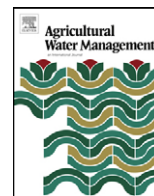




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Rainfall simulation to identify the storm-scale mechanisms of gully bank retreat

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ABSTRACT

Gully erosion is one of the main causes of soil loss in drylands. Understanding the dominant mechanisms of erosion is important to achieve effective erosion control, thus in this study our main objective was to quantify the mechanisms involved in gully bank retreat as a result of three processes, falling of entire soil aggregates, transport of soil material by splash and by water running along gully banks (runoff), during rainfall events. The study was conducted in the sloping lands of the KwaZulu-Natal province, a region that is highly affected by gully erosion. Artificial rain was applied at 60 mm h^{-1} for 45 min at the vertical wall of a gully bank typical to the area. The splash material was collected by using a network of 0.045 m^2 buckets. The sediments in the running water were assessed by sampling the runoff collected from a microplot inserted within the base of the bank, and collecting the fallen aggregates after the rainfall simulation was complete. Results indicated that the overall erosion for the simulation was $721 \text{ g m}^{-2} \text{ h}^{-1}$. Runoff erosion proved to be the dominant mechanism and amounted to $450 \text{ g m}^{-2} \text{ h}^{-1}$, followed by splash and fall down of aggregates (about $170 \text{ g m}^{-2} \text{ h}^{-1}$). Gully bank retreat occurred at a rate of 0.55 mm h^{-1} and assuming that the soil bulk density is 1.3 g cm^{-3} , this corresponds to a retreat of 8.8 mm y^{-1} . Extrapolations to the watershed level, where about 500 m^2 of gully bank are observed per hectare, would lead to an erosion rate of $4.8 \text{ t ha}^{-1} \text{ y}^{-1}$. These limited results based on a simulated storm show that the three main mechanisms (runoff, splash and fall down of aggregates) are responsible for the retreat of gully banks and that to mitigate gully erosion, appropriate measures are required to control all three mechanisms. Further research studies are needed to confirm and to scale up, both in time and space, as these data are obtained at one location and from a single artificial storm.

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1. Introduction

The issue of soil erosion is fast becoming a severe challenge to food supply, food security, human health, natural ecosystems as well as to the economic development of countries. Erosion leads to irreversible damage of cropping systems by removing fertile horizons of soils and reducing the water holding capacity and all the associated ecological functions (Lal, 1998). Linear erosion, which is defined as erosion due to the concentrated and channelized runoff and includes gully and ephemeral gully erosion, is also responsible for off-site consequences such as debris flow

or the silting up of valley bottoms and reservoirs (Poesen et al., 1996).

In inter-tropical and tropical areas, linear erosion is considered to be one the main contributors to soil degradation and the sediment loads from river basins (IGBP, 1995). The literature shows that gullies account for most soil erosion (e.g., Poesen et al., 2002). For instance, in the tropical regions of southern China, linear erosion contributed up to 85% of sediment load from a 0.73 km^2 catchment (DiCenzo and Luk, 1997).

On- and off-site effects of linear erosion may jeopardize the future of natural ecosystems and the economic development of societies. Consequently, better understanding of the mechanisms of linear erosion has become an important issue, because understanding linear erosion mechanisms and their controlling factors is fundamental to the identification of pos-

