

DESIGN AND OPTIMUM OPERATION OF A RE-CONFIGURABLE PLANAR GOUGH- STEWART MACHINING PLATFORM

by

Lukas Johannes du Plessis

A dissertation submitted in partial fulfillment of the
requirements for the degree of

Philosophiae Doctor (Mechanical Engineering)

in the

Faculty of Engineering, Built Environment and Information
Technology, University of Pretoria

December 2001

b15432245

AKADEMIESE INLIGTINGSDIENS UNIVERSITEIT VAN PRETORIA	
2002-11-13	
Klasnomer	ZAPR 621.812
Aanvraagnoer	i16034864 DU PLESSIS

Dedicated to my family
and in memory of
“Oom Nap & Tannie Lalie Esterhuizen”

ABSTRACT

DESIGN AND OPTIMUM OPERATION OF A RE-CONFIGURABLE PLANAR GOUGH-STEWART MACHINING PLATFORM

by

Lukas Johannes du Plessis

Promoter: **Professor J.A. Snyman**

Department of Mechanical and Aeronautical Engineering

Degree: Philosophiae Doctor (Mechanical Engineering)

Keywords: Gough-Stewart platform, re-configurable machine tool, adjustable geometry, inverse kinematics, inverse dynamic analysis, trajectory-planning, cubic spline interpolation, mathematical optimization, constrained optimization problem.

This study presents a computer operating system for a novel *re-configurable planar Gough-Stewart machining platform*. The operating system is tested on a physically constructed *test-model* of the proposed re-configurable platform. In doing so, the proposed concept of a re-configurable planar machine tool, consisting of a moving platform connected to a fixed base via three linear actuators is validated, both from a theoretical and practical point of view.

The computer operating system consists of four sections:

1. **Simulation:** A computer program for simulating the motion of a planar Gough-Stewart platform was developed. This was done by applying the basic principles of Newton-Euler dynamics to a mechanical model of the platform. In particular, this special purpose simulation program allows for the *inverse dynamic analysis* of a planar Gough-Stewart platform so as to give closed-form expressions for the required actuator forces necessary for the execution of a *specified trajectory*. As a prerequisite for the inverse dynamic analysis, the special purpose program that was developed, also performs the *inverse kinematic analysis* of the mechanism by solving closed-form expressions for the positions, velocities and accelerations of the individual bodies comprising the machine.
2. **Trajectory-planning:** A new *path-planning* interpolation algorithm has been developed with which a user may specify the desired path to be followed by any *planar* industrial robot, and therefore in particular also the planar Gough-Stewart platform. Given prescribed kinematical requirements and

specified points along the path, a *cubic spline interpolation curve* is fitted in the time-domain, and further user-specified information is used to determine how the end-effector orientation angle should vary along the specified curve. This trajectory-planning algorithm is combined with the above-mentioned inverse dynamic simulation program to determine and monitor the required actuator forces as the planar Gough-Stewart platform traces the prescribed trajectory.

3. **Optimization:** With the ability to determine the required actuator forces at any instant along any prescribed path, an *adjustable geometry* planar Gough-Stewart machining platform becomes a viable option. The rationale is that the simulation of the mechanism allows for the off-line *optimization* of the operational geometry of the mechanism for the prescribed path. The single criterion objective function used is the minimization of the “maximum magnitude actuator force” identified via the above-mentioned dynamic simulation. The minimization of this objective function with respect to the variable geometry, ensures that singular configurations are avoided as the specified path is traced. The minimization of the objective function is further subjected to compliance with formulated inequality constraints that ensures mechanical feasibility as the *constrained optimization problem* is solved.

Once the optimum operational geometry is determined, the physical re-configurable planar Gough-Stewart platform can be adjusted accordingly to ensure the successful execution of the desired trajectory. If it is not possible to trace the prescribed path, then user intervention is required. This may be done in a rational manner since the specific numerical optimization algorithm used here (LFOPC), gives a best compromised solution if no feasible design exists for the specified trajectory. The importance of this compromised solution is that it points out which constraints are violated and to what extent. This provides information for determining a piece-wise execution strategy by means of which the complete task may be performed, both feasibly and optimally.

