

Dynamic response of biofilm to pipe surface and fluid velocity

T.E. Cloete, D. Westaard and S.J. van Vuuren

Introduction

Numerous research efforts have focused on the development of biofilms (Costerton *et al.*, 1995; Cloete, *et al.*, 1998). MIC is caused by the presence of bacteria in water systems, especially by bacterial biofilms and to prevent this, such bacterial biofilms must be removed. Five mitigation approaches are currently followed: (i) bacteria are chemically killed by application of bactericidal compounds, termed biocides, at lethal doses, (ii) biofilms are dispersed by dispersants, (iii) biofilms are removed physically by a variety of processes, (iv) the biofilm structure is weakened by enzymes or chelants, and (v) planktonic bacterial numbers are controlled by ultraviolet light (Cloete *et al.*, 1998).

However, in order to be more effective in the control of biofouling, it is also very important to identify the growth conditions that are less favorable for microbial activity and biofilm formation. Biofilms are subjected to fluid shear effects, including detachment caused by flowing water (Lawrence *et al.*, 1995; Vieira *et al.*, 1993). Detachment was classified into four categories by Bryers, (1988) i.e. erosion; sloughing; abrasion and grazing. Trulear and Characklis (1982) found that detachment increases with fluid velocity and mass of biofilm. When the shear stress decreased, it had no effect on detachment. Peyton (1996) studied erosion and concluded that detachment is not affected by the shear stress. Understanding the dynamic response of biofilms to various flow velocities could lead to a better understanding of how flow velocity influences the growth and adhesion of the biofilm and whether it is possible to decrease biofilm formation and/or increase detachment, by manipulating flow velocities.

The main objective of this study was therefore to monitor biofilm development and to study the effect of fluid velocity on biofilm formation on different piping materials used in potable water distribution systems.

Materials and methods

Evaluation of fluid velocity on biofilm formation

To test the effect of velocity on the growth of biofilm, a Roto-Scope was designed and built to imitate the flow conditions in potable water distribution systems. Two sets of pipe sections were made in order to test more than one velocity during the test period.

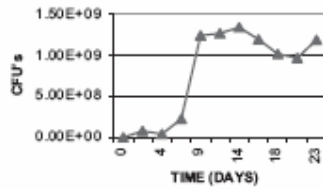


Figure 1 Biofilm growth on asbestos cement

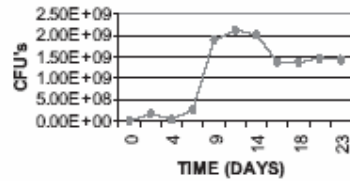


Figure 2 Biofilm growth on PVC

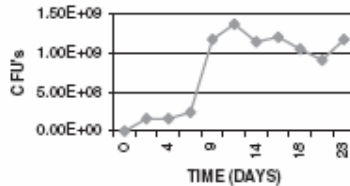


Figure 3 Biofilm growth on coated cast iron

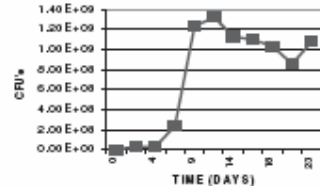


Figure 4 Biofilm growth on galvanized steel

The first set, was fastened to a 100 mm-diameter pulley and the second set was fastened to a 76 mm-diameter pulley. The result of this configuration was that the first set rotated at a much higher angular velocity than the second set. Thus two different flow conditions were simulated simultaneously at room temperature (16–20°C). Four different piping materials were used to test the response of biofilm growth to fluid velocity i.e.: asbestos-cement (10 mm thick); cast iron in a red epoxy coating (6 mm thick); galvanized steel (4 mm thick) and PVC (2 mm thick). The following analysis were conducted on the biofilm: i) DAPI staining and UV-light microscopy (Wolfaardt *et al.*, 1991); ii) determination of the number of culturable cells (Cloete and Jacobs, 2001).

Results and discussion

Biofilm formation took place on all piping surfaces in a potable water distribution system (Figures 1–4). There was no significant difference in the bacterial colonization rates on the different surfaces, irrespective of the type of material (Figures 1–4). The yield measured as the total number of viable cells in the biofilm did however differ, with the cfu being the highest on the PVC piping and the lowest on the galvanized steel piping (Figures 1–4). The number of cfu reached a maximum between 9–10 days after which the cfu started to level off somewhat and fluctuated for the remainder of the study period.

Increased flow in the system resulted in a specific detaching velocity, where the formation of biofilm was overcome (Figures 7–8). These results are in agreement with that of Trulear and Characklis (1982) and Wolfaardt and Cloete (1992). Most of the time these detaching velocities were not the highest velocities tested.

The range of detaching velocities were between $\pm 3 \text{ m}\cdot\text{s}^{-1}$ and $4 \text{ m}\cdot\text{s}^{-1}$ (Figures 7–8). A flow velocity within this range would thus be ideal for achieving reduced biofilm growth in potable water distribution systems.

Conclusions

Increased velocity in the system resulted in a specific detaching velocity, where the formation of biofilm was limited. Most of the time these detaching velocities were not the highest velocities tested. The range of detaching velocities were between $\pm 3 \text{ m}\cdot\text{s}^{-1}$ and $4 \text{ m}\cdot\text{s}^{-1}$. A flow velocity within this range would thus be ideal for achieving reduced biofilm growth in a distribution system.

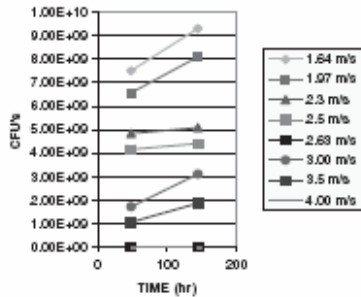


Figure 5 Total viable sessile bacteria on PVC

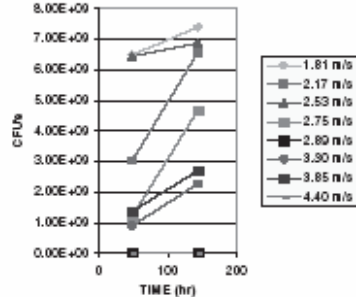


Figure 6 Total viable sessile bacteria on coated cast iron

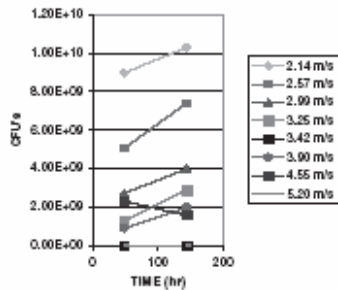


Figure 7 Total viable sessile bacteria on asbestos cement

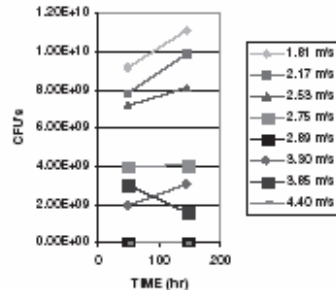


Figure 8 Total viable sessile bacteria on galvanized steel

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