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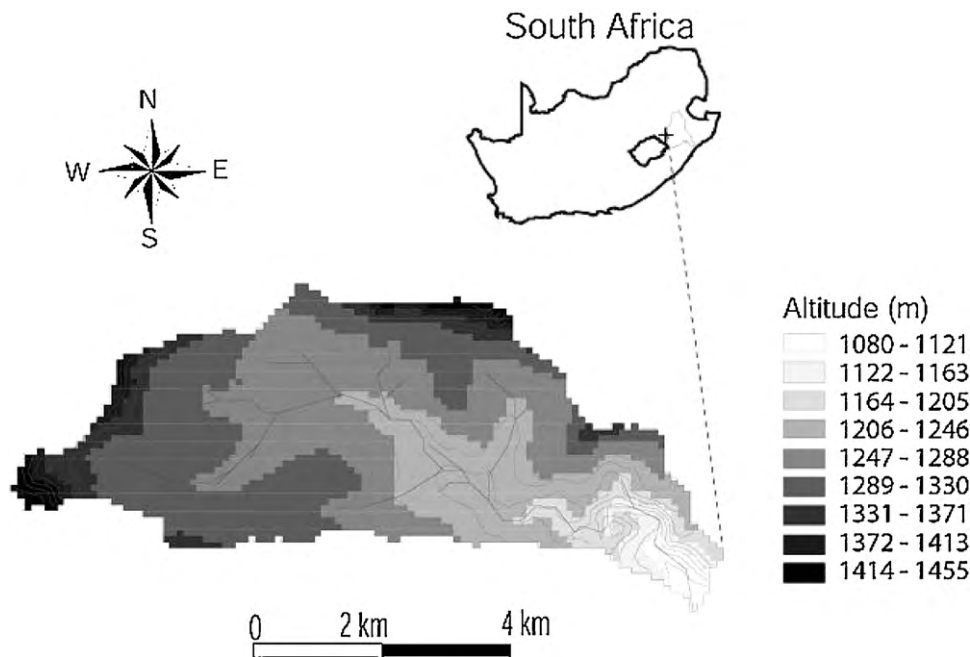


Fig. 1. Location of the study area in South Africa.

sible solutions to environmental issues associated with linear erosion.

Attempts at evaluating linear erosion mechanisms have been made over several years (Moore et al., 1994; Montgomery and Dietrich, 1994; Poesen et al., 1996; Nachtergaele et al., 2001) and mechanisms such as erosion due to concentrated surface flow or piping have been identified so far. However, once formed, erosion resulting from the lateral retreat of gully banks has shown to be the main source of the sediment exported from river basins and a main factor of control of gully evolution in landscapes (Vandekerckhove et al., 2001; Hu et al., 2007). Estimations made by Vandekerckhove et al. (2001) at 46 active bank gullies, of the Guadalentin and the Guadix basin in south east Spain, showed that the linear headcut retreat contributed to less than 10% of the total gully erosion. Most of the gully erosion thus occurs along the gully, via the lateral retreat of gully banks.

Despite such significant evidence, the mechanisms involved in the lateral retreat of gully banks are not quantified. Vandekerckhove et al. (2001) found that runoff has a positive correlation to linear headcut retreat, and therefore no impact on the lateral retreat of gully banks. Mechanisms, other than those linked to runoff, may control such a retreat, however little is known about them (Poesen et al., 2002). In order to mitigate gully bank retreat, there is a need to identify the erosion mechanisms involved during a rainstorm, especially those associated with raindrops. The mechanisms include detachment and transport of particles as a result of splash and the fall down of entire soil aggregates.

This study was performed within the steep slopes of the KwaZulu-Natal province of South Africa, a region highly affected by gully erosion (Martin, 1987; Beckedahl, 1996). Linear erosion rates in this region are significantly higher than the natural soil pedogenesis (Martin, 1987) and thus represent a major threat to the non-renewable soil resource and its numerous associated ecological services linked to food production, water storage, and biodiversity. Deep incisions, locally named 'dongas', are shown to be mainly associated with the presence of certain parent materials (Weaver and van, 1991), such as unconsolidated colluvions which erode easily (Wintle et al., 1995), and are generally associated with high sodium contents (Yaalon, 1987). Moreover, from the literature

it appears that in this region, gully bank retreat is more prominent compared to the retreat of gully head cuts (Martin, 1987), thus placing greater emphasis on the retreat of gully banks.

Nowadays, linear erosion may accelerate due to land use changes and/or misuses (Lal, 1998), as has occurred in this region, and result in decreased soil infiltration and increased runoff (Le Roux et al., 2007; Dlamini et al., this issue). Despite numerous studies on linear erosion, gully or donga systems, there is still a need for remediation techniques and a better understanding of the mechanisms and processes of their formation and evolution. In a recent study, Rienks et al. (2000) revealed (using an erodibility test) that the silt and sodium contents of the parent material have a great effect on soil erodibility, suggesting that dispersion plays an important role in linear erosion. Furthermore, little is known about the other mechanisms of gully evolution such as detachment and transport of soil particles due to raindrop impact and fall down of entire soil aggregates as a result of rainstorm events.