4. **Control:** Apart from optimizing the Gough-Stewart platform configuration for a given task, the computer operating system also generates the necessary commands for controlling the required variation of the actuator leg lengths. This allowed for the physical execution of a number of representative prescribed machining paths.

SAMEVATTING

ONTWERP EN OPTIMALE WERKING VAN ‘n HERKONFIGUREERBARE VLAK GOUGH-STEWART- MASJINERINGSPLATFORM

deur

Lukas Johannes du Plessis

Promotor: **Professor J.A. Snyman**

Department Meganiese and Lugvaartkundige Ingenieurswese

Graadbenaming: Philosophiae Doctor (Meganiese Ingenieurswese)

Sleutelwoorde: Gough-Stewart platform, herkonfigureerbare masjienwerktuig, verstelbare geometrie, terugwaartse kinematika, terugwaartse dinamiese analise, kubiese lat-interpolasie, wiskundige optimering, begrensde optimeringsprobleem.

Hierdie studie handel oor ‘n rekenaarbedryfstelsel vir die inwerkingstelling van ‘n unieke *herkonfigureerbare vlak Gough-Stewart-masjineringsplatform*. Die bedryfstelsel is getoets met behulp van ‘n toetsmodel van die voorgestelde herkonfigureerbare platform, wat spesiaal vir die doel ontwerp en gebou is. Sodoende is die uitvoerbaarheid van die voorgestelde konsep van ‘n herkonfigureerbare vlak masjienwerktuig bevestig, beide vanuit ‘n teoretiese en praktiese oogpunt. Die herkonfigureerbare vlak Gough-Stewart-masjineringsplatform waarna verwys word, bestaan uit ‘n bewegende platform wat deur middel van drie lineêre aktueerders aan ‘n vaste basis gekoppel is.

Die rekenaarbedryfstelsel bestaan uit vier dele:

1. **Simulasie:** ‘n Rekenaarprogram is geskryf om die beweging van ‘n vlak, Gough-Stewart-platform na te boots. Dit is gedoen deur die basiese beginsels van Newton-Euler-dinamika toe te pas op ‘n meganiese model van die platform. Hierdie doelgerigte en toegewyde simulasieprogram stel ‘n mens in staat om die *terugwaartse dinamiese analise* van ‘n vlak Gough-Stewart-platform ekonomies te doen. Dit behels die gebruik van geslote-vorm wiskundige uitdrukings waardeur die onbekende aktueerdekrakte tydens die uitvoering van die *voorgeskrewe baan* bereken kan word. As deel van die terugwaarste dinamiese analise voer hierdie spesiale rekenaarprogram ook die terugwaartse kinematiese analise uit deur gebruik te maak van geslote-vorm uitdrukings vir die posisies, snelhede en versnellings van die individuele liggame waaruit die masjien bestaan.

