

Table C.1 Correlation of input variables

## Appendix C

### Correlation

**Table C.1** Correlation of input variables.

	in1u	in1l	in2u	in2l	in3u	in3l	in4u	in4l	in5u	in5l	in6u	in6l	in7u	in7l	in8u	in8l
in1u	1	0.89	0.9	0.69	0.9	0.54	0.68	0.18	0.76	0.29	0.85	0.57	0.9	0.77	0.82	0.72
in1l	0.89	1	0.79	0.74	0.8	0.63	0.66	0.27	0.77	0.4	0.81	0.62	0.79	0.79	0.81	0.86
in2u	0.9	0.79	1	0.82	0.86	0.38	0.75	0.26	0.75	0.31	0.88	0.57	0.96	0.85	0.76	0.7
in2l	0.69	0.74	0.82	1	0.6	0.38	0.65	0.37	0.67	0.38	0.8	0.65	0.83	0.93	0.66	0.74
in3u	0.9	0.8	0.86	0.6	1	0.52	0.75	0.29	0.75	0.38	0.78	0.54	0.83	0.69	0.7	0.62
in3l	0.54	0.63	0.38	0.38	0.52	1	0.12	0.51	0.46	0.59	0.41	0.67	0.44	0.42	0.6	0.48
in4u	0.68	0.66	0.75	0.65	0.75	0.12	1	0.3	0.74	0.36	0.78	0.44	0.73	0.68	0.5	0.58
in4l	0.18	0.27	0.26	0.37	0.29	0.51	0.3	1	0.44	0.91	0.32	0.65	0.32	0.37	0.32	0.27
in5u	0.76	0.77	0.75	0.67	0.75	0.46	0.74	0.44	1	0.53	0.78	0.62	0.76	0.71	0.8	0.75
in5l	0.29	0.4	0.31	0.38	0.38	0.59	0.36	0.91	0.53	1	0.42	0.73	0.37	0.39	0.45	0.4
in6u	0.85	0.81	0.88	0.8	0.78	0.41	0.78	0.32	0.78	0.42	1	0.56	0.91	0.77	0.79	0.78
in6l	0.57	0.62	0.57	0.65	0.54	0.67	0.44	0.65	0.62	0.73	0.56	1	0.62	0.7	0.68	0.5
in7u	0.9	0.79	0.96	0.83	0.83	0.44	0.73	0.32	0.76	0.37	0.91	0.62	1	0.85	0.79	0.7
in7l	0.77	0.79	0.85	0.93	0.69	0.42	0.68	0.37	0.71	0.39	0.77	0.7	0.85	1	0.7	0.77
in8u	0.82	0.81	0.76	0.66	0.7	0.6	0.5	0.32	0.8	0.45	0.79	0.68	0.79	0.7	1	0.78
in8l	0.72	0.86	0.7	0.74	0.62	0.48	0.58	0.27	0.75	0.4	0.78	0.5	0.7	0.77	0.78	1
n11u	0.86	0.75	0.87	0.73	0.8	0.37	0.73	0.23	0.69	0.27	0.81	0.53	0.87	0.78	0.71	0.61
n11l	0.85	0.72	0.88	0.7	0.82	0.34	0.71	0.23	0.7	0.27	0.82	0.51	0.87	0.75	0.74	0.59
n12u	0.86	0.72	0.82	0.61	0.78	0.34	0.6	0.18	0.65	0.21	0.77	0.45	0.82	0.71	0.79	0.61
n12l	0.81	0.68	0.81	0.63	0.76	0.28	0.63	0.19	0.64	0.19	0.75	0.44	0.8	0.72	0.73	0.58
ou1u	0.93	0.85	0.88	0.72	0.82	0.5	0.65	0.13	0.73	0.26	0.86	0.55	0.87	0.75	0.83	0.72
ou1l	0.8	0.86	0.76	0.76	0.72	0.51	0.63	0.18	0.73	0.32	0.75	0.63	0.73	0.8	0.77	0.81
ou2u	0.9	0.85	0.91	0.76	0.88	0.47	0.78	0.37	0.81	0.43	0.92	0.56	0.93	0.8	0.8	0.77
ou2l	0.69	0.72	0.74	0.65	0.71	0.37	0.63	0.46	0.68	0.49	0.65	0.54	0.69	0.79	0.66	0.73
ou3u	0.84	0.82	0.87	0.79	0.84	0.5	0.76	0.4	0.8	0.42	0.87	0.59	0.9	0.82	0.74	0.74
ou3l	0.72	0.72	0.74	0.67	0.79	0.5	0.68	0.51	0.69	0.51	0.63	0.69	0.71	0.82	0.6	0.61
ou4u	0.72	0.74	0.71	0.54	0.74	0.27	0.81	0.25	0.7	0.39	0.82	0.32	0.69	0.58	0.57	0.71
ou4l	0.12	0.19	0.12	-0.02	0.26	0.29	0.25	0.69	0.29	0.76	0.19	0.37	0.1	0.09	0.24	0.18
ou5u	0.61	0.61	0.63	0.5	0.65	0.17	0.81	0.24	0.54	0.36	0.73	0.3	0.62	0.51	0.36	0.54
ou5l	0.14	0.21	0.31	0.31	0.33	0.07	0.55	0.63	0.41	0.64	0.24	0.48	0.26	0.39	0.13	0.23
ou6u	0.86	0.8	0.87	0.82	0.8	0.36	0.78	0.15	0.73	0.21	0.85	0.51	0.89	0.83	0.66	0.71
ou6l	0.79	0.76	0.8	0.75	0.8	0.41	0.76	0.35	0.72	0.39	0.72	0.61	0.78	0.86	0.58	0.67
ou7u	0.9	0.8	0.92	0.67	0.86	0.48	0.66	0.3	0.77	0.41	0.85	0.55	0.91	0.75	0.82	0.72
ou7l	0.78	0.8	0.82	0.72	0.75	0.38	0.69	0.4	0.73	0.47	0.76	0.59	0.78	0.84	0.75	0.79
ou8u	0.94	0.81	0.89	0.67	0.85	0.46	0.65	0.15	0.73	0.25	0.81	0.52	0.87	0.76	0.79	0.68
ou8l	0.91	0.87	0.8	0.63	0.84	0.56	0.61	0.18	0.7	0.31	0.73	0.6	0.76	0.75	0.77	0.7
nr1u	0.92	0.79	0.87	0.66	0.85	0.43	0.66	0.22	0.71	0.28	0.81	0.54	0.87	0.76	0.8	0.65
nr1l	0.89	0.77	0.86	0.69	0.84	0.41	0.67	0.23	0.68	0.26	0.8	0.55	0.86	0.78	0.76	0.64
nr2u	0.9	0.86	0.87	0.75	0.82	0.46	0.72	0.26	0.79	0.37	0.85	0.58	0.88	0.81	0.81	0.79
nr2l	0.86	0.8	0.88	0.77	0.77	0.37	0.71	0.22	0.71	0.28	0.86	0.52	0.9	0.8	0.75	0.73
CS	0.74	0.67	0.69	0.53	0.69	0.41	0.52	0.24	0.68	0.29	0.64	0.46	0.68	0.66	0.72	0.63
MCS	0.18	0.19	0.16	0.31	0.07	0.23	-0.07	0.09	0.24	0.03	0.1	0.23	0.16	0.35	0.33	0.28
ML	0.15	0.18	0.15	0.3	0.06	0.25	-0.08	0.09	0.19	0.05	0.08	0.22	0.12	0.34	0.3	0.28
IT	0.23	0.39	0.18	0.21	0.21	0.22	0.35	0.21	0.35	0.36	0.37	0.31	0.2	0.16	0.26	0.37
FWL	-0.01	0	0	0	-0.02	-0.01	-0.01	-0.01	0	0	0	-0.01	-0.01	0	-0.01	0.01
FWF	-0.02	-0.02	-0.01	0	-0.02	-0.01	-0.02	0	-0.01	0	-0.01	-0.01	-0.01	-0.01	-0.01	0
FNL	-0.01	-0.02	-0.01	-0.01	-0.02	0	-0.02	-0.01	-0.01	-0.02	-0.01	-0.01	-0.01	-0.01	-0.01	0
FNR	-0.01	-0.01	0	0	0.01	-0.02	0	-0.01	0	0	-0.01	0	0	0.01	0	0.01
DWL	0.67	0.78	0.66	0.65	0.63	0.38	0.62	0.23	0.79	0.39	0.69	0.51	0.63	0.69	0.71	0.84
DWF	0.57	0.69	0.54	0.54	0.55	0.33	0.56	0.21	0.77	0.37	0.57	0.47	0.52	0.58	0.64	0.76
DNL	0.81	0.84	0.73	0.59	0.74	0.39	0.59	0.07	0.78	0.22	0.69	0.44	0.68	0.68	0.79	0.81
DNR	0.8	0.82	0.76	0.65	0.72	0.3	0.65	0.06	0.78	0.19	0.73	0.44	0.7	0.74	0.79	0.83
OF	0.75	0.68	0.7	0.54	0.7	0.41	0.53	0.24	0.69	0.3	0.65	0.47	0.68	0.68	0.72	0.64
DC	0.01	0.04	0	0	0.01	0.1	-0.02	0.08	0.03	0.11	0.05	0.04	0.03	-0.03	0.04	0.05
HWL	0.66	0.77	0.65	0.64	0.62	0.37	0.6	0.22	0.78	0.38	0.68	0.5	0.62	0.68	0.71	0.84