In this study, our main objective was to quantify the contribution of splash detachment, sediment transport by runoff and fall down of entire soil aggregates to overall erosion by rainfall from a gully bank. Erosion mechanisms are difficult to investigate and control during natural rainfall events, therefore rainfall simulation was used to reach the desired objectives. Rainfall was simulated for 45 min, at a typical gully bank, and the erosion rate of the three mechanisms described was evaluated.

The study was conducted at the South African site of the Smallholder System Innovations (SSI) project which focuses on improved management of soil and water resources for small holder farmers livelihoods whose are strongly affected by the degradation of the soil resource.

2. Materials and methods

2.1. The characteristics of the study site

The study area is located in KwaZulu-Natal, South Africa (Fig. 1) in a 10 km² watershed situated in the northern sloping lands of the Thukela basin (30 000 km²). The site (22° 19' 15" 3S; 22° 49' 52" 8E) is situated in a sub-tropical, semi-humid climate with summer rain-



Fig. 2. Typical gully incision of the Potshini area. Note the presence of fresh gully banks is the disconnection between the water pathway of the central gully and the banks.

fall (October–March). At Bergville, located 10 km to the east, the mean annual precipitation over the last 30 years has been 684 mm, with a potential evaporation of 1600 mm and a mean annual temperature of 13 °C (Schulze, 1997). Altitudes range between 1080 and 1455 m. The relief is relatively smooth with a mean slope gradient of about 15%. Steep slopes on the upper watershed may however reach gradients of 50–70%, while flat areas may be observed downstream. Cattle constitute the second most important part of the Zulu smallholders' livelihood, and because it is also an important cultural asset, the number of cattle has increased. This, combined with highly acidic soils of low productivity (Table 1), leads to rapid overgrazing with dramatic consequences on soil degradation (Fey, 2003; Dlamini et al., *this issue*) and especially gully erosion (Botha et al., 1994). At the study site the density of gully banks is approximately 500 m² ha⁻¹ (Dlamini et al., *this issue*) (Fig. 2).

The gully of interest for this study is situated on the northern upper limit of the catchment. The selected bank was 30 m downslope of the gully head cut. A representative 1 m wide zone was selected in an area accessible from the road and with a flat bottom in order to facilitate the experiment. The gully bank that was 10 m away from the gully center is a typical Luvisol (WRB, 1998) characterized by a thick Fragic horizon. The surface 0–0.1 m horizon is brown (10YR 4/3), very coherent and has a medium, subangular, blocky structure. It is a sandy silt horizon with many roots. The horizon directly below (0.1–0.2 m) is an organo-mineral, sandy silt, that is coherent, yellowish brown horizon (10YR 5/4) with a clear medium, subangular, blocky structure. A mineral Fragic horizon, 1 m thick, lies below this. It is a yellowish brown (5YR 5/4), sandy clay, that is slightly coherent and exhibits a massive to columnar structure. The transition to the underlying horizon is sharp. It is a light grey, sandy silt with a massive structure.

2.2. The evaluation of the different mechanisms of erosion induced by rainfall

Rainfall was simulated on 20 November 2008 to evaluate the potential gully bank retreat resulting from rainfall erosion. This date

followed a dry period of about six months and the soil horizons were all dry.

The gully bank was covered with plastic sheeting, except for a 1 m wide portion which remained exposed. Rainfall intensity was applied to the exposed portion at a rate of 60 mm h⁻¹ for 45 min, simulating a typical rainfall event of the region (Schulze, 1997). The rainfall was produced using an ORSTOM simulator (Valentin, 1978). The simulator comprised an oscillating nozzle (Teejet SS 6560) which was aligned with the center of the exposed portion of the vertical bank, approximately 4 m above the soil surface. A valve and a pressure gauge were located at the same altitude as the nozzle, allowing for precise control of water pressure and consequently the maintenance of a consistent rain kinetic energy. At a water pressure of 40 kPa the estimated kinetic energy was 25 J m⁻² mm⁻¹.

The rainfall intensity was set and controlled electronically prior to the experiment. Error for rainfall intensity was assumed to be less than 5%.