2. **Trajekbeplanning:** 'n Nuwe intepolerende *trajekbeplannings*-algoritme is ontwikkel waarmee die gebruiker die verlangde baan, wat deur enige *vlak* industrieëlle robot en gevvolglik ook die vlak Gough-Stewart-platform gevolg moet word, analities kan spesifiseer. Met sekere voorgeskrewe kinematische vereistes bekend, asook die gespesifiseerde node-punte langs die baan, pas die trajekbeplannings-algoritme interpolerende kubiese latfunksies in die tyddomein. Verdere insette van die gebruiker is egter nodig om te bepaal hoe die orientasie-hoek van die meganisme se beheerde eindwerktyg moet varieer langs die voorgeskrewe baan. Ten einde die aktueerdekrakte langs verskillende voorgeskrewe bane te bereken, is die trajekbeplannings-algoritme gekombineer met bogenoemde terugwaartse dinamiese analise van die vlak Gough-Stewart-masjineringsplatform.
3. **Optimering:** Die lewensvatbaarheid van 'n vlak Gough-Stewart-platform met 'n *verstelbare geometrie*, lê daarin opgesluit dat dit moontlik is om die onbekende aktueerdekrakte langs enige voorgeskrewe baan en op enige gegewe tydstip te bereken. Die rekenaarsimulasie van die meganisme stel 'n mens in staat stel om die werkingsgeometrie van die meganisme te *optimeer* na gelang van die voorgeskrewe baan. Die enkelmaatstafdoelfunksie wat hiervoor gebruik word, is die mimimering van die "maksimum-grootte-aktueerdekrug" wat via bogenoemde dinamiese rekenaarsimulasie geïdentifiseer word. Die minimering van hierdie doelfunksie, met betrekking tot die verstelbare geometrie, waarborg dat singuliere konfigurasies geassosieer met oneindige groot aktueerdekrakte tydens die uitvoering van die voorgeskrewe baan, vermy word. Verder moet die minimering van hierdie doelfunksie uitgevoer word met inagneming van geformuleerde ongelykheidsbegrensings. Sodoende word die meganiese uitvoerbaarheid van die berekende oplossing tot die *begrensde optimeringsprobleem*, verseker.
Sodra die optimale werkingsgeometrie bepaal is, word die fisiese herkonfigureerbare vlak Gough-Stewart-platform dienooreenkomsdig verstel, ten einde die voorgeskrewe baan suksesvol uit te voer. Indien dit onmoontlik is om die voorgeskrewe baan te volg, moet die gebruiker 'n beredeneerde besluit maak. Die spesifieke numeriese optimerings-algoritme wat in hierdie studie gebruik word (LFOPC), bereken die beste moontlike kompromie-oplossing indien daar geen lewensvatbare ontwerp vir 'n voorgeskrewe baan bestaan nie. Die beste kompromie-oplossing dui aan watter ongelykheidsbegrensings oorskry is, en tot watter mate. Hierdie kompromie-oplossing is noodsaaklik om 'n beredeneerde besluit te maak aangaande die stuksgewyse uitvoering van die voorgeskrewe baan op 'n lewensvatbare en optimale wyse.
4. **Beheer:** Afgesien van die konfigurasie-optimering van die Gough-Stewart-platform na gelang van 'n gegewe taak, genereer die rekenaarbedryfstelsel ook die beheerkode wat nodig is vir die verlangde variasie in aktueerdebeenlengtes. Gevolglik is 'n paar verteenwoordigende masjineringsbane fisies uitgevoer met behulp van die toetsmodel.

ACKNOWLEDGEMENTS

I would like to express my deepest gratitude towards my promoter and mentor Prof. Jan Snyman for his guidance and input over the past five years. I consider it a great privilege and honor to have studied under such an excellent scientist and researcher.

This study was made possible through the financial support of the South African National Research Foundation, the University of Pretoria, the Department of Mechanical and Aeronautical Engineering at the University of Pretoria as well as my loving mother. A Mellon Foundation grant was also awarded. I am very grateful to everybody who was involved in arranging the necessary funding.

A very special acknowledgement goes to Mr. Hannes Smit of Deman CC for all the time and resources that he has contributed to getting the test-model running. I would also like to thank Mr. Wolfgang Kaizer and the staff of Jawo Engineering for the excellent job they did manufacturing the test-model.

The kind help of Mr. Mike Spalletta and his colleagues at the University of Pretoria Engineering Computer Center is greatly appreciated, as is the help of Mr. Waldemar Wandschneider, Mr. Fred Proctor (NIST), Mr. Will Shackleford (NIST), Mr. Alex Hay, Mr. Michael Hindley, Mr. Christiaan Erasmus and Mr. Johannes Jordaan.

My sincerest thanks to everybody else not mentioned here who contributed to the successful completion of this study.

Praise the Lord!