HWF	0.57	0.68	0.54	0.53	0.54	0.32	0.55	0.19	0.76	0.36	0.56	0.46	0.52	0.58	0.64	0.76
HNL	0.81	0.83	0.72	0.59	0.74	0.39	0.59	0.07	0.78	0.22	0.69	0.44	0.68	0.68	0.79	0.81
HNR	0.8	0.82	0.76	0.65	0.72	0.3	0.65	0.06	0.78	0.19	0.73	0.44	0.7	0.74	0.79	0.83
in1	-0.85	-0.52	-0.78	-0.45	-0.76	-0.28	-0.52	-0.03	-0.53	-0.08	-0.65	-0.35	-0.78	-0.53	-0.62	-0.36
in2	-0.69	-0.45	-0.7	-0.18	-0.75	-0.17	-0.49	0.02	-0.45	-0.07	-0.53	-0.17	-0.62	-0.32	-0.5	-0.28
in3	-0.66	-0.48	-0.73	-0.42	-0.79	0.11	-0.79	0.03	-0.55	-0.02	-0.62	-0.15	-0.65	-0.5	-0.39	-0.38
in4	-0.58	-0.5	-0.61	-0.44	-0.59	0.18	-0.83	0.28	-0.48	0.17	-0.6	-0.06	-0.55	-0.47	-0.31	-0.43
in5	-0.56	-0.48	-0.53	-0.39	-0.48	0.04	-0.47	0.37	-0.61	0.35	-0.47	0	-0.49	-0.42	-0.45	-0.45
in6	-0.48	-0.39	-0.52	-0.34	-0.43	0.13	-0.52	0.2	-0.36	0.17	-0.67	0.25	-0.5	-0.27	-0.31	-0.45
in7	-0.66	-0.44	-0.66	-0.34	-0.63	-0.26	-0.47	-0.11	-0.47	-0.17	-0.67	-0.24	-0.74	-0.28	-0.55	-0.3
in8	-0.25	-0.03	-0.19	0.03	-0.21	-0.25	0.06	-0.12	-0.18	-0.14	-0.12	-0.34	-0.24	0	-0.45	0.21
n11	0.23	0.1	0.27	0.09	0.26	-0.01	0.14	0.07	0.2	0.06	0.24	0.07	0.24	0.13	0.29	0.09
n12	-0.44	-0.38	-0.34	-0.16	-0.35	-0.33	-0.14	-0.04	-0.27	-0.15	-0.33	-0.21	-0.34	-0.22	-0.45	-0.34
ou1	-0.63	-0.39	-0.61	-0.29	-0.54	-0.22	-0.34	0	-0.36	-0.04	-0.57	-0.16	-0.63	-0.29	-0.5	-0.23
ou2	-0.66	-0.54	-0.63	-0.5	-0.61	-0.34	-0.54	-0.07	-0.53	-0.14	-0.75	-0.28	-0.71	-0.39	-0.54	-0.42
ou3	-0.58	-0.55	-0.6	-0.55	-0.51	-0.26	-0.5	-0.1	-0.55	-0.14	-0.73	-0.21	-0.69	-0.44	-0.56	-0.53
ou4	-0.63	-0.59	-0.61	-0.55	-0.54	-0.04	-0.61	0.29	-0.47	0.21	-0.67	-0.03	-0.61	-0.51	-0.38	-0.57
ou5	-0.35	-0.28	-0.2	-0.08	-0.19	-0.06	-0.1	0.45	-0.02	0.37	-0.35	0.24	-0.24	-0.01	-0.16	-0.21
ou6	-0.58	-0.52	-0.59	-0.56	-0.45	-0.15	-0.48	0.15	-0.43	0.08	-0.64	-0.18	-0.65	-0.45	-0.47	-0.46
ou7	-0.52	-0.32	-0.5	-0.2	-0.49	-0.32	-0.22	0.01</td								

**Table C.2** Correlation of input variables.

	n11u	n11l	n12u	n12l	ou1u	ou1l	ou2u	ou2l	ou3u	ou3l	ou4u	ou4l	ou5u	ou5l	ou6u	ou6l
in1u	<b>0.86</b>	<b>0.85</b>	<b>0.86</b>	<b>0.81</b>	<b>0.93</b>	<b>0.8</b>	<b>0.9</b>	<b>0.69</b>	<b>0.84</b>	<b>0.72</b>	<b>0.72</b>	<b>0.12</b>	<b>0.61</b>	<b>0.14</b>	<b>0.86</b>	<b>0.79</b>
in1l	<b>0.75</b>	<b>0.72</b>	<b>0.72</b>	<b>0.68</b>	<b>0.85</b>	<b>0.86</b>	<b>0.85</b>	<b>0.72</b>	<b>0.82</b>	<b>0.72</b>	<b>0.74</b>	<b>0.19</b>	<b>0.61</b>	<b>0.21</b>	<b>0.8</b>	<b>0.76</b>
in2u	<b>0.87</b>	<b>0.88</b>	<b>0.82</b>	<b>0.81</b>	<b>0.88</b>	<b>0.76</b>	<b>0.91</b>	<b>0.74</b>	<b>0.87</b>	<b>0.74</b>	<b>0.71</b>	<b>0.12</b>	<b>0.63</b>	<b>0.31</b>	<b>0.87</b>	<b>0.8</b>
in2l	<b>0.73</b>	<b>0.7</b>	<b>0.61</b>	<b>0.63</b>	<b>0.72</b>	<b>0.76</b>	<b>0.76</b>	<b>0.65</b>	<b>0.79</b>	<b>0.67</b>	<b>0.54</b>	<b>-0.02</b>	<b>0.5</b>	<b>0.31</b>	<b>0.82</b>	<b>0.75</b>
in3u	<b>0.8</b>	<b>0.82</b>	<b>0.78</b>	<b>0.76</b>	<b>0.82</b>	<b>0.72</b>	<b>0.88</b>	<b>0.71</b>	<b>0.84</b>	<b>0.79</b>	<b>0.74</b>	<b>0.26</b>	<b>0.65</b>	<b>0.33</b>	<b>0.8</b>	<b>0.8</b>
in3l	<b>0.37</b>	<b>0.34</b>	<b>0.34</b>	<b>0.28</b>	<b>0.5</b>	<b>0.51</b>	<b>0.47</b>	<b>0.37</b>	<b>0.5</b>	<b>0.5</b>	<b>0.27</b>	<b>0.29</b>	<b>0.17</b>	<b>0.07</b>	<b>0.36</b>	<b>0.41</b>
in4u	<b>0.73</b>	<b>0.71</b>	<b>0.6</b>	<b>0.63</b>	<b>0.65</b>	<b>0.63</b>	<b>0.78</b>	<b>0.63</b>	<b>0.76</b>	<b>0.68</b>	<b>0.81</b>	<b>0.25</b>	<b>0.81</b>	<b>0.55</b>	<b>0.78</b>	<b>0.76</b>
in4l	<b>0.23</b>	<b>0.23</b>	<b>0.18</b>	<b>0.19</b>	<b>0.13</b>	<b>0.18</b>	<b>0.37</b>	<b>0.46</b>	<b>0.4</b>	<b>0.51</b>	<b>0.25</b>	<b>0.69</b>	<b>0.24</b>	<b>0.63</b>	<b>0.15</b>	<b>0.35</b>
in5u	<b>0.69</b>	<b>0.7</b>	<b>0.65</b>	<b>0.64</b>	<b>0.73</b>	<b>0.73</b>	<b>0.81</b>	<b>0.68</b>	<b>0.8</b>	<b>0.69</b>	<b>0.7</b>	<b>0.29</b>	<b>0.54</b>	<b>0.41</b>	<b>0.73</b>	<b>0.72</b>
in5l	<b>0.27</b>	<b>0.27</b>	<b>0.21</b>	<b>0.19</b>	<b>0.26</b>	<b>0.32</b>	<b>0.43</b>	<b>0.49</b>	<b>0.42</b>	<b>0.51</b>	<b>0.39</b>	<b>0.76</b>	<b>0.36</b>	<b>0.64</b>	<b>0.21</b>	<b>0.39</b>
in6u	<b>0.81</b>	<b>0.82</b>	<b>0.77</b>	<b>0.75</b>	<b>0.86</b>	<b>0.75</b>	<b>0.92</b>	<b>0.65</b>	<b>0.87</b>	<b>0.63</b>	<b>0.82</b>	<b>0.19</b>	<b>0.73</b>	<b>0.24</b>	<b>0.85</b>	<b>0.72</b>
in6l	<b>0.53</b>	<b>0.51</b>	<b>0.45</b>	<b>0.44</b>	<b>0.55</b>	<b>0.63</b>	<b>0.56</b>	<b>0.54</b>	<b>0.59</b>	<b>0.69</b>	<b>0.32</b>	<b>0.37</b>	<b>0.3</b>	<b>0.48</b>	<b>0.51</b>	<b>0.61</b>
in7u	<b>0.87</b>	<b>0.87</b>	<b>0.82</b>	<b>0.8</b>	<b>0.87</b>	<b>0.73</b>	<b>0.93</b>	<b>0.69</b>	<b>0.9</b>	<b>0.71</b>	<b>0.69</b>	<b>0.1</b>	<b>0.62</b>	<b>0.26</b>	<b>0.89</b>	<b>0.78</b>
in7l	<b>0.78</b>	<b>0.75</b>	<b>0.71</b>	<b>0.72</b>	<b>0.75</b>	<b>0.8</b>	<b>0.8</b>	<b>0.79</b>	<b>0.82</b>	<b>0.82</b>	<b>0.58</b>	<b>0.09</b>	<b>0.51</b>	<b>0.39</b>	<b>0.83</b>	<b>0.86</b>