The vertical runoff, along with its sediments was evaluated using a 1 m² microplot inserted within the base of the bank (Fig. 3) during the rainfall period. The sampling protocol involved sampling the initial runoff in three consecutive 500 ml bottles. The proceeding 500 ml aliquots were collected every 5 min to the 20th minute and every 5 min to the end of the experiment. These bottles were then labelled and the time taken to fill them recorded. The splash material was collected using twelve rectangular 0.27 m × 0.17 m (0.045 m²) buckets, positioned at the node of a regular grid of 0.5 m increments. The minimum distance from the source (i.e., the gully bank) was 0.5 m and the maximum was 1.5 m. Finally, fallen soil aggregates were gathered from the 1 m² microplot after the simulation had stopped.

The 500 ml aliquots of runoff water were dried at 105 °C to evaluate the sediment concentration in the runoff. The runoff fluxes were estimated over time by using the filling duration of bottles. Total sediment lost during a bottle filling period corresponded to the product of the sediment concentration in that bottle and its runoff volume. Data were then integrated over the duration of the rainfall to calculate the total soil loss as a result of runoff. Sediments

Table 1
Main chemical and physical properties of the studied profiles.

Hz	Depth cm	pH H ₂ O	pH KCl	BD (g cm ⁻³)	H ₂ O 105 °C (%)	Ca (cmol ⁽⁺⁾ kg ⁻¹)	Mg (cmol ⁽⁺⁾ kg ⁻¹)	K (cmol ⁽⁺⁾ kg ⁻¹)	Na (cmol ⁽⁺⁾ kg ⁻¹)	S (cmol ⁽⁺⁾ kg ⁻¹)	ECEC (cmol ⁽⁺⁾ kg ⁻¹)	Clay (%)	Silt (%)	Sand (%)
A1	0–10	4.7	4.3	1.34	3.5	2.32	1.38	0.24	0.10	4.04	3.56	16.4	16.8	66.8
A2	10–30	5.1	4.3	1.32	3.1	1.50	1.32	0.14	0.10	3.06	3.62	18.2	16.1	65.7
Bw1	30–60	5.3	4.3	1.36	5.2	1.44	1.28	0.08	0.10	2.91	3.52	17.4	16.5	66.1
Bw2	60–95	5.6	4.1	1.36	4.6	3.08	3.29	0.23	0.19	6.79	6.36	32.6	18.8	48.6
Bxg	95–185	5.7	4.5	1.55	3.8	1.88	2.37	0.14	0.16	4.55	6.62	32.9	17.9	49.2
Bwg	185–210+	6.4	4.9			3.48	2.80	0.16	0.17	6.61	6.14	21.9	16.5	61.6



Fig. 3. Rainfall simulation along a 1 m width and 2.3 m in height. Position of some of the twelve 0.27 m × 0.17 m buckets for splash collection and of the microplot to gather both the vertical runoff and the entire soil aggregates falling down the bank. Picture taken 6 min after the beginning of a 45 min and 60 mm h⁻¹ intensity artificial rainfall with the sprinkler for rainfall simulation located at the vertical of the bank.

resulting from the splash and fallen aggregates were dried at 105 °C and the dry weight was recorded. The overall splash erosion corresponded to the average erosion in each bucket (in kg m²) multiplied by the surface of the sampling grid, i.e. 4 m² (2 m × 2 m).

Finally, the erosion from the three mechanisms was added to evaluate the total erosion induced by the rainfall.

3. Results

3.1. The evolution of the wetting front within the soil profile of the gully bank

Fig. 3 is a picture of the gully bank 6 min after the beginning of the rainfall simulation. The different horizons are easily distinguished: an organo-mineral A horizon above a Bw horizon and a Bxg frigid horizon that juts out and a Bwg mineral horizon at the bottom, which is set back due to reduced cohesion of soil particles. It is interesting to note that after 6 min of rainfall, with a sprinkler located at the vertical of the prominent horizon of the gully bank, the A, Bw horizons are wet, whereas the underlying Bwg horizon is still dry because it is protected by the Bxg horizon. Closer inspection of Fig. 3 reveals that the wetting front entered the horizon as vertical tongues that form within the basis of the gully bank. These are initiated at the base of the depressions between the Bxg columns that collect and drive the vertical runoff that comes from the upper part of the bank profile. Only the surface A horizon was wet after the first minute of rainfall. After the fifth minute, the rain had almost completely wet the Bxg horizon, this was followed by vertical runoff reaching the base of the gully bank. After approximately 10 min runoff reached the runoff collector. At the end of