TABLE OF CONTENTS

ABSTRACT.....	I
SAMEVATTING.....	III
ACKNOWLEDGEMENTS.....	V
CHAPTER 1 INTRODUCTION: OVERVIEW OF GOUGH-STEWART PLATFORMS USED AS MACHINING CENTERS	1
1.1 INTRODUCTION	1
1.2 HISTORY OF GOUGH-STEWART PLATFORMS.....	1
1.3 GOUGH-STEWART PLATFORMS AS MACHINING CENTERS	6
1.3.1 <i>6-DOF Gough-Stewart machining platforms</i>	6
1.3.2 <i>Planar Gough-Stewart machining platforms</i>	10
1.3.2.1 The “Smartcuts” planar Gough-Stewart platform.....	10
1.3.2.2 The “Dyna-M” and “Honda HVS-5000” machine tools.....	13
1.4 THE RE-CONFIGURABLE CONCEPT	15
1.4.1 <i>Modular Gough-Stewart platforms</i>	16
1.4.2 <i>Variable geometry Gough-Stewart platforms</i>	17
1.5 THE OPTIMUM DESIGN OF GOUGH-STEWART PLATFORMS	18
1.5.1 <i>The analytical approach</i>	19
1.5.2 <i>The numerical approach</i>	20
1.5.2.1 Genetic Algorithms	20
1.5.2.2 The “Democrat” design methodology.....	23
1.5.2.2.1 Democrat: the cutting phase	23
1.5.2.2.2 Democrat: the refining phase	25
1.5.2.2.3 Democrat: Optimizing the “HFM2” 6-DOF Gough-Stewart platform design	27
1.5.2.2.4 Democrat: Optimizing the “HDM1” 6-DOF Gough-Stewart platform design.....	30
1.6 MOTIVATION FOR THE PRESENT STUDY.....	31
1.6.1 <i>The concept of a re-configurable planar Gough-Stewart machining platform</i>	31
1.6.1.1 Mechanical feasibility.....	31
1.6.1.2 Simulation of a planar Gough-Stewart platform.....	32
1.6.1.2.1 Inverse Dynamic simulation.....	32
1.6.1.2.2 Trajectory-planning	33
1.6.1.3 Optimal adjustment of the variable geometry	35
1.6.2 <i>The concept verification: a re-configurable planar Gough-Stewart platform test-model</i>	36
CHAPTER 2 KINEMATIC AND KINETIC MODELING OF A PLANAR MACHINING CENTER.....	39
2.1 INTRODUCTION	39
2.2 RIGID BODY MODEL	41

2.3 KINEMATIC CONSTRAINT EQUATIONS	44
2.3.1 <i>Revolute joints</i>	45
2.3.2 <i>Translational joints</i>	46
2.3.3 <i>Simplified constraints</i>	49
2.4 DRIVING CONSTRAINTS.....	49
2.4.1 <i>Fixed workpiece</i>	50
2.4.2 <i>Fixed cutting tool</i>	53
2.5 INVERSE KINEMATIC ANALYSIS	55
2.6 KINETIC ANALYSIS.....	62
2.6.1 <i>Planar equations of motion for a system of unconstrained bodies</i>	62
2.6.2 <i>Planar equations of motion for a system of constrained bodies</i>	63
2.6.3 <i>Constraint reaction forces</i>	66
2.6.3.1 Revolute joint.....	67
2.6.3.2 Translational joint.....	69
2.6.4 <i>Vector of forces</i>	71
2.6.4.1 Gravity	71
2.6.4.2 Single force.....	72
2.6.4.2.1 Fixed workpiece	73
2.6.4.2.2 Fixed cutting tool.....	75
2.6.5 <i>Inverse dynamic analysis</i>	77
2.7 VERIFICATION OF SPECIAL PURPOSE PROGRAM.....	81
2.7.1 <i>Jacobian matrix verification</i>	81
2.7.2 <i>Inverse dynamic analysis verification</i>	83
2.7.3 <i>Fixed workpiece vs. fixed tool verification</i>	84
CHAPTER 3 TRAJECTORY-PLANNING THROUGH INTERPOLATION BY OVERLAPPING CUBIC ARCS AND CUBIC SPLINES.....	90
3.1 BASIC INTERPOLATION PROBLEM IN TRAJECTORY PLANNING.....	90
3.1.1 <i>Determination of time parametric intervals</i>	91
3.1.1.1 Determination of interpolating and overlapping cubic arcs.....	91
3.1.1.2 Computation of total path length S	97
3.1.1.3 Dependence of curve length on parameter t	98
3.1.2 <i>Cubic spline representations for $X(t)$ and $Y(t)$</i>	100
3.2 PRACTICAL PROBLEM OF DETERMINING DY/DX AT P_0 AND P_N	102
3.3 SYNTHESIS OF MORE GENERAL CURVES	107
3.3.1 <i>Linear segment with cubic blends</i>	107
3.3.2 <i>Treatment of constraint on acceleration</i>	112
3.3.2.1 Attainment of central speed v^*	113
3.3.2.2 Violation of maximum allowable acceleration	114
3.4 INCORPORATION OF AN ORIENTATION ANGLE ϕ	117
3.5 TEST PROBLEMS.....	121
3.5.1 <i>Parabolic test function</i>	121