in8u	<b>0.71</b>	<b>0.74</b>	<b>0.79</b>	<b>0.73</b>	<b>0.83</b>	<b>0.77</b>	<b>0.8</b>	<b>0.66</b>	<b>0.74</b>	<b>0.6</b>	<b>0.57</b>	<b>0.24</b>	<b>0.36</b>	<b>0.13</b>	<b>0.66</b>	<b>0.58</b>
in8l	<b>0.61</b>	<b>0.59</b>	<b>0.61</b>	<b>0.58</b>	<b>0.72</b>	<b>0.81</b>	<b>0.77</b>	<b>0.73</b>	<b>0.74</b>	<b>0.61</b>	<b>0.71</b>	<b>0.18</b>	<b>0.54</b>	<b>0.23</b>	<b>0.71</b>	<b>0.67</b>
n11u	<b>I</b>	<b>0.95</b>	<b>0.87</b>	<b>0.88</b>	<b>0.84</b>	<b>0.74</b>	<b>0.85</b>	<b>0.67</b>	<b>0.82</b>	<b>0.73</b>	<b>0.66</b>	<b>0.1</b>	<b>0.6</b>	<b>0.25</b>	<b>0.83</b>	<b>0.79</b>
n11l	<b>0.95</b>	<b>I</b>	<b>0.9</b>	<b>0.92</b>	<b>0.83</b>	<b>0.7</b>	<b>0.86</b>	<b>0.68</b>	<b>0.81</b>	<b>0.71</b>	<b>0.66</b>	<b>0.14</b>	<b>0.57</b>	<b>0.21</b>	<b>0.79</b>	<b>0.75</b>
n12u	<b>0.87</b>	<b>0.9</b>	<b>I</b>	<b>0.96</b>	<b>0.82</b>	<b>0.7</b>	<b>0.83</b>	<b>0.72</b>	<b>0.77</b>	<b>0.69</b>	<b>0.63</b>	<b>0.18</b>	<b>0.48</b>	<b>0.13</b>	<b>0.72</b>	<b>0.7</b>
n12l	<b>0.88</b>	<b>0.92</b>	<b>0.96</b>	<b>I</b>	<b>0.78</b>	<b>0.68</b>	<b>0.81</b>	<b>0.7</b>	<b>0.76</b>	<b>0.7</b>	<b>0.6</b>	<b>0.13</b>	<b>0.48</b>	<b>0.18</b>	<b>0.73</b>	<b>0.71</b>
ou1u	<b>0.84</b>	<b>0.83</b>	<b>0.82</b>	<b>0.78</b>	<b>I</b>	<b>0.87</b>	<b>0.86</b>	<b>0.59</b>	<b>0.79</b>	<b>0.62</b>	<b>0.71</b>	<b>0.07</b>	<b>0.59</b>	<b>0.11</b>	<b>0.84</b>	<b>0.72</b>
ou1l	<b>0.74</b>	<b>0.7</b>	<b>0.68</b>	<b>0.87</b>	<b>I</b>	<b>0.75</b>	<b>0.65</b>	<b>0.72</b>	<b>0.69</b>	<b>0.64</b>	<b>0.08</b>	<b>0.51</b>	<b>0.26</b>	<b>0.78</b>	<b>0.77</b>	
ou2u	<b>0.85</b>	<b>0.86</b>	<b>0.83</b>	<b>0.81</b>	<b>0.86</b>	<b>0.75</b>	<b>I</b>	<b>0.79</b>	<b>0.94</b>	<b>0.75</b>	<b>0.81</b>	<b>0.23</b>	<b>0.67</b>	<b>0.28</b>	<b>0.84</b>	<b>0.78</b>
ou2l	<b>0.67</b>	<b>0.68</b>	<b>0.72</b>	<b>0.7</b>	<b>0.59</b>	<b>0.65</b>	<b>0.79</b>	<b>I</b>	<b>0.73</b>	<b>0.85</b>	<b>0.63</b>	<b>0.46</b>	<b>0.48</b>	<b>0.5</b>	<b>0.59</b>	<b>0.76</b>
ou3u	<b>0.82</b>	<b>0.81</b>	<b>0.77</b>	<b>0.76</b>	<b>0.79</b>	<b>0.72</b>	<b>0.94</b>	<b>0.73</b>	<b>I</b>	<b>0.79</b>	<b>0.74</b>	<b>0.15</b>	<b>0.62</b>	<b>0.3</b>	<b>0.86</b>	<b>0.8</b>
ou3l	<b>0.73</b>	<b>0.71</b>	<b>0.69</b>	<b>0.7</b>	<b>0.62</b>	<b>0.69</b>	<b>0.75</b>	<b>0.85</b>	<b>0.79</b>	<b>I</b>	<b>0.58</b>	<b>0.37</b>	<b>0.51</b>	<b>0.57</b>	<b>0.68</b>	<b>0.89</b>
ou4u	<b>0.66</b>	<b>0.66</b>	<b>0.63</b>	<b>0.6</b>	<b>0.71</b>	<b>0.64</b>	<b>0.81</b>	<b>0.63</b>	<b>0.74</b>	<b>0.58</b>	<b>I</b>	<b>0.39</b>	<b>0.88</b>	<b>0.34</b>	<b>0.71</b>	<b>0.68</b>
ou4l	<b>0.1</b>	<b>0.14</b>	<b>0.18</b>	<b>0.13</b>	<b>0.07</b>	<b>0.08</b>	<b>0.23</b>	<b>0.46</b>	<b>0.15</b>	<b>0.37</b>	<b>0.39</b>	<b>I</b>	<b>0.31</b>	<b>0.62</b>	<b>-0.1</b>	<b>0.18</b>
ou5u	<b>0.6</b>	<b>0.57</b>	<b>0.48</b>	<b>0.48</b>	<b>0.59</b>	<b>0.51</b>	<b>0.67</b>	<b>0.48</b>	<b>0.62</b>	<b>0.51</b>	<b>0.88</b>	<b>0.31</b>	<b>I</b>	<b>0.44</b>	<b>0.69</b>	<b>0.65</b>
ou5l	<b>0.25</b>	<b>0.21</b>	<b>0.13</b>	<b>0.18</b>	<b>0.11</b>	<b>0.26</b>	<b>0.28</b>	<b>0.5</b>	<b>0.3</b>	<b>0.57</b>	<b>0.34</b>	<b>0.62</b>	<b>0.44</b>	<b>I</b>	<b>0.22</b>	<b>0.83</b>
ou6u	<b>0.83</b>	<b>0.79</b>	<b>0.72</b>	<b>0.73</b>	<b>0.84</b>	<b>0.78</b>	<b>0.84</b>	<b>0.59</b>	<b>0.86</b>	<b>0.68</b>	<b>0.71</b>	<b>-0.1</b>	<b>0.69</b>	<b>0.22</b>	<b>I</b>	<b>0.83</b>
ou6l	<b>0.79</b>	<b>0.75</b>	<b>0.7</b>	<b>0.71</b>	<b>0.72</b>	<b>0.77</b>	<b>0.78</b>	<b>0.76</b>	<b>0.8</b>	<b>0.89</b>	<b>0.68</b>	<b>0.18</b>	<b>0.65</b>	<b>0.5</b>	<b>0.83</b>	<b>I</b>
ou7u	<b>0.8</b>	<b>0.82</b>	<b>0.82</b>	<b>0.78</b>	<b>0.87</b>	<b>0.71</b>	<b>0.91</b>	<b>0.74</b>	<b>0.83</b>	<b>0.7</b>	<b>0.75</b>	<b>0.27</b>	<b>0.61</b>	<b>0.28</b>	<b>0.79</b>	<b>0.76</b>
ou7l	<b>0.76</b>	<b>0.77</b>	<b>0.8</b>	<b>0.77</b>	<b>0.72</b>	<b>0.75</b>	<b>0.84</b>	<b>0.94</b>	<b>0.78</b>	<b>0.84</b>	<b>0.71</b>	<b>0.41</b>	<b>0.55</b>	<b>0.46</b>	<b>0.68</b>	<b>0.8</b>
ou8u	<b>0.84</b>	<b>0.85</b>	<b>0.86</b>	<b>0.83</b>	<b>0.91</b>	<b>0.78</b>	<b>0.86</b>	<b>0.68</b>	<b>0.77</b>	<b>0.69</b>	<b>0.68</b>	<b>0.1</b>	<b>0.57</b>	<b>0.16</b>	<b>0.82</b>	<b>0.79</b>
ou8l	<b>0.79</b>	<b>0.78</b>	<b>0.77</b>	<b>0.84</b>	<b>0.84</b>	<b>0.79</b>	<b>0.71</b>	<b>0.73</b>	<b>0.76</b>	<b>0.65</b>	<b>0.18</b>	<b>0.53</b>	<b>0.19</b>	<b>0.75</b>	<b>0.8</b>	<b>0.79</b>
nr1u	<b>0.89</b>	<b>0.89</b>	<b>0.91</b>	<b>0.9</b>	<b>0.87</b>	<b>0.76</b>	<b>0.87</b>	<b>0.72</b>	<b>0.82</b>	<b>0.73</b>	<b>0.67</b>	<b>0.16</b>	<b>0.55</b>	<b>0.2</b>	<b>0.8</b>	<b>0.79</b>
nr1l	<b>0.89</b>	<b>0.89</b>	<b>0.91</b>	<b>0.91</b>	<b>0.84</b>	<b>0.76</b>	<b>0.85</b>	<b>0.72</b>	<b>0.81</b>	<b>0.75</b>	<b>0.64</b>	<b>0.13</b>	<b>0.55</b>	<b>0.22</b>	<b>0.81</b>	<b>0.8</b>