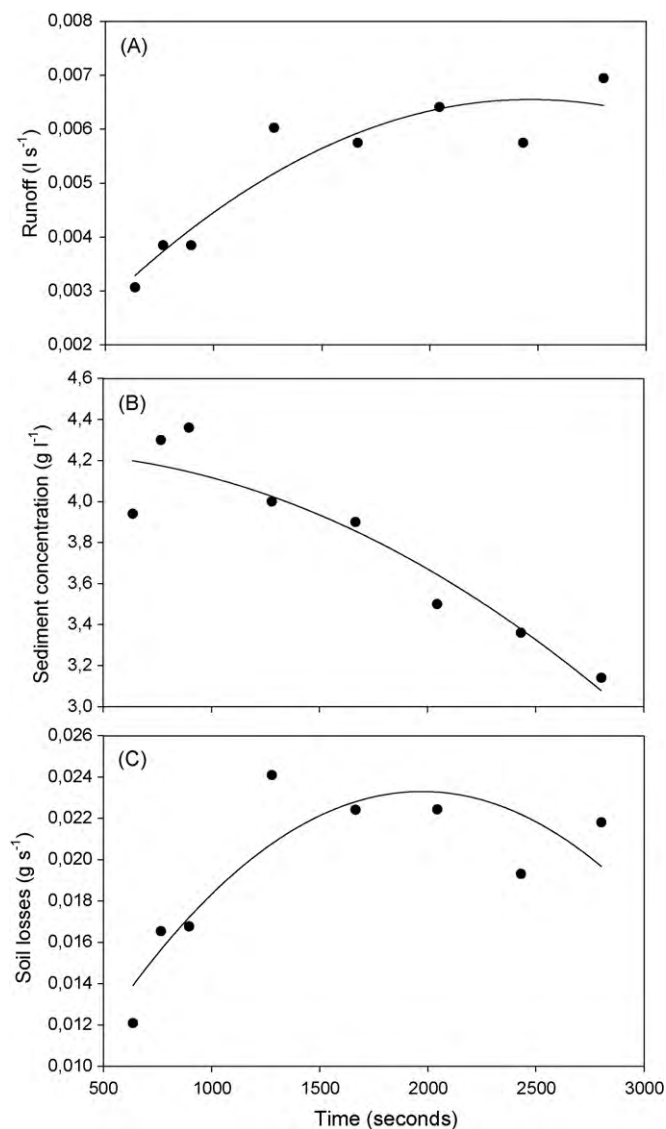


Fig. 4. Evolution over time of runoff, sediment concentration and sediment losses from the vertical runoff and during the 45 min and 60 mm h⁻¹ artificial rainfall. Ajustement of data point by using quadratic functions.

the rainfall event, three main runoff pathways had crossed on the underlying horizon, and the rest of the surface remained dry.

3.2. Vertical runoff (R) and its sediment concentration (SC)

The cumulative runoff collected at the base of the gully bank was 14.05 l. The runoff fluxes varied between 3×10^{-3} and 7×10^{-3} l s⁻¹. Runoff rate showed a sharp increase from the initiation of runoff to the 20th minute of rainfall, after which runoff rate increased more gradually (Fig. 4A). The average sediment concentration in the runoff was 3.8 g l⁻¹ and values varied between 3.1 and 4.4 g l⁻¹ (Fig. 4B). Despite a sharp increase during the first minutes of runoff, sediment concentration significantly decreased over time.

