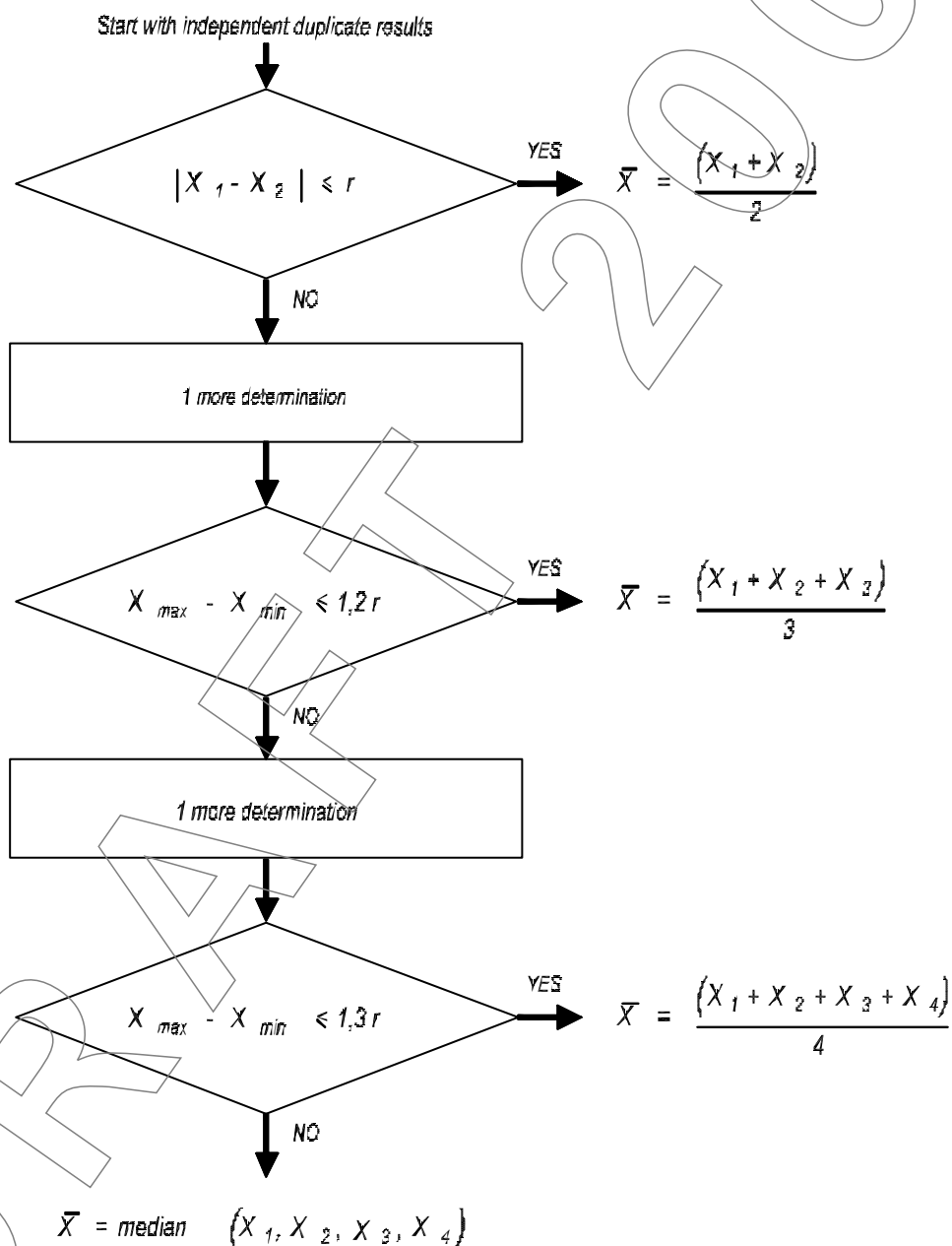
- 1 Vessel
- 2 Lid
- 3 Clamps
- 4 Frame with lifters

Lifters: 20 mm wide by 2 mm thick
Material: plain carbon steel

Figure 3 - Example of RDI tumble drum (schematic diagram)

Annex A (normative)

Flowsheet of the procedure for the acceptance of test results



r. see Table 1

APPENDIX 3

TEST RESULTS

DETERMINATION OF FACTORS INFLUENCING THE DEGREE OF REDUCTION DISINTEGRATION IN NORTHERN CAPE LUMP ORE AND THE ROLE OF GANGUE MINERALS IN THE PROPAGATION OF CRACKS