nr2u	<b>0.87</b>	<b>0.84</b>	<b>0.82</b>	<b>0.8</b>	<b>0.87</b>	<b>0.81</b>	<b>0.88</b>	<b>0.73</b>	<b>0.83</b>	<b>0.71</b>	<b>0.73</b>	<b>0.16</b>	<b>0.63</b>	<b>0.3</b>	<b>0.86</b>	<b>0.81</b>
nr2l	<b>0.89</b>	<b>0.86</b>	<b>0.83</b>	<b>0.85</b>	<b>0.77</b>	<b>0.87</b>	<b>0.87</b>	<b>0.68</b>	<b>0.84</b>	<b>0.67</b>	<b>0.71</b>	<b>0.09</b>	<b>0.63</b>	<b>0.24</b>	<b>0.86</b>	<b>0.77</b>
CS	<b>0.73</b>	<b>0.72</b>	<b>0.76</b>	<b>0.72</b>	<b>0.69</b>	<b>0.69</b>	<b>0.68</b>	<b>0.62</b>	<b>0.67</b>	<b>0.53</b>	<b>0.2</b>	<b>0.4</b>	<b>0.29</b>	<b>0.64</b>	<b>0.73</b>	
MCS	<b>0.21</b>	<b>0.2</b>	<b>0.26</b>	<b>0.27</b>	<b>0.22</b>	<b>0.32</b>	<b>0.12</b>	<b>0.24</b>	<b>0.11</b>	<b>0.26</b>	<b>-0.14</b>	<b>-0.15</b>	<b>-0.25</b>	<b>0</b>	<b>0.15</b>	<b>0.29</b>
ML	<b>0.17</b>	<b>0.15</b>	<b>0.2</b>	<b>0.2</b>	<b>0.22</b>	<b>0.31</b>	<b>0.09</b>	<b>0.25</b>	<b>0.07</b>	<b>0.24</b>	<b>-0.11</b>	<b>-0.09</b>	<b>-0.22</b>	<b>0.03</b>	<b>0.12</b>	<b>0.27</b>
IT	<b>0.12</b>	<b>0.09</b>	<b>0.06</b>	<b>0.04</b>	<b>0.22</b>	<b>0.32</b>	<b>0.29</b>	<b>0.16</b>	<b>0.3</b>	<b>0.15</b>	<b>0.44</b>	<b>0.24</b>	<b>0.41</b>	<b>0.19</b>	<b>0.22</b>	<b>0.13</b>
FWL	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0.01</b>	<b>0.01</b>	<b>0</b>	<b>-0.01</b>	<b>-0.01</b>	<b>0.01</b>	<b>0</b>	<b>0.01</b>	<b>-0.01</b>	<b>0</b>	<b>-0.02</b>	<b>-0.02</b>
FWF	<b>-0.01</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.01</b>
FNL	<b>-0.01</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.01</b>
FNR	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0.01</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>-0.01</b>	<b>-0.02</b>	<b>-0.01</b>	<b>-0.01</b>	<b>0</b>	<b>0.01</b>
DWL	<b>0.57</b>	<b>0.54</b>	<b>0.52</b>	<b>0.52</b>	<b>0.66</b>	<b>0.77</b>	<b>0.69</b>	<b>0.67</b>	<b>0.65</b>	<b>0.57</b>	<b>0.64</b>	<b>0.17</b>	<b>0.5</b>	<b>0.37</b>	<b>0.67</b>	<b>0.65</b>
DWF	<b>0.47</b>	<b>0.44</b>	<b>0.41</b>	<b>0.42</b>	<b>0.56</b>	<b>0.7</b>	<b>0.58</b>	<b>0.59</b>	<b>0.55</b>	<b>0.51</b>	<b>0.53</b>	<b>0.15</b>	<b>0.41</b>	<b>0.4</b>	<b>0.58</b>	<b>0.57</b>
DNL	<b>0.69</b>	<b>0.7</b>	<b>0.72</b>	<b>0.69</b>	<b>0.75</b>	<b>0.78</b>	<b>0.75</b>	<b>0.72</b>	<b>0.69</b>	<b>0.64</b>	<b>0.65</b>	<b>0.12</b>	<b>0.44</b>	<b>0.16</b>	<b>0.69</b>	<b>0.69</b>
DNR	<b>0.73</b>	<b>0.75</b>	<b>0.76</b>	<b>0.77</b>	<b>0.82</b>	<b>0.78</b>	<b>0.76</b>	<b>0.72</b>	<b>0.66</b>	<b>0.68</b>	<b>0.5</b>	<b>0.48</b>	<b>0.2</b>	<b>0.72</b>	<b>0.72</b>	
OF	<b>0.73</b>	<b>0.73</b>	<b>0.77</b>	<b>0.73</b>	<b>0.7</b>	<b>0.69</b>	<b>0.63</b>	<b>0.68</b>	<b>0.55</b>	<b>0.21</b>	<b>0.41</b>	<b>0.3</b>	<b>0.65</b>	<b>0.74</b>		
DC	<b>-0.03</b>	<b>-0.02</b>	<b>-0.04</b>	<b>-0.04</b>	<b>0.01</b>	<b>-0.01</b>	<b>0.03</b>	<b>-0</b>								

**Table C.3** Correlation of input variables.

	ou7u	ou7l	ou8u	ou8l	nr1u	nr1l	nr2u	nr2l	CS	MCS	ML	IT	FWL	FWF	FNL	FNR
in1u	0.9	0.78	0.94	0.91	0.92	0.89	0.9	0.86	0.74	0.18	0.15	0.23	-0.01	-0.02	-0.01	-0.01
in1l	0.8	0.8	0.81	0.87	0.79	0.77	0.86	0.8	0.67	0.19	0.18	0.39	0	-0.02	-0.02	-0.01
in2u	0.92	0.82	0.89	0.8	0.87	0.86	0.87	0.88	0.69	0.16	0.15	0.18	0	-0.01	-0.01	0
in2l	0.67	0.72	0.67	0.63	0.66	0.69	0.75	0.77	0.53	0.31	0.3	0.21	0	-0.01	-0.01	0.01
in3u	0.86	0.75	0.85	0.84	0.85	0.84	0.82	0.77	0.69	0.07	0.06	0.21	-0.02	-0.02	-0.02	-0.02
in3l	0.48	0.38	0.46	0.56	0.43	0.41	0.46	0.37	0.41	0.23	0.25	0.22	-0.01	-0.01	0	0
in4u	0.66	0.69	0.65	0.61	0.66	0.67	0.72	0.71	0.52	-0.07	-0.08	0.35	-0.01	-0.02	-0.02	-0.01
in4l	0.3	0.4	0.15	0.18	0.22	0.23	0.26	0.22	0.24	0.09	0.09	0.21	-0.01	0	-0.01	0
in5u	0.77	0.73	0.73	0.7	0.71	0.68	0.79	0.71	0.68	0.24	0.19	0.35	0	-0.01	-0.01	0
in5l	0.41	0.47	0.25	0.31	0.28	0.26	0.37	0.28	0.29	0.03	0.05	0.36	0	0	-0.02	-0.01
in6u	0.85	0.76	0.81	0.73	0.81	0.8	0.85	0.86	0.64	0.1	0.08	0.37	0	-0.01	-0.01	0
in6l	0.55	0.59	0.52	0.6	0.54	0.55	0.58	0.52	0.46	0.23	0.22	0.31	-0.01	-0.01	-0.01	0
in7u	0.91	0.78	0.87	0.76	0.87	0.86	0.88	0.9	0.68	0.16	0.12	0.2	-0.01	-0.01	-0.01	0
in7l	0.75	0.84	0.76	0.75	0.76	0.78	0.81	0.8	0.66	0.35	0.34	0.16	0	-0.01	-0.01	0.01
in8u	0.82	0.75	0.79	0.77	0.8	0.76	0.81	0.75	0.72	0.33	0.3	0.26	-0.01	-0.01	-0.01	0
in8l	0.72	0.79	0.68	0.7	0.65	0.64	0.79	0.73	0.63	0.28	0.28	0.37	0.01	0	0	0.01
nl1u	0.8	0.76	0.84	0.79	0.89	0.89	0.87	0.89	0.73	0.21	0.17	0.12	0	-0.01	-0.01	0
nl1l	0.82	0.77	0.85	0.78	0.89	0.89	0.84	0.86	0.72	0.2	0.15	0.09	0	-0.02	-0.02	0
nl2u	0.82	0.8	0.86	0.81	0.91	0.91	0.82	0.83	0.77	0.26	0.2	0.06	0	-0.02	-0.02	0
nl2l	0.78	0.77	0.83	0.77	0.9	0.91	0.8	0.83	0.76	0.27	0.2	0.04	0	-0.02	-0.02	0
ou1u	0.87	0.72	0.91	0.84	0.87	0.84	0.87	0.85	0.72	0.22	0.22	0.22	0.01	-0.02	-0.02	0