As expected from the evolution of R and SC over time, the computed soil losses showed a sharp increase from 0.012 g s⁻¹ to about 0.024 g s⁻¹ at 25 min of rainfall and a slight decrease to the end of the rainfall event (Fig. 4C). As a result, the computed soil lost during the artificial rainfall of 45 min was 723 g, which corresponded to an erosion rate of 450 g m⁻² h⁻¹ (Fig. 5). This erosion rate seems relatively low but when extrapolated to about 500 m² of bank observed

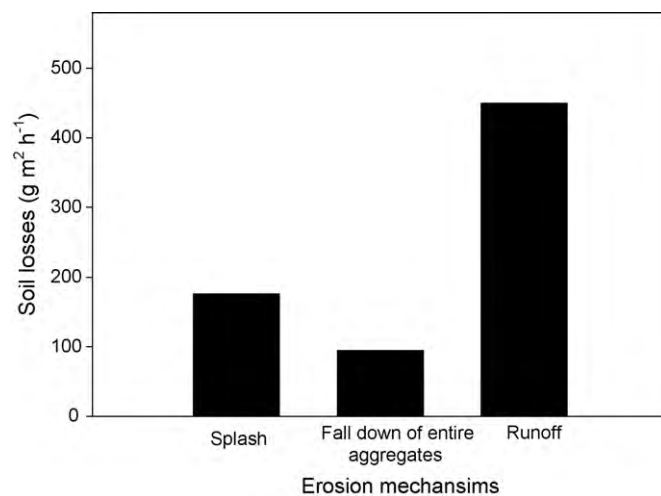


Fig. 5. Cumulative soil erosion for the different erosion mechanisms.

per hectare, it would correspond to an erosion rate of 4.5 t h⁻¹ which already represents high amounts.

3.3. Splash erosion and fall down of entire soil aggregates

As shown in Fig. 3, splash erosion seemed to only occur on the A and Bw and the top of Bxg horizons, the only horizons wet by raindrops. The average value of sediment erosion caused by splash, calculated from the 10 buckets, was 76 g m⁻². The CV of splash deposition rate was very high (160%), reflecting values between 4.1 and 419 g m⁻² (corresponding to 5.5 and 557 g m⁻² h⁻¹, respectively). The rate of deposition of soil particles did not occur randomly, but as expected decreased sharply with distance from the gully bank. The average deposition rate was 258 g m⁻² h⁻¹ at 0.5 m from the bank, which decreased to 37 g m⁻² h⁻¹ at 1 m and to 8.3 g m⁻² h⁻¹ at 1.5 m. As a result, the computed sedimentation, due to splash, on the 4 m² area where splash deposition was shown to occur, was 405 g h⁻¹ corresponding to 176 g m⁻² h⁻¹ per m² of gully bank. Finally, a 164 g aggregate detached from the gully bank during the course of the experiment and resulted in an overall erosion rate of 94 g m⁻² h⁻¹ (Fig. 5).

Overall, the erosion rate computed from runoff, splash and erosion due to fall down of entire soil aggregates was 721 g m⁻² h⁻¹.

4. Discussion

4.1. Overall erosion of gully banks

The overall erosion rate calculated from runoff, splash and erosion due to fall down of entire soil aggregates was 721 g m⁻² h⁻¹. Extrapolated to the annual rainfall of 800 mm (Schulze, 1997), with the assumption of similar impact to the simulated rainfall, the total erosion might reach 9.6 kg m⁻² y⁻¹. Such an amount corresponds to an annual average bank retreat of about 7 mm for an average soil bulk density of 1.35 g cm⁻³.

Given that about 500 m² of bank is present per ha at the watershed level, extrapolation of soil losses would lead to 4.8 t ha y⁻¹. This rate of gully bank retreat is slightly higher than that observed in Kenya (3 t ha y⁻¹, Oostwoud Wijdenes and Bryan, 2001), and in catchments under sloping land conditions in Northern Laos, as described by Chaplot et al. (2005), which have rates of between 0.1 and 2.4 t ha y⁻¹. Gully erosion at our site was significantly lower than rates measured under temperate or Mediterranean conditions (Govers and Poesen, 1988) for Belgium at 22 t ha y⁻¹, and Casali et al. (2003) and Poesen et al., 2002 (between 38 and 65 t ha y⁻¹).

Lower erosion rates in northern Laos may be explained by a high structural stability provided by high clay and organic matter contents (Chaplot et al., 2007) while in our study the cohesion of the B_{tg} horizon buffer the local erosion rate compare to the values measured under temperate and Mediterranean conditions.

