

CLOSED-LOOP IDENTIFICATION OF PLANTS UNDER MODEL PREDICTIVE CONTROL

by

Elsa de Klerk

Submitted in partial fulfilment of the requirements for the degree

Master of Engineering (Electronic Engineering)

in the

Faculty of Engineering, The Built Environment and Information
Technology

UNIVERSITY OF PRETORIA

July 2003

SUMMARY

The open-loop step testing approach, which is, typically, used in process identification for model-based predictive control (MPC), has some disadvantages. Closed-loop system identification is less intrusive than the open-loop approach and can reduce re-identification time considerably. If the process model is identified while the MPC controller is operating, safety, product quality and optimality problems will be avoided.

For above-mentioned reasons, multivariable closed-loop identification for use in MPC is studied. Relevant closed-loop approaches are reviewed and a closed-loop identification methodology for MPC controlled plants is chosen. Simulations and real process data are used to validate and evaluate this methodology.

Many estimation methods fail when applied directly to closed-loop data, because of correlation between the additive output noise and the plant input. However, the prediction error estimation method can still give consistent estimates in the presence of noise. Therefore, this method is utilised.

In open-loop a persistently exciting plant input ensures identifiability. This does not ensure identifiability in closed-loop. For identifiability in closed-loop either the feedback mechanism should be nonlinear or the reference signal should be persistently exciting. The inter-sampling approach, where the plant output is sampled at a higher rate than the control input, can also ensure identifiability. However, a variance simulation study shows that a model identified with this approach is imprecise when structured tests are not performed.

The direct closed-loop system identification approach, where only the plant output and input are used for identification of the plant, is employed. This approach works irrespective of the feedback mechanism, it ensures consistency and optimal precision, and it makes use of standard MATLAB functions.

In the simulation a multivariable MPC controlled plant is identified from closed-loop data. To evaluate the consistency of the methodology, the plant is identified for different controller settings and different added disturbances. Different methods for ensuring identifiability are also investigated. Together with the standard validation tests used in open-loop identification, models are compared to the open-loop identified model and the stability of the closed-loop systems are examined.

The simulation results show that the proposed methodology gives reliable results for the type of system disturbances and constraints used when structured tests are performed that

ensure persistently exciting reference signals and good signal-to-noise ratios. The results also show that imprecise models are usually identified when only relying on inter-sampling or the nonlinearity of the controller for identifiability.

A part of an industrial multivariable plant is also identified. No structured tests are performed on the plant. Logged data sets from normal operation are used in the identification. It is concluded that the open-loop identified model is not a good representation of the plant in closed-loop operation at the relevant time. Therefore, the results from the comparison between the open-loop and closed-loop identified models are unreliable.

From this experiment a preliminary conclusion is made that an unsatisfactory model will usually be identified from data measured under normal closed-loop control, because the reference signals are usually not persistently exciting and the signal-to-noise ratios are not good.

Keywords: closed-loop system identification, open-loop, model-based predictive control, multivariable, prediction error estimation method, methodology, identifiability, persistently exciting, nonlinear feedback, inter-sampling, validation, evaluation, variance, simulation, process data, signal-to-noise ratio.

SAMEVATTING

Die opelustraptoetsbenadering, wat tipies gebruik word in aanlegidentifikasie vir modelgebaseerde voorspellingsbeheer (MVB), het sekere nadele. Geslotelusstelselidentifikasie het 'n kleiner impak as die opelusbenadering en kan her-identifikasietyd aansienlik verminder. Indien die prosesmodel geïdentifiseer word terwyl die MVB beheerde in bedryf is, sal probleme met betrekking tot veilighed, produk kwaliteit en optimaliteit vermy word.

Om bogenoemde rede word multiveranderlike geslotelusidentifikasie vir gebruik met MVB bestudeer. Toepaslike geslotelusbenaderings word hersien en 'n geslotelusidentifikasiemetodiek vir MVB beheerde aanlegte word gekies. Simulasies en prosesdata word gebruik om die metodiek te verifieer en te evaluateer.

Baie skattingsmetodes faal wanneer dit direk toegepas word op geslotelusdata as gevolg van die korrelasie tussen die aanleginset en ruis op die aanleguitset. Die foutvoorspellingskattingsmetode kan egter wel konsekwente skattings gee; dus word dié skattingsmetode geïmplimenteer.

In opelus word identifiseerbaarheid verseker deur 'n aanhoudend stimulerende ("persistently exciting") aanleginset. Dit verseker nie identifiseerbaarheid in geslotelus nie. In geslotelus word identifiseerbaarheid verseker as óf die terugvoermeganisme nie-linieér is óf die verwysingssein aanhoudend stimulerend is. Die inter-monsteringsmetode, waar die aanleguitset teen 'n hoër spoed as die beheerinset gemonster word, verseker ook identifiseerbaarheid. 'n Simulasiestudie oor variansie dui egter aan dat 'n model geïdentifiseer met dié metode, sonder gestruktureerde toetse, gewoonlik nie presies is nie.