ou1l	0.71	0.75	0.78	0.83	0.76	0.76	0.81	0.77	0.69	0.32	0.31	0.32	0.01	-0.01	-0.02	0.01
ou2u	0.91	0.84	0.86	0.79	0.87	0.85	0.88	0.87	0.69	0.12	0.09	0.29	0	-0.02	-0.01	0
ou2l	0.74	0.94	0.68	0.71	0.72	0.72	0.73	0.68	0.68	0.24	0.25	0.16	0	-0.02	-0.02	0
ou3u	0.83	0.78	0.77	0.73	0.8	0.81	0.83	0.84	0.62	0.11	0.07	0.3	-0.01	-0.02	-0.02	0
ou3l	0.7	0.84	0.69	0.76	0.73	0.75	0.71	0.67	0.67	0.26	0.24	0.15	-0.01	-0.01	-0.02	0
ou4u	0.75	0.71	0.68	0.65	0.67	0.64	0.73	0.71	0.53	-0.14	-0.11	0.44	0.01	-0.02	-0.01	-0.01
ou4l	0.27	0.41	0.1	0.18	0.16	0.13	0.16	0.09	0.2	-0.15	-0.09	0.24	0	-0.01	-0.02	-0.02
ou5u	0.61	0.55	0.57	0.53	0.55	0.55	0.63	0.63	0.4	-0.25	-0.22	0.41	0.01	-0.02	-0.01	-0.01
ou5l	0.28	0.46	0.16	0.19	0.2	0.22	0.3	0.24	0.29	0	0.03	0.19	-0.01	0	-0.01	-0.01
ou6u	0.79	0.68	0.82	0.75	0.8	0.81	0.86	0.86	0.64	0.15	0.12	0.22	0	-0.02	-0.02	0
ou6l	0.76	0.8	0.79	0.8	0.79	0.8	0.81	0.77	0.73	0.29	0.27	0.13	0	-0.02	-0.01	0.01
ou7u	<i>I</i>	0.82	0.91	0.81	0.87	0.84	0.88	0.85	0.76	0.17	0.15	0.18	0	-0.02	-0.01	0
ou7l	0.82	<i>I</i>	0.77	0.8	0.79	0.81	0.77	0.71	0.22	0.22	0.25	0	0	-0.01	-0.02	0
ou8u	0.91	0.77	<i>I</i>	0.91	0.92	0.89	0.87	0.84	0.8	0.29	0.26	0.11	0	-0.02	-0.01	-0.01
ou8l	0.81	0.8	0.91	<i>I</i>	0.86	0.85	0.82	0.76	0.75	0.24	0.22	0.25	0	-0.01	-0.02	-0.01
nr1u	0.87	0.8	0.92	0.86	<i>I</i>	0.97	0.9	0.89	0.83	0.29	0.24	0.1	0	-0.01	-0.02	0.01
nr1l	0.84	0.79	0.89	0.85	0.97	<i>I</i>	0.88	0.89	0.81	0.29	0.23	0.1	-0.01	-0.02	-0.02	0.01
nr2u	0.88	0.81	0.87	0.82	0.9	0.88	<i>I</i>	0.94	0.8	0.27	0.23	0.22	0	-0.02	-0.03	0
nr2l	0.85	0.77	0.84	0.76	0.89	0.89	0.94	<i>I</i>	0.74	0.2	0.15	0.2	-0.01	-0.02	-0.02	0.01
CS	0.76	0.71	0.8	0.75	0.83	0.81	0.8	0.74	<i>I</i>	0.58	0.54	-0.09	-0.01	-0.02	-0.01	0
MCS	0.17	0.22	0.29	0.24	0.29	0.29	0.27	0.2	0.58	<i>I</i>	0.89	-0.45	0.01	0	0	0.02
ML	0.15	0.22	0.26	0.22	0.24	0.23	0.23	0.15	0.54	0.89	<i>I</i>	-0.49	0.02	0	0.02	0.02
IT	0.18	0.25	0.11	0.25	0.1	0.22	0.2	-0.09	-0.45	-0.49	<i>I</i>	0	0	-0.01	0	0
FWL	0	0	0	0	-0.01	0	-0.01	-0.01	0.01	0.02	0	<i>I</i>	-0.29	-0.11	-0.06	
FWF	-0.02	-0.01	-0.02	-0.01	-0.01	-0.02	-0.02	-0.02	-0.02	0	0	0	-0.29	<i>I</i>	0.06	0.28
FNL	-0.01	-0.02	-0.01	-0.02	-0.02	-0.02	-0.03	-0.02	-0.01	0	0.02	-0.01	-0.11	0.06	<i>I</i>	0.23
FNR	0	0	-0.01	-0.01	0.01	0.01	0	0.01	0	0.02	0.02	0	-0.06	0.28	0.23	<i>I</i>
DWL	0.68	0.72	0.65	0.66	0.62	0.6	0.76	0.69	0.66	0.27	0.22	0.44	0	0	-0.01	0.01
DWF	0.58	0.61	0.55	0.57	0.52	0.5	0.68	0.58	0.61	0.29	0.23	0.41	0.01	-0.01	-0.01	0
DNL	0.75	0.78	0.79	0.83	0.76	0.73	0.8	0.73	0.74	0.29	0.24	0.28	0	-0.01	0	0
DNR	0.75	0.83	0.79	0.81	0.78	0.76	0.82	0.77	0.74	0.3	0.26	0.28	0.01	-0.01	0	0.01
OF	0.77	0.72	0.81	0.76	0.84	0.82	0.81	0.75	<i>I</i>	0.57	0.54	-0.09	0	-0.02	-0.01	0
DC	0.03	-0.02	-0.02	-0.02	-0.02	-0.02	0.02	0.02	-0.04	-0.07	-0.07	0.1	0.03	-0.02	0.01	0.01
HWL	0.68	0.71	0.65	0.66	0.62	0.6	0.76	0.68	0.67	0.3	0.25	0.42	0.06	-0.02	-0.02	0.01
HWF	0.57	0.61	0.55	0.57	0.52	0.5	0.68	0.58	0.62	0.31	0.26	0.39	-0.01	0.05	-0.01	0.02
HNL	0.75	0.78	0.79	0.83	0.76	0.73	0.8	0.73	0.74	0.29	0.24	0.28	-0.01	-0.01	0.04	0.01
HNR	0.75	0.83	0.79	0.81	0.78	0.76	0.82	0.77	0.74	0.3	0.26	0.28	0	0	0.01	0.04
in1	-0.77	-0.54	-0.84	-0.7	-0.81	-0.78	-0.7	-0.69	-0.62	-0.12	-0.07	0.03	0.01	0.01	0	0.01
in2	-0.76	-0.52	-0.71	-0.6	-0.68	-0.63	-0.57	-0.56	-0.53	0.11	0.12	-0.05	0.01	0.02	0.02	0.02
in3	-0.66	-0.61	-0.67	-0.57	-0.68	-0.69	-0.63	-0.64	-0.52	0.08	0.11	-0.08	0.02	0.02	0.02	0.02
in4	-0.49	-0.46	-0.57	-0.51	-0.54	-0.54	-0.57	-0.59	-0.38	0.12	0.13	-0.23	0	0.02	0.01	0.01
in5	-0.47	-0.37	-0.57	-0.49	-0.52	-0.5	-0.52	-0.52	-0.47	-0.23	-0.17	-0.06	0	0.02	0	-0.01
in6	-0.5	-0.35	-0.48	-0.32	-0.46	-0.44	-0.47	-0.53	-0.33	0.1	0.1	-0.15	0	0.01	0	0
in7	-0.71	-0.35	-0.62	-0.44	-0.62	-0.58	-0.58	-0.61	-0.39	0.17	0.22	-0.16	0.03	0.01	0	0.01
in8	-0.24	-0.04	-0.27	-0.19	-0.31	-0.27	-0.14	-0.13	-0.22	-0.12	-0.08	0.13	0.03	0.01	0.02	0.02
nl1	0.29	0.25	0.27	0.21	0.26	0.26	0.13	0.16	0.18	0.01	-0.02	-0.07	0.01	-0.02	-0.04	-0.02
nl2	-0.42	-0.36	-0.41	-0.43	-0.38	-0.32	-0.34	-0.29	-0.29	-0.04	-0.08	-0.08	0.01	0	0.01	0.01
ou1	-0.65	-0.31	-0.64	-0.44	-0.6	-0.54	-0.51	-0.54	-0.4	0.04	0.03	0.04	0.01	0.02	0	0
ou2	-0.62	-0.29	-0.61	-0.47	-0.58	-0.56	-0.59	-0.62	-0.35	0.09	0.13	-0.29	0.01	0.02	-0.01	0
ou3	-0.58	-0.36	-0.5	-0.35	-0.51	-0.49	-0.57	-0.62	-0.29	0.1	0.14	-0.32	0	0.02	0.01	0
ou4	-0.53	-0.39	-0.6	-0.51	-0.54	-0.54	-0.6	-0.64	-0.37	0.02	0.04	-0.25	-0.01	0	0	-0.01
ou5	-0.21	0.02	-0.31	-0.24	-0.25	-0.22	-0.22	-0.27	-0.03	0.21	0.21	-0.14	-0.02	0.01	0	0
ou6	-0.5	-0.25	-0.51	-0.38	-0.48	-0.48	-0.56	-0.61	-0.28	0.08	0.11	-0.23	0	0.01	0.02	0.01
ou7	-0.64	-0.08	-0.54	-0.32	-0.44	-0.39	-0.44	-0.43	-0.36	0.01	0.03	0.02	0	0.02	0	0.01
ou8	-0.67	-0.38	-0.72	-0.35	-0.62	-0.56	-0.58	-0.6	-0.55	-0.23	-0.18	-0.01	0			