Soil erosion due to gully bank retreat should be considered with respect to the other forms of erosion within the area. Since the area is under pasture with no artificial perturbation, erosion by tillage is assumed to be near zero. Estimations of interrill erosion (Kinnell, 2001) at the same site revealed great amounts of soil are removed due to splash and shallow runoff. Dlamini et al. (this issue) calculated the average interrill erosion rate to be 7.7 t ha⁻¹, by using fifteen 1 m² microplots installed within the catchment, in between gullies.

4.2. The different mechanisms of gully bank retreat during the rain

From our investigations, runoff (62% of total soil loss) contributed the most to the overall erosion rate followed by splash erosion (24%) and fall down of aggregates (13%).

Sediment transport due to runoff sharply increased during the first minutes of the artificial rainfall and significantly decreased afterwards. The first increase in sediment concentration (SC) may be explained by the fact that on very dry soil (less than 5% of moisture) with exposed flank to soil evaporation, sediment detachment and transport need a certain time to be effective. From the soil detachment point of view, the different disaggregation mechanisms (slaking, mechanical breakdown and chemical dissolution) require the wetting front to penetrate the soil aggregates deeply (Le Bissonnais, 1996). Runoff must reach a certain velocity to transport this material (Chaplot and Le Bissonnais, 2003). The decrease of SC over time might be explained by a dilution effect, i.e. the sediment detachment is diluted in a greater runoff volume, and/or by the fact that disaggregation mechanisms are very effective on a dry soil and when the easily detachable material is exported the remaining aggregates are less erodible.

Overall, greater erosion by runoff than by splash may be explained by the fact that sediment detached by splash is more easily transported by runoff than by splash itself (Kinnell, 2001). It is important to note that at the first stage of the simulation, when the soil surface at the bank was still dry, splash erosion and transport was the only operative mechanisms of gully bank retreat.

Such results show that other than dispersion (which has been proven to play an important role in linear erosion), mechanical disaggregation is another important mechanism that favors gully erosion and occurs under conditions where sodium content is high (Rienks et al., 2000). Such results seem to show the great impact that splash that plays on disaggregation by slaking, mechanical breakdown or chemical dispersion.

It is surprising that fall down of entire soil aggregates was listed third on the list of erosion mechanisms, especially considering the large amount of aggregates generally found in the vicinities of banks that have fallen down as individuals or as massive “landslides” of several m³. The question thus arises: how is it possible that the fall down of aggregates only contributes to 13% of our total soil losses? One possible explanation is probably due to the time frame used for the study. Where splash is active at the rainfall event only, fall down of blocks may occur either during or between rainfall events, due to swelling and shrinking as a result of wetting and drying of the soil. For this reason this process is likely to have been underestimated. Longer periods of observation as well as longer portions of gully banks would need to be considered to assess the hazardous behavior of aggregate fall down and the exact timing of the collapse of entire portions of gully bank, that produce very large amounts of sediments which may be eroded and be transported by splash

and runoff. The second possible explanation is that the soil type is highly impacting the bank retreat process. Soils derived from sandstone and colluviums show a low aggregation. On dolerite, surface morphologic features appear completely different with a very clear stable fine structure very prone to detachment. Further comparative research studies are therefore necessary.

5. Conclusion

In this study our main objective was to identify the storm-scale mechanisms of gully bank retreat and this was investigated by collecting soil erosion resulting from runoff, splash transport and fall down of soil aggregates, during an artificial rainfall event.

Two main conclusions could be drawn from this study:

1. The retreat of gully banks is confirmed to be a main process in overall gully evolution and overall erosion in landscapes.
2. Soil erosion due to raindrops and runoff is very active mechanism of gully bank retreat. Runoff contributed to about 90% of total exports. Fall down of entire aggregates proved to be the least significant on that type of soil.

Considering splash is an important factor of bank retreat at the rainfall event level, remediation of gully evolution might be obtained through an improved protection of the surface of gully banks from raindrops by increasing for instance soil surface coverage by vegetation (e.g., Morgan, 2004).

However, further research studies, that investigate the erosion mechanisms for longer periods and on larger areas, need to be performed to gather more data for a single storm event, and to emphasize the hazardous behavior of the fall down of soil aggregates or landsliding of gully banks.

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