

# UNIVERSITEIT VAN PRETORIA UNIVERSITY OF PRETORIA YUNIBESITHI YA PRETORIA

**APPENDICES** 



APPENDIX A. MEASUREMENT SYSTE 💋

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# **APPENDIX A – MEASUREMENT SYSTEM AND CALIBRATION**

# 1. MEASUREMENT SYSTEM

Equipment	Description	Serial Number
Signal generator	DSPT Siglab SN 11251	
& analyser	Model 20-42	
Signal amplifiers	Rotel stereo integrated	SN 522 45811
	amplifiers RA-970 BX	SN 434 75550
Shakers	Vibro Pet Model Pet-01	SN 40-381-2
	IMV Corp.	SN 40-376-2
Condition amplifiers	Model 480E09 ICP	SN 17185
	Power Unit	SN 3657
		SN 3435
		SN 17187
Force transducers	PCB208 B02	SN 12980
		SN 12742
Shear accelerometers	PCB U353 B65	SN 20520
	PCB U353 B66	SN 44564
	PCB B15	SN 50276
Piezoelectric strain gauges	PCB 740 B02	SN 823
	PCB 740 B02	SN 857
РС	Pentium 100 MHz	SN 0467570
	"Apollo"	

Table A.1 – Measurement system for the identification of a single harmonic force

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### 2. CALIBRATION FACTORS

#### 2.1 Accelerometer/Force Transducer Pair

Alternating voltage signals were measured from both the accelerometer and force transducers. These signals had to be multiplied by a calibration factor to obtain the correct magnitude of the frequency response functions. Since the frequency response function is simply the ratio of the response to the force, a straightforward technique can be applied to determine the calibration factor for each pair of accelerometer/force transducer. The force transducer and accelerometer are attached to the rigid body of known mass (m = 4.02 kg), as depicted in Figure A.1.



Figure A.1 – Calibration measurement setup

A time-varying force is applied to a rigid body for which the inertance is measured for the specified frequency range. The measured quantity has units of volt/volt and corresponds to:

$$A(\omega) = \frac{\ddot{x}(t)}{f(t)} = \frac{1}{m}$$
(A.1)

from which the overall sensitivity for each pair of accelerometer/transducer can be calculated. Figure A.2 illustrates a typical inertance and coherence measurement for one of the pairs of accelerometer/force transducer used in the experimental measurements. The overall sensitivities are listed in Table A.1.



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Accelerometer/	Overall Sensitivity	
force transducer pair	$\left[\frac{V/V}{m.s^{-2}/N}\right]$	
SN 44564 & SN 12742	1.1610	
SN 20520 & SN 12742	1.2746	
SN 44564 & SN 12980	1.1584	
SN 20520 & SN 12980	1.2933	
SN 50276 & SN 12980	9.9367	

Table A.1 -	Calibration	of acceler	ometer/force	transducer	pair
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Figure A.2 – Inertance and coherence plots for the calibration of an accelerometer/force transducer pair

# 2.2 Accelerometers

The accelerometers were calibrated separately with a hand-held calibrator. This calibration was done with the accelerometers still connected to the rest of the measurements system as used in experimental setup. The calibration factors for each of the accelerometers are listed in Table A.2.

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Accelerometer	Calibration factor		
	$\left[\frac{m.s^{-2}}{Vrms}\right]$		
SN 44564	154.841		
SN 20520	172.358		
SN 50276	1261.221		

### 2.3 Force Transducers

Having determined the calibration factors for the accelerometers, the calibration factor for each of the force transducers was deduced from the overall sensitivity ratios given in Section 2.1 of this appendix. Two values were obtained for each force transducer, of which the average was used in the force identification process. These calibration values are given in Table A.3.

Table A.3 – Calibration of force transducers

Calibration factor
$\left[\frac{N}{Vrms}\right]$
134.297
133.472

## 2.4 Piezoelectric Strain Gauges

The manufacturer's quoted sensitivities were used to determine the calibration factor for the piezoelectric strain gauges and are given in Table A.4.

 Table A.4 – Calibration of piezoelectric strain gauges

Piezoelectric	Calibration factor
Strain Gauges	$\left[\frac{\mu\varepsilon}{Vrms}\right]$
SN 823	24.595
SN 857	28.3409

APPENDIX B. MODAL ANALYSIS OF F.



# **APPENDIX B - MODAL ANALYSIS OF FREE-FREE BEAM**

Number of averaged Procedures: 100

The identified natural frequencies, modal damping factors and normal modes are listed in Tables B.1 and B.2.

Table B.1 - Natural frequencies and modal damping factors for the free-free beam

Natural frequencies	Modal damping factors
[Hz]	× [10 <sup>-4</sup> ]
32.538	29.313
88.471	7.6010
172.76	17.404
286.01	6.8997
426.03	4.7836

Table	B, 2 -	Identified	l normal	modes	for the	: free-free	beam
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Position	Mode 1	Mode 2	Mode 3	Mode 4	Mode 5
	<b>x</b> [10 <sup>-1</sup> ]	<b>x</b> [10 <sup>-1</sup> ]	x [10 <sup>-1</sup> ]	x [10 <sup>-1</sup> ]	<b>x</b> [10 <sup>-1</sup> ]
1	7.1528	-7.1878	7.2027	-5.7285	4.7910
2	4.0191	-1.5927	-0.4212	2.1804	-3.6031
3	0.7958	2.7162	-5.0597	4.4827	-2.1790
4	-1.8826	4.9710	-2.9900	-1.6166	4.8615
5	-3.7555	3.4185	2.4462	-5.0856	0.8848
6	-4.3651	0.0434	5.2002	-0.0889	-5.1665
7	-3.7685	-3.1402	2.5276	4.9914	0.6129
8	-1.9486	-4.8481	-2.8685	1.7411	5.1903
9	0.6817	-2.6716	-4.6202	-4.4145	-2.0095
10	3.7753	1.3380	-0.5484	-2.2280	-3.6572
11	7.0687	6.8776	6.4475	6.4463	6.1806

The following figures show the measured frequency response function data and the reconstructed normal mode model obtained after optimisation for the reference position 11. The truncated modes are accounted for by the inclusion of the residual terms in the normal mode model. It can be seen that the normal mode model corresponds fairly well to the experimentally measured data. At the high frequencies the normal mode model deviates slightly from the measured data due to the residuals of the truncated modes.

#### Position 1 10<sup>4</sup> Inertance [ms<sup>-2</sup>/N] 10<sup>2</sup> $10^{0}$ Data Nor. model 10<sup>-2</sup> 50 150 200 100 250 300 400 450 500 350 Frequency [Hz]

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APPENDIX B. MODAL ANALYSIS OF F.

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# Position 9

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