**Table C.4** Correlation of input variables.

	DWL	DWF	DNL	DNR	OF	DC	HWL	HWF	HNL	HNR	in1	in2	in3	in4	in5	in6
in1u	0.67	0.57	0.81	0.8	0.75	0.01	0.66	0.57	0.81	0.8	-0.85	-0.69	-0.66	-0.58	-0.56	-0.48
in1l	0.78	0.69	0.84	0.82	0.68	0.04	0.77	0.68	0.83	0.82	-0.52	-0.45	-0.48	-0.5	-0.48	-0.39
in2u	0.66	0.54	0.73	0.76	0.7	0	0.65	0.54	0.72	0.76	-0.78	-0.7	-0.73	-0.61	-0.53	-0.52
in2l	0.65	0.54	0.59	0.65	0.54	0	0.64	0.53	0.59	0.65	-0.45	-0.18	-0.42	-0.44	-0.39	-0.34
in3u	0.63	0.55	0.74	0.72	0.7	0.01	0.62	0.54	0.74	0.72	-0.76	-0.75	-0.79	-0.59	-0.48	-0.43
in3l	0.38	0.33	0.39	0.3	0.41	0.1	0.37	0.32	0.39	0.3	-0.28	-0.17	0.11	0.18	0.04	0.13
in4u	0.62	0.56	0.59	0.65	0.53	-0.02	0.6	0.55	0.59	0.65	-0.52	-0.49	-0.79	-0.83	-0.47	-0.52
in4l	0.23	0.21	0.07	0.06	0.24	0.08	0.22	0.19	0.07	0.06	-0.03	0.02	0.03	0.28	0.37	0.2
in5u	0.79	0.77	0.78	0.78	0.69	0.03	0.78	0.76	0.78	0.78	-0.53	-0.45	-0.55	-0.48	-0.61	-0.36
in5l	0.39	0.37	0.22	0.19	0.3	0.11	0.38	0.36	0.22	0.19	-0.08	-0.07	-0.02	0.17	0.35	0.17
in6u	0.69	0.57	0.69	0.73	0.65	0.05	0.68	0.56	0.69	0.73	-0.65	-0.53	-0.62	-0.6	-0.47	-0.67
in6l	0.51	0.47	0.44	0.44	0.47	0.04	0.5	0.46	0.44	0.44	-0.35	-0.17	-0.15	-0.06	0	0.25
in7u	0.63	0.52	0.68	0.7	0.68	0.03	0.62	0.52	0.68	0.7	-0.78	-0.62	-0.65	-0.55	-0.49	-0.5
in7l	0.69	0.58	0.68	0.74	0.68	-0.03	0.68	0.58	0.68	0.74	-0.53	-0.32	-0.5	-0.47	-0.42	-0.27
in8u	0.71	0.64	0.79	0.79	0.72	0.04	0.71	0.64	0.79	0.79	-0.62	-0.5	-0.39	-0.31	-0.45	-0.31
in8l	0.84	0.76	0.81	0.83	0.64	0.05	0.84	0.76	0.81	0.83	-0.36	-0.28	-0.38	-0.43	-0.45	-0.45
n11u	0.57	0.47	0.69	0.73	0.73	-0.03	0.56	0.46	0.69	0.73	-0.75	-0.59	-0.67	-0.6	-0.51	-0.47
n11l	0.54	0.44	0.7	0.75	0.73	-0.02	0.53	0.43	0.69	0.75	-0.78	-0.65	-0.71	-0.58	-0.51	-0.49
n12u	0.52	0.41	0.72	0.77	0.77	-0.04	0.52	0.41	0.72	0.77	-0.78	-0.67	-0.66	-0.5	-0.52	-0.49
n12l	0.52	0.42	0.69	0.76	0.77	-0.04	0.52	0.42	0.69	0.76	-0.75	-0.62	-0.68	-0.52	-0.52	-0.48
ou1u	0.66	0.56	0.75	0.77	0.73	0.01	0.66	0.56	0.75	0.77	-0.76	-0.62	-0.59	-0.57	-0.56	-0.5
ou1l	0.77	0.7	0.78	0.82	0.7	-0.01	0.77	0.7	0.78	0.82	-0.52	-0.36	-0.47	-0.53	-0.51	-0.31
ou2u	0.69	0.58	0.75	0.78	0.7	0.03	0.68	0.57	0.75	0.77	-0.71	-0.62	-0.68	-0.57	-0.49	-0.57
ou2l	0.67	0.59	0.72	0.76	0.69	-0.02	0.67	0.58	0.72	0.76	-0.47	-0.47	-0.56	-0.36	-0.29	-0.27
ou3u	0.65	0.55	0.69	0.72	0.63	0.03	0.64	0.54	0.69	0.72	-0.63	-0.51	-0.63	-0.53	-0.49	-0.49
ou3l	0.57	0.51	0.64	0.66	0.68	-0.04	0.57	0.51	0.64	0.66	-0.52	-0.44	-0.56	-0.38	-0.29	-0.11
ou4u	0.64	0.53	0.65	0.68	0.55	0.05	0.62	0.52	0.65	0.68	-0.5	-0.55	-0.67	-0.67	-0.41	-0.67
ou4l	0.17	0.15	0.12	0.1	0.21	0.07	0.16	0.15	0.12	0.1	0	-0.23	-0.09	0.15	0.39	0.12
ou5u	0.5	0.41	0.44	0.48	0.41	0.06	0.48	0.39	0.44	0.48	-0.45	-0.47	-0.64	-0.67	-0.26	-0.58
ou5l	0.37	0.4	0.16	0.21	0.3	-0.01	0.36	0.39	0.16	0.2	-0.03	-0.14	-0.34	-0.18	0.15	0.15
ou6u	0.67	0.58	0.69	0.72	0.65	0	0.66	0.57	0.69	0.72	-0.69	-0.49	-0.67	-0.7	-0.6	-0.53
ou6l	0.65	0.57	0.69	0.72	0.74	-0.05	0.64	0.57	0.69	0.72	-0.6	-0.45	-0.64	-0.56	-0.43	-0.29
ou7u	0.68	0.58	0.75	0.75	0.77	0.03	0.68	0.57	0.75	0.75	-0.77	-0.76	-0.66	-0.49	-0.47	-0.5
ou7l	0.72	0.61	0.78	0.83	0.72	-0.02	0.71	0.61	0.78	0.83	-0.54	-0.52	-0.61	-0.46	-0.37	-0.35
ou8u	0.65	0.55	0.79	0.79	0.81	-0.02	0.65	0.55	0.79	0.79	-0.84	-0.71	-0.67	-0.57	-0.57	-0.48
ou8l	0.66	0.57	0.83	0.81	0.76	-0.02	0.66	0.57	0.83	0.81	-0.7	-0.6	-0.57	-0.51	-0.49	-0.32
nrlu	0.62	0.52	0.76	0.78	0.84	-0.02	0.62	0.52	0.76	0.78	-0.81	-0.68	-0.68	-0.54	-0.52	-0.46
nrl1	0.6	0.5	0.73	0.76	0.82	-0.02	0.6	0.5	0.73	0.76	-0.78	-0.63	-0.69	-0.54	-0.5	-0.44
nr2u	0.76	0.68	0.8	0.82	0.81	0.02	0.76	0.67	0.8	0.82	-0.7	-0.57	-0.63	-0.57	-0.52	-0.47
nr2l	0.69	0.58	0.73	0.77	0.75	0.02	0.68	0.57	0.73	0.77	-0.69	-0.56	-0.64	-0.59	-0.52	-0.53
CS	0.66	0.61	0.74	0.74	1	-0.04	0.67	0.62	0.74	0.74	-0.62	-0.53	-0.52	-0.38	-0.47	-0.33
MCS	0.27	0.29	0.29	0.3	0.57	-0.07	0.3	0.31	0.29	0.3	-0.12	0.11	0.08	0.12	0.23	0.1
ML	0.22	0.23	0.24	0.26	0.54	-0.07	0.25	0.26	0.24	0.26	-0.07	0.12	0.11	0.13	-0.17	0.1
IT	0.44	0.41	0.28	0.28	-0.09	0.1	0.42	0.39	0.28	0.28	0.03	-0.05	-0.08	-0.23	-0.06	-0.15
FWL	0	0.01	0	0.01	0	0.03	0.06	-0.01	0	0.01	0.01	0.02	0	0	0	0
FWF	0	-0.01	-0.01	-0.01	-0.02	-0.02	-0.02	0.05	-0.01	0	0.01	0.02	0.02	0.02	0.02	0.01
FNL	-0.01	-0.01	0	0	-0.01	0.01	-0.02	-0.01	0.04	0.01	0	0.02	0.02	0.01	0	0
FNR	0.01	0	0	0.01	0	0.01	0.01	0.02	0.01	0.04	0.01	0.02	0.02	0.01	-0.01	0
DWL	<i>I</i>	<b>0.96</b>	<b>0.87</b>	<b>0.86</b>	<b>0.67</b>	0.04	<i>I</i>	<b>0.96</b>	<b>0.87</b>	<b>0.86</b>	-0.36	-0.33	-0.46	-0.48	-0.5	-0.35
DWF	<b>0.96</b>	<i>I</i>	<b>0.83</b>	<b>0.8</b>	<b>0.62</b>	0.03	<b>0.96</b>	<i>I</i>	<b>0.83</b>	<b>0.8</b>	-0.28	-0.27	-0.41	-0.45	-0.5	-0.24