Die direkte geslotelusstelselidentifikasiebenadering, waar slegs die aanleguitset en -inset gebruik word in die identifisering, word gebruik. Hierdie benadering werk onafhanklik van die terugvoermeganisme, dit verseker konsekwente skattings en optimale presiesheid, en dit maak gebruik van standaard MATLAB funksies.

In die simulasié word 'n multiveranderlike MVB beheerde aanleg geïdentifiseer uit geslotelusdata. Om die konsekwensie van die metodiek te evaluateer, word die aanleg geïdentifiseer vir verskillende beheerderstellings en ook verskillende toegevoegde versteurings. Verskillende metodes om identifiseerbaarheid te verseker, word ook ondersoek. Saam met die standaard verifieeringstoetse, wat in opelusidentifikasie gebruik word, word modelle ook vergelekyk met opelusgeïdentificeerde modelle en die stabiliteit van die geslotelusstelsels word ondersoek.

Die simulasieresultate toon aan dat die voorgestelde metodiek betroubare resultate lewer vir die tipe versteurings en beheerdestellerings wat gebruik is, wanneer gestructureerde toetse gedoen word wat 'n aanhoudend stimulerende verwysingssein en 'n goeie sein-tot-ruis verhouding verseker. Die resultate toon ook aan dat daar gewoonlik 'n groot variansie in geïdentifiseerde modelle ontstaan wanneer daar slegs op inter-monstering of 'n nie-liniêre beheerde vertrou word vir identifiseerbaarheid.

'n Deel van 'n multiveranderlike industriële aanleg word ook geïdentifiseer. Geen gestructureerde toetse word uitgevoer op die aanleg nie. Data, gemonster tydens normale werking, word gebruik vir identifikasie. Daar word tot die gevolgtrekking gekom dat die opelusgeïdentifiseerde model nie 'n goeie voorstelling van die aanleg onder geslotelusbeheer, tydens die toepaslike tyd, is nie; dus is die resultate uit die vergelyking tussen die opelus- en geslotelusgeïdentifiseerde modelle onbetroubaar.

Uit die eksperiment kan 'n voorlopige gevolgtrekking gemaak word dat 'n onaanvaarbare model gewoonlik geïdentifiseer sal word uit data gemonster tydens normale geslotelusbeheer, aangesien in dié geval die verwysingsseine gewoonlik nie aanhoudend stimulerend is nie en die sein-tot-ruis verhouding nie goed is nie.

Sleutelwoorde: geslotelusstelselidentifikasie, opelus, modelgebasseerde voorspellingsbeheer, multiveranderlik, foutvoorspellingsskattingsmetode, metodiek, identifiseerbaarheid, aanhoudend stimulerend ("persistently exciting"), nie-liniêre terugvoer, inter-monstering, verifieer, evalueer, variansie, simulasie, prosesdata, sein-tot-ruis verhouding.

ABBREVIATIONS

AIC	Akaike's Information Theoretic Criterion
ARMAX	Auto-Regressive Moving Average with External input
ARX	Auto-Regressive with External input
ASYM	Asymptotic Method
BJ	Box-Jenkins
CLOSID	Closed-loop System Identification
CV	Controlled Variable
DMC	Dynamic Matrix Controller
DMK	Dimethyl Ketone
FIR	Finite Impulse Response
FPE	Final Prediction Error
IDARX	Multivariable ARX
IPA	Isopropyl Alcohols
IV	Instrumental Variables
LSE	Least-Squares Estimate
MDL	Minimum Description Length
MIBK	Methyl Iso Butyl Ketone
MIMO	Multiple-Input-Multiple-Output
MISO	Multiple-Input-Single-Output
MPC	Model-based Predictive Control
MPCI	MPC and Identification
MV	Manipulated Variable
OE	Output Error
PDF	Probability Density Function
PE	Persistently Exciting
PEM	Prediction-Error Method
PRBS	Pseudo-Random Binary Signal
QP	Quadratic programme
RBS	Random Binary Signal
RMPCT	Robust Model Predictive Control
SCI	Sasol Chemical Industries
SID	System Identification
SISO	Single-Input-Single-Output
SITB	System Identification Toolbox
SNR	Signal-to-Noise Ration
SSF	Sasol Synthetic Fuels
SVD	Singular Value Decomposition
w.p.	with probability
ZOH	Zero-Order-Hold