3.5.2	<i>Spike test function</i>	124
3.5.3	<i>Circular test curve</i>	126
3.5.4	<i>Logarithmic spiral test curve</i>	130
3.5.5	<i>Non-analytical test curve</i>	133
CHAPTER 4 THE DETERMINATION OF OPTIMUM PLATFORM GEOMETRIES FOR PRESCRIBED MACHINING TASKS.....		138
4.1	INTRODUCTION	138
4.2	FORMULATION OF THE CONSTRAINED OPTIMIZATION PROBLEM.....	139
4.2.1	<i>Design variables describing the adjustable geometry of the planar Gough-Stewart platform machining center</i>	139
4.2.2	<i>Objective function used to optimize the planar machining center geometry</i>	141
4.2.3	<i>Constraints applicable on the planar machining center</i>	142
4.3	EVALUATION OF THE CONSTRAINED OPTIMIZATION PROBLEM	143
4.3.1	<i>Evaluation of the objective function</i>	143
4.3.2	<i>Evaluation of the inequality constraints</i>	147
4.4	SOLVING THE CONSTRAINED OPTIMIZATION PROBLEM	148
4.5	DISCUSSION OF OPTIMIZATION RESULTS	151
CHAPTER 5 DEMONSTRATION OF THE OPTIMUM EXECUTION OF REPRESENTATIVE PRESCRIBED MACHINING PATHS.....		159
5.1	INTRODUCTION	159
5.2	PARABOLIC TOOL PATH	161
5.2.1	<i>Nodal points and orientation angle</i>	161
5.2.2	<i>Optimization results</i>	162
5.2.3	<i>Analysis of convergence to optimum</i>	165
5.2.4	<i>Execution of parabolic tool path</i>	169
5.3	SPIKE TOOL PATH.....	170
5.3.1	<i>Nodal points and orientation angle</i>	170
5.3.2	<i>Optimization results</i>	171
5.3.3	<i>Analysis of convergence to optimum</i>	174
5.3.4	<i>Execution of the spike tool path</i>	176
5.4	CIRCULAR TOOL PATH	178
5.4.1	<i>Nodal points and orientation angle</i>	178
5.4.2	<i>Optimization results</i>	179
5.4.3	<i>Analysis of convergence to optimum</i>	181
5.4.4	<i>Execution of the circular tool path</i>	185
5.5	SPIRAL TOOL PATH.....	186
5.5.1	<i>Nodal points and orientation angle</i>	186
5.5.2	<i>Optimization results</i>	187
5.5.3	<i>Analysis of convergence to optimum</i>	189