DNL	<b>0.87</b>	<b>0.83</b>	<i>I</i>	<b>0.96</b>	<b>0.74</b>	-0.02	<b>0.88</b>	<b>0.83</b>	<i>I</i>	<b>0.96</b>	-0.56	-0.52	-0.58	-0.56	-0.66	-0.41
DNR	<b>0.86</b>	<b>0.8</b>	<b>0.96</b>	<i>I</i>	<b>0.75</b>	-0.03	<b>0.86</b>	<b>0.8</b>	<b>0.96</b>	<i>I</i>	-0.56	-0.49	-0.63	-0.62	-0.68	-0.46
OF	<b>0.67</b>	<b>0.62</b>	<b>0.74</b>	<b>0.75</b>	<i>I</i>	-0.04	<b>0.67</b>	<b>0.63</b>	<b>0.74</b>	<b>0.75</b>	-0.63	-0.53	-0.52	-0.39	-0.48	-0.33
DC	0.04	0.03	-0.02	-0.03	-0.04	<i>I</i>	0.03	0.02	-0.02	-0.03	0.03	0	0.05	0.07	0.07	-0.03
HWL	<i>I</i>	<b>0.96</b>	<b>0.88</b>	<b>0.86</b>	<b>0.67</b>	0.03	<i>I</i>	<b>0.96</b>	<b>0.87</b>	<b>0.86</b>	-0.36	-0.33	-0.45	-0.47	-0.51	-0.35
HWF	<b>0.96</b>	<i>I</i>	<b>0.83</b>	<b>0.8</b>	<b>0.63</b>	0.02	<b>0.96</b>	<i>I</i>	<b>0.83</b>	<b>0.8</b>	-0.28	-0.27	-0.4	-0.44	-0.5	-0.24
HNL	<b>0.87</b>	<b>0.83</b>	<i>I</i>	<b>0.96</b>	<b>0.74</b>	-0.02	<b>0.87</b>	<b>0.83</b>	<i>I</i>	<b>0.96</b>	-0.56	-0.52	-0.58	-0.56	-0.66	-0.41
HNR	<b>0.86</b>	<b>0.8</b>	<b>0.96</b>	<i>I</i>	<b>0.75</b>	-0.03	<b>0.86</b>	<b>0.8</b>	<b>0.96</b>	<i>I</i>	-0.55	-0.49	-0.63	-0.62	-0.68	-0.46
in1	-0.36	-0.28	<b>-0.56</b>	<b>-0.56</b>	-0.63	0.03	-0.36	-0.28	-0.56	-0.55	<i>I</i>	<b>0.79</b>	<b>0.68</b>	<b>0.51</b>	<b>0.51</b>	<b>0.44</b>
in2	-0.33	-0.27	<b>-0.52</b>	<b>-0.49</b>	-0.53	0	-0.33	-0.27	-0.52	-0.49	<b>0.79</b>	<i>I</i>	<b>0.74</b>	<b>0.5</b>	<b>0.43</b>	<b>0.47</b>
in3	-0.46	-0.41	<b>-0.58</b>	<b>-0.63</b>	<b>-0.52</b>	0.05	-0.45	-0.4	-0.58	-0.63	<b>0.68</b>	<b>0.74</b>	<i>I</i>	<b>0.81</b>	<b>0.59</b>	<b>0.59</b>
in4	-0.48	-0.45	<b>-0.56</b>	<b>-0.62</b>	-0.39	0.07	-0.47	-0.44	-0.56	-0.62	<b>0.51</b>	<b>0.5</b>	<b>0.81</b>	<i>I</i>	<b>0.69</b>	<b>0.65</b>
in5	-0.5	-0.5	<b>-0.66</b>	<b>-0.68</b>	<b>-0.48</b>	0.07	<b>-0.51</b>	<b>-0.5</b>	-0.66	-0.68	<b>0.51</b>	<b>0.43</b>	<b>0.59</b>	<b>0.69</b>	<i>I</i>	<b>0.55</b>
in6	-0.35	-0.24	<b>-0.41</b>	<b>-0.46</b>	-0.33	-0.03	-0.35	-0.24	-0.41	-0.46	<b>0.44</b>	<b>0.47</b>	<b>0.59</b>	<b>0.65</b>	<b>0.55</b>	<i>I</i>
in7	-0.29	-0.21	<b>-0.37</b>	<b>-0.34</b>	-0.39	-0.09	-0.27	-0.2	-0.37	-0.34	<b>0.74</b>	<b>0.73</b>	<b>0.54</b>	<b>0.41</b>	<b>0.36</b>	<b>0.56</b>
in8	0.1	0.09	-0.08	-0.04	-0.22	0.01	0.1	0.09	-0.08	-0.04	<b>0.45</b>	<b>0.38</b>	0.07	-0.13	0.07	-0.16
nl1	0.06	0.03	0.22	0.25	0.19	0.01	0.07	0.03	0.22	0.25	-0.32	-0.36	-0.31	-0.1	-0.16	-0.21
nl2	-0.19	-0.12	<b>-0.36</b>	<b>-0.3</b>	-0.29	-0.01	-0.19	-0.12	-0.36	-0.3	<b>0.38</b>	<b>0.39</b>	0.18	0.12	0.16	0.2
ou1	-0.16	-0.07	-0.32	<b>-0.31</b>	<b>-0.4</b>	-0.04	-0.16	-0.07	-0.32	-0.31	<b>0.73</b>	<b>0.69</b>	<b>0.47</b>	<b>0.34</b>	<b>0.36</b>	<b>0.52</b>
ou2	-0.34	-0.26	<b>-0.39</b>	<b>-0.34</b>	<b>-0.34</b>	-0.08	-0.33	-0.25	-0.39	-0.39	<b>0.61</b>	<b>0.47</b>	<b>0.46</b>	<b>0.5</b>	<b>0.45</b>	<b>0.62</b>
ou3	-0.43	-0.34	<b>-0.43</b>	<b>-0.45</b>	-0.29	-0.09	-0.42	-0.33	-0.43	-0.45	<b>0.45</b>	<b>0.36</b>	<b>0.41</b>	<b>0.45</b>	<b>0.47</b>	<b>0.66</b>

**Table C.5** Correlation of input variables.

	in7	in8	nl1	nl2	ou1	ou2	ou3	ou4	ou5	ou6	ou7	ou8	nr1	nr2
in1u	<b>-0.66</b>	-0.25	0.23	-0.44	<b>-0.63</b>	-0.66	-0.58	-0.63	-0.35	<b>-0.58</b>	<b>-0.52</b>	<b>-0.59</b>	<b>-0.6</b>	-0.24
in1l	<b>-0.44</b>	-0.03	0.1	-0.38	-0.39	<b>-0.54</b>	-0.55	<b>-0.59</b>	-0.28	<b>-0.52</b>	-0.32	-0.36	-0.48	-0.29
in2u	<b>-0.66</b>	-0.19	0.27	-0.34	<b>-0.61</b>	-0.63	-0.6	-0.61	-0.2	<b>-0.59</b>	-0.5	<b>-0.65</b>	-0.5	-0.1
in2l	-0.34	0.03	0.09	-0.16	-0.29	-0.5	-0.55	-0.55	-0.08	<b>-0.56</b>	-0.2	-0.44	-0.28	-0.05
in3u	<b>-0.63</b>	-0.21	0.26	-0.35	<b>-0.54</b>	<b>-0.61</b>	<b>-0.51</b>	<b>-0.54</b>	-0.19	-0.45	-0.49	<b>-0.51</b>	-0.49	-0.26
in3l	-0.26	-0.25	-0.01	-0.33	-0.22	-0.34	-0.26	-0.04	-0.06	-0.15	-0.32	-0.09	-0.3	-0.33
in4u	-0.47	0.06	0.14	-0.14	<b>-0.34</b>	<b>-0.54</b>	-0.5	<b>-0.61</b>	-0.1	-0.48	-0.22	<b>-0.43</b>	<b>-0.35</b>	-0.15
in4l	-0.11	-0.12	0.07	-0.04	0	-0.07	-0.1	0.29	0.45	0.15	0.01	-0.02	-0.11	-0.17
in5u	-0.47	-0.18	0.2	-0.27	-0.36	<b>-0.53</b>	<b>-0.55</b>	-0.47	-0.02	-0.43	-0.35	-0.46	-0.5	-0.34
in5l	-0.17	-0.14	0.06	-0.15	-0.04	-0.14	-0.14	0.21	0.37	0.08	-0.09	-0.04	-0.22	-0.3
in6u	<b>-0.67</b>	-0.12	0.24	-0.33	<b>-0.57</b>	<b>-0.75</b>	<b>-0.73</b>	<b>-0.67</b>	-0.35	<b>-0.64</b>	-0.46	<b>-0.59</b>	-0.49	-0.1
in6l	-0.24	-0.34	0.07	-0.21	-0.16	-0.28	-0.21	-0.03	0.24	-0.18	-0.17	-0.15	-0.3	-0.26
in7u	<b>-0.74</b>	-0.24	0.24	-0.34	<b>-0.63</b>	<b>-0.71</b>	<b>-0.69</b>	<b>-0.61</b>	-0.24	<b>-0.65</b>	<b>-0.54</b>	<b>-0.67</b>	<b>-0.52</b>	-0.09
in7l	-0.28	0	0.13	-0.22	-0.29	-0.39	-0.44	<b>-0.51</b>	-0.01	-0.45	-0.18	-0.44	-0.37	-0.15