Test no.	Ore Type	Size fraction	Changes made to ISO 4696	Sieve analysis after testing (%)										
				+20mm	+16mm	+12.5mm	+10mm	+8mm	+6.3mm	+3.15mm	+2mm	+1mm	+0.5mm	- 0.5mm
1	Northern Cape STD	-25+20mm	Size Fraction	46.8	39.28	4.19	1.95	0	0.78	1.33	0.46	0.48	0.58	4.14
2	Northern Cape STD	-20+16mm	Size Fraction		67.74	23.29	1.91	2.37	0.84	1.17	0.66	0.44	0.4	1.17
3	Northern Cape STD	-16+12.5mm	Size Fraction			82.6	11.28	1.58	0.7	1.18	0.56	0.6	0.4	1.08
4	Northern Cape STD	-12.5+10mm	Normal				71.92	16.32	2.62	3.24	1.67	1.53	0.77	1.93
5	Northern Cape STD	-10+8mm	Size Fraction					72.43	12.11	6.73	2.79	2.38	1.29	2.26
6	NORTHERN CAPE OT 1	-12.5+10mm	Normal				64.3	21.4	4.3	3.9	1.6	1.7	0.8	2.1
7	NORTHERN CAPE OT 2	-12.5+10mm	Normal				40.57	28.62	7.71	8.06	3.11	3.67	2.11	6.15
8	NORTHERN CAPE OT 3	-12.5+10mm	Normal				52.1	26.4	8.7	6.2	1.7	1.9	1.3	1.7
9	NORTHERN CAPE OT 4	-12.5+10mm	Normal				81	17.12	0.8	0.42	0.08	0.14	0.14	0.3
10	NORTHERN CAPE OT 5	-12.5+10mm	Normal				58.83	28.41	2.68	4.04	1.6	1.79	0.89	1.77
11	NORTHERN CAPE OT 6	-12.5+10mm	Normal				59.04	14.6	5.93	7.78	3.24	3.75	2.07	3.59
12	NORTHERN CAPE OT 7	-12.5+10mm	Normal				71.3	15.9	3.6	4.3	1.1	1	1	1.8
13	Northern Cape STD	-25+20mm	90 minutes	79.77	15.41	2.57	0	0.44	0.4	0.34	0.1	0.12	0.14	0.7
14	Northern Cape STD	-20+16mm	90 minutes		71.33	8.41	3.81	4.97	1.73	3.45	1.4	1.4	1.16	2.33
15	Northern Cape STD	-16+12.5mm	90 minutes			62.99	16.05	5.68	1.89	3.89	2.42	2.64	1.55	2.88
16	Northern Cape STD	-12.5+10mm	90 minutes				59.64	19.66	4.31	6.24	3.2	2.54	1.67	2.74
17	Northern	-10+8mm	90 minutes					66.12	12.17	9.63	4.01	3.77	1.62	2.68

DETERMINATION OF FACTORS INFLUENCING THE DEGREE OF REDUCTION DISINTEGRATION IN NORTHERN CAPE LUMP ORE AND THE ROLE OF GANGUE MINERALS IN THE PROPAGATION OF CRACKS

	Cape STD													
18	Northern Cape STD	-25+20mm	120 minutes	80.46	8.5	3.21	0.54	1.06	0.44	1.27	0.76	0.88	0.92	1.95
19	Northern Cape STD	-20+16mm	120 minutes		57.86	22.6	1.91	2.21	2.66	3.96	1.95	2.5	1.71	2.64
20	Northern Cape STD	-16+12.5mm	120 minutes			51.17	15.66	7.09	3.54	7.87	4.97	4.85	2.17	2.68
21	Northern Cape STD	-12.5+10mm	120 minutes				57.4	20.8	4.4	6.5	3.1	3.2	2	2.6
22	Northern Cape STD	-10+8mm	120 minutes					54.68	17.2	12.41	5.31	5.09	2.34	2.97
23	Northern Cape STD	-12.5+10mm	550°C				66	17.3	3.4	5.8	2.2	1.9	1.4	2
24	Northern Cape STD	-12.5+10mm	600°C				63.8	18.8	4.5	5.9	1.8	1.9	1.2	2.1
25	Northern Cape STD	-12.5+10mm	650°C				69.1	15.2	3.5	5.2	2	1.9	1.2	1.9
26	Northern Cape STD	-12.5+10mm	700°C				67.7	14.8	4.8	5	2.4	2.1	1.1	2.1
27	Northern Cape STD	-12.5+10mm	5% H2				71.4	17.3	2.3	3.2	0.9	1.5	0.9	2.5
28	Northern Cape STD	-12.5+10mm	10% H2				66.2	17	3.9	5.1	2.3	2	1.5	2
29	Northern Cape STD	-12.5+10mm	600°C 90 min				64.6	16.72	5.13	5.03	2.66	2.51	1.22	2.13
30	Northern Cape STD	-12.5+10mm	600°C 120 min				56	11.7	8.6	10.3	4.3	4.3	1.9	2.9
31	Northern Cape STD	-12.5+10mm	700°C 90 min				64.1	16.5	7.8	4.7	2.1	1.8	1.2	1.8
32	Northern Cape STD	-12.5+10mm	700°C 120 min				57.5	16.8	6.5	8.9	3.7	3.1	1.4	2.1
33	Northern Cape STD	-12.5+10mm	750°C 60 min				76.3	12.5	3.2	3.3	1.4	1.2	0.6	1.5
34	Northern Cape STD	-12.5+10mm	800°C 60 min				83.1	8.5	3.1	1.8	0.6	0.5	0.3	2.1