5.5.4	<i>Execution of the spiral tool path</i>	191
5.6	TREBLE CLEF TOOL PATH.....	193
5.6.1	<i>Nodal points and orientation angle</i>	193
5.6.2	<i>Optimization results</i>	194
5.6.3	<i>Analysis of convergence to optimum</i>	196
5.6.4	<i>Execution of the treble clef tool path</i>	198
5.7	BIGGER PARABOLIC TOOL PATH	199
5.7.1	<i>Continuous prescribed tool path</i>	200
5.7.1.1	Nodal points and orientation angle.....	200
5.7.1.2	Optimization results.....	201
5.7.2	<i>Dividing the prescribed path into segments</i>	205
5.7.2.1	Nodal points and orientation angle.....	205
5.7.2.2	Optimization results for segment (b) of Figure 5.34.....	208
5.7.2.3	Optimization results for segment (a) of Figure 5.34.....	211
5.7.3	<i>Execution of the prescribed bigger parabolic tool path</i>	214
5.7.3.1	First execution of segment (b) (see Figure 5.34).....	214
5.7.3.2	Execution of segment (a) (see Figure 5.34).....	215
5.7.3.3	Second execution of segment (b) (see Figure 5.34).....	216
CHAPTER 6 CONCLUSION		219
6.1	COMPUTER SIMULATION.....	219
6.1.1	<i>Kinematic and kinetic modeling</i>	220
6.1.2	<i>OCAS trajectory-planning algorithm</i>	220
6.2	FORMULATION OF THE CONSTRAINED DESIGN OPTIMIZATION PROBLEM	221
6.3	THE LFOPC-ALGORITHM	222
6.4	THE ADJUSTABLE GEOMETRY PLANAR GOUGH-STEWART PLATFORM TEST-MODEL.....	223
APPENDIX A DERIVATION OF THE PLANAR EQUATIONS OF MOTION.....		226
A.1	NEWTON'S SECOND LAW.....	226
A.2	PLANAR EQUATIONS OF MOTION.....	228
A.2.1	<i>Planar translational equations of motion</i>	229
A.2.2	<i>Planar rotational equations of motion</i>	230
APPENDIX B FLOWCHART OF THE OCAS TRAJECTORY-PLANNING METHODOLOGY		235
APPENDIX C THE LFOPC MATHEMATICAL OPTIMIZATION ALGORITHM.....		239
C.1	BACKGROUND	239
C.2	BASIC DYNAMIC MODEL.....	239
C.3	LFOP: BASIC ALGORITHM FOR UNCONSTRAINED PROBLEMS	240
C.4	LFOPC: MODIFICATION FOR CONSTRAINED PROBLEMS	241

APPENDIX D PHYSICAL SPECIFICATION FOR SIMULATION AND OPERATIONAL CONSTRAINTS OF THE TEST-MODEL.....	243
D.1 INTRODUCTION.....	243
D.2 PHYSICAL SPECIFICATIONS FOR SIMULATION OF THE TEST-MODEL.....	243
D.2.1 <i>Operational geometry</i>	244
D.2.2 <i>Local coordinates</i>	245
D.2.3 <i>Gravitational and frictional external forces</i>	246
D.3 SPECIFICATION OF THE PHYSICAL OPERATIONAL CONSTRAINTS OF THE TEST-MODEL.....	249
D.3.1 <i>Inequality constraint specification for the prevention of mechanical interference</i>	249
D.3.2 <i>Linearly adjustable revolute joints</i>	252
D.3.3 <i>Extreme motion constraints</i>	253
D.3.3.1 Upper frame boundary.....	254
D.3.3.2 Lower frame boundary	255
D.3.3.3 Left hand frame boundary	257
D.3.3.4 Right hand frame boundary.....	258
D.3.4 <i>Revolute joint mechanical interference constraints</i>	259
D.3.4.1 Revolute joint C mechanical interference constraints	260
D.3.4.2 Revolute joint D mechanical interference constraints	264
D.3.4.3 Revolute joint E mechanical interference constraints.....	264
D.3.4.4 Revolute joint A mechanical interference.....	265
REFERENCES	268