CONTENTS

Summary	3
Samevatting	5
Abbreviations	7
1 Introduction	12
1.1 Problem Statement	12
1.2 Literature Review	13
1.2.1 Advantages of Closed-Loop Identification	13
1.2.2 Correlation Problems in Closed-Loop	14
1.2.3 Closed-Loop Identifiability Problem	15
1.2.4 Special-Purpose Closed-Loop Identification Software	16
1.3 Research Objectives	16
1.4 Research Approach	17
1.5 Research Contribution	17
1.6 Organization of the Dissertation	18
2 Process Description	20
2.1 Introduction	20
2.2 Overview of the Industry	20
2.3 Operational Description of the MIBK Process	21
2.4 Controller	24
2.4.1 Model Predictive Controllers in General	24
2.4.2 Dynamic Matrix Controllers	28
2.4.3 The DMCplus Controller implemented on the MIBK plant	28
2.5 Available Process Information	29
2.5.1 Process Model	29
2.5.2 Measured Data	30
2.5.3 Other Relevant Information	31
2.6 Conclusion	31
3 Closed-Loop System Identification Theory	33
3.1 Introduction	33
3.2 System Identification Problem	33

3.3 Closed-Loop Configuration: Assumptions and Notation	36
3.4 Closed-Loop Correlation Problem	38
3.5 Informative Closed-Loop Experiments	39
3.6 Different Approaches to Closed-Loop Identification	41
3.7 Closed-Loop Identification in the Prediction Error Framework	42
3.7.1 Assumptions and Notation	42
3.7.2 Prediction Error Estimation Method	44
3.7.3 Family of Model Structures	45
3.7.4 Computing the Estimate	47
3.7.5 Consistency and Identifiability	48
3.7.6 Bias Distribution	50
3.7.7 Asymptotic Variance Distribution	52
3.8 Excitation Signals	53
3.9 Inter-Sampling Approach	55
3.9.1 Introduction	55
3.9.2 Model Representation	55
3.9.3 Identifiability Analysis	57
3.10 Conclusion	58
4 Selection of a Methodology Applicable to MPC Controlled Plants	61
4.1 Introduction	61
4.2 Closed-Loop Identification Approach	61
4.3 Guarantee of Identifiability	63
4.4 Evaluation of the Inter-Sampling Approach	65
4.4.1 Set-Up of the Variance Simulation	65
4.4.2 Results of Variance Simulation	67
4.4.3 Discussion of the Variance Simulation Results	73
4.4.4 Conclusion of the Variance Simulation	74
4.5 Model Structure Selection	74
4.5.1 Model Consistency	74
4.5.2 Compactness and Parametric Structures	75
4.5.3 Numerical Complexity	76
4.5.4 Multivariable Models	76
4.5.5 Model Order Selection	77

4.6 Model Validation	78
4.6.1 Standard Validation with the Closed-Loop Data	79
4.6.2 Comparison with the Open-Loop Identified Model	81
4.6.3 Examination of the Closed-Loop System	82
4.7 System Identification Toolbox	83
4.8 System Identification Steps	84
4.8.1 Experiment Design	84
4.8.2 Data Collection	85
4.8.3 Model Structure Selection	86
4.8.4 Model Estimation	87
4.8.5 Model Validation	87
4.8.6 Methodology Validation	87
4.9 Conclusion	88
5 Validation and Evaluation of the Methodology with Simulations	90
5.1 Introduction	90
5.2 Simulation Set-Up	90
5.2.1 Plant	90
5.2.2 Controller	91
5.2.3 Simulation Scenarios	92
5.3 Implementation of the Methodology	94
5.3.1 Experiment Design	95
5.3.2 Data Collection	95
5.3.3 Model Structure Selection	98
5.3.4 Model Estimation	98
5.3.5 Model Validation	99
5.3.6 Methodology Validation	99
5.4 Validation Results	100
5.4.1 Expected Results	100
5.4.2 Obtained Results	101
5.4.3 Discussion	125
5.5 Conclusion	128
6 Validation and Evaluation of the Methodology with Real Process Data	130
6.1 Introduction	130

6.2 Implementation of the Methodology	130
6.2.1 Experiment Design	130
6.2.2 Data Collection.....	131
6.2.3 Model Structure Selection.....	132
6.2.4 Model Estimation	132
6.2.5 Model Validation	133
6.2.6 Methodology Validation	133
6.3 Validation Results	135
6.3.1 Expected Results	136
6.3.2 Obtained Results	136
6.3.3 Discussion	144
6.4 Evaluation of the Proposed Methodology	147
6.4.1 Reasons for Success/Failure of the Implemented Methodology	147
6.4.2 Recommendation for Future Implementation of the Methodology	147
6.5 Conclusion	148
7 Conclusions and Future Research	150
7.1 Introduction.....	150
7.2 Review of the Closed-Loop Techniques	150
7.3 Selection of a Methodology Applicable to MPC Controlled Plants	151
7.4 Validation and Evaluation of the Methodology with Simulations	153
7.5 Validation and Evaluation of the Methodology with Real Process Data	153
7.6 Direction of Future Research	154
References	155
A Closed-Loop System for the Inter-Sampling Simulation Study	160
B Approximate Realization of Step Response Data	162
C Residual Analysis of Experimental Data	164