in8u	<b>-0.55</b>	-0.45	0.29	-0.45	-0.5	<b>-0.54</b>	<b>-0.56</b>	-0.38	-0.16	-0.47	-0.41	-0.49	<b>-0.57</b>	-0.29
in8l	-0.3	0.21	0.09	-0.34	-0.23	-0.42	<b>-0.53</b>	<b>-0.57</b>	-0.21	-0.46	-0.19	-0.34	-0.42	-0.28
nl1u	<b>-0.59</b>	-0.24	0.12	-0.3	<b>-0.56</b>	<b>-0.61</b>	<b>-0.54</b>	<b>-0.58</b>	-0.23	<b>-0.54</b>	<b>-0.38</b>	<b>-0.56</b>	-0.49	-0.08
nl1l	<b>-0.62</b>	-0.33	0.42	-0.27	-0.6	<b>-0.62</b>	<b>-0.54</b>	<b>-0.55</b>	-0.24	<b>-0.51</b>	-0.4	<b>-0.59</b>	-0.5	-0.06
nl2u	<b>-0.59</b>	-0.35	0.33	-0.49	<b>-0.59</b>	<b>-0.52</b>	-0.5	-0.49	-0.26	-0.44	-0.36	<b>-0.56</b>	<b>-0.54</b>	-0.09
nl2l	<b>-0.55</b>	-0.32	0.37	-0.22	<b>-0.53</b>	-0.5	-0.48	-0.49	-0.21	-0.44	-0.32	<b>-0.56</b>	-0.47	-0.03
ou1u	<b>-0.64</b>	-0.27	0.21	-0.42	<b>-0.68</b>	-0.7	<b>-0.6</b>	-0.65	-0.37	<b>-0.62</b>	<b>-0.54</b>	<b>-0.62</b>	<b>-0.57</b>	-0.19
ou1l	<b>-0.67</b>	-0.04	0.08	-0.29	-0.23	-0.47	-0.42	<b>-0.57</b>	-0.16	-0.47	-0.24	-0.36	-0.42	-0.26
ou2u	<b>-0.67</b>	-0.14	0.27	-0.38	<b>-0.58</b>	<b>-0.72</b>	-0.7	<b>-0.62</b>	-0.26	<b>-0.56</b>	<b>-0.45</b>	<b>-0.59</b>	<b>-0.54</b>	-0.16
ou2l	-0.26	0.01	0.23	-0.32	-0.21	-0.14	-0.28	-0.27	0.12	-0.14	-0.03	-0.34	-0.42	-0.24
ou3u	<b>-0.61</b>	-0.11	0.21	-0.3	-0.48	<b>-0.68</b>	<b>-0.76</b>	<b>-0.62</b>	-0.2	<b>-0.58</b>	-0.39	-0.5	-0.45	-0.12
ou3l	-0.25	-0.06	0.15	-0.24	-0.19	-0.25	-0.2	-0.29	0.17	-0.14	-0.09	-0.27	-0.35	-0.23
ou4u	<b>-0.53</b>	0.12	0.18	-0.33	-0.44	<b>-0.59</b>	<b>-0.58</b>	<b>-0.69</b>	-0.37	-0.45	-0.34	-0.43	-0.45	-0.17
ou4l	-0.07	-0.12	0.17	-0.19	-0.01	0.14	0.14	0.4	0.38	0.39	0.09	0.08	-0.18	-0.23
ou5u	<b>-0.49</b>	0.21	0.05	-0.16	-0.4	<b>-0.53</b>	<b>-0.45</b>	<b>-0.63</b>	-0.37	-0.45	-0.32	-0.38	-0.31	-0.11
ou5l	0.02	0.13	-0.05	0.11	0.16	0.12	0.12	0.14	0.67	0.19	0.12	-0.03	-0.04	-0.2
ou6u	<b>-0.57</b>	-0.01	0.09	-0.23	-0.5	<b>-0.69</b>	<b>-0.66</b>	<b>-0.79</b>	-0.34	<b>-0.77</b>	-0.47	<b>-0.58</b>	-0.42	-0.12
ou6l	-0.33	0.05	0.1	-0.2	-0.29	-0.4	-0.32	<b>-0.53</b>	-0.02	-0.29	-0.24	-0.44	-0.41	-0.23
ou7u	<b>-0.71</b>	-0.24	0.29	-0.42	<b>-0.65</b>	<b>-0.62</b>	<b>-0.58</b>	<b>-0.53</b>	-0.21	<b>-0.5</b>	<b>-0.64</b>	<b>-0.67</b>	<b>-0.6</b>	-0.22
ou7l	-0.35	-0.04	0.25	-0.36	-0.31	-0.29	-0.36	-0.39	0.02	-0.25	-0.08	-0.38	-0.47	-0.22
ou8u	<b>-0.62</b>	-0.27	0.27	-0.41	<b>-0.64</b>	<b>-0.61</b>	-0.5	<b>-0.6</b>	-0.31	<b>-0.51</b>	<b>-0.54</b>	<b>-0.72</b>	<b>-0.63</b>	-0.23
ou8l	-0.44	-0.19	0.21	-0.43	-0.44	-0.47	-0.35	<b>-0.51</b>	-0.24	-0.38	-0.32	-0.35	<b>-0.52</b>	-0.29
nrlu	<b>-0.62</b>	-0.31	0.26	-0.38	<b>-0.6</b>	<b>-0.58</b>	<b>-0.51</b>	<b>-0.54</b>	-0.25	-0.48	-0.44	<b>-0.62</b>	<b>-0.66</b>	-0.17
nrl1	<b>-0.58</b>	-0.27	0.26	-0.32	<b>-0.54</b>	<b>-0.56</b>	<b>-0.49</b>	<b>-0.54</b>	-0.22	-0.48	-0.39	<b>-0.56</b>	-0.45	-0.1
nr2u	<b>-0.58</b>	-0.14	0.13	-0.34	<b>-0.51</b>	<b>-0.59</b>	<b>-0.57</b>	<b>-0.6</b>	-0.22	<b>-0.56</b>	-0.44	<b>-0.58</b>	<b>-0.57</b>	-0.32
nr2l	<b>-0.61</b>	-0.13	0.16	-0.29	<b>-0.54</b>	<b>-0.62</b>	<b>-0.64</b>	<b>-0.6</b>	-0.27	<b>-0.61</b>	-0.43	<b>-0.6</b>	-0.49	0.02
CS	-0.39	-0.22	0.18	-0.29	-0.4	-0.35	-0.29	-0.37	-0.03	-0.28	-0.36	<b>-0.55</b>	<b>-0.55</b>	-0.31
MCS	0.17	-0.12	0.01	-0.04	0.04	0.09	0.1	0.02	0.21	0.08	0.01	-0.23	-0.17	-0.22
ML	0.22	-0.08	-0.02	-0.08	0.03	0.13	0.14	0.04	0.21	0.11	0.03	-0.21	-0.19	-0.27
IT	-0.16	0.13	-0.07	-0.08	0.04	-0.29	-0.32	-0.25	-0.14	-0.23	0.02	0.18	-0.05	-0.08
FWL	0.03	0.03	0.01	0.01	0.01	0	-0.01	-0.02	0	0	-0.01	-0.02	-0.02	-0.02
FWF	0.01	0.01	-0.02	0	0.02	0.02	0.02	0.01	0.01	0.01	0.02	0.01	0	0
FNL	0	0.02	-0.04	0.01	0	-0.01	0.01	0	0	0.02	0	-0.01	0.02	0.02
FNR	0.01	0.02	-0.02	0.01	0	0	-0.01	0	0.01	0.01	0	0.01	0.01	0.01
DWL	-0.29	0.1	0.06	-0.19	-0.16	-0.34	-0.43	-0.5	-0.02	-0.41	-0.22	-0.34	-0.4	-0.33
DWF	-0.21	0.09	0.03	-0.12	-0.07	-0.26	-0.34	-0.41	0.08	-0.34	-0.19	-0.27	-0.35	-0.38
DNL	-0.37	-0.08	0.22	-0.36	-0.32	-0.39	-0.43	<b>-0.55</b>	-0.19	-0.4	-0.26	-0.39	<b>-0.51</b>	-0.32
DNR	-0.34	-0.04	0.25	-0.3	-0.31	-0.39	-0.45	<b>-0.6</b>	-0.18	-0.43	-0.19	-0.42	-0.49	-0.27
OF	-0.39	-0.22	0.19	-0.29	-0.4	-0.34	-0.29	-0.38	-0.03	-0.28	-0.36	<b>-0.55</b>	<b>-0.55</b>	-0.31
DC	-0.09	0.01	0.01	-0.01	-0.04	-0.08	-0.09	0	-0.06	-0.05	-0.08	0	0.01	-0.02
HWL	-0.27	0.1	0.07	-0.19	-0.16	-0.33	-0.42	-0.49	-0.02	-0.4	-0.22	-0.35	-0.4	-0.33
HWF	-0.2	0.09	0.03	-0.12	-0.07	-0.25	-0.33	-0.4	0.08	-0.33	-0.18	-0.27	-0.35	-0.38
HNL	<b>-0.37</b>	-0.08	0.22	-0.36	-0.32	-0.39	-0.43	<b>-0.55</b>	-0.19	-0.4	-0.26	-0.39	-0.5	-0.32
HNR	-0.34	-0.04	0.25	-0.3	-0.31	-0.39	-0.45	<b>-0.6</b>	-0.18	-0.43	-0.19	-0.42	-0.49	-0.27
in1	<b>0.74</b>	<b>0.45</b>	-0.32	<b>0.38</b>	<b>0.73</b>	<b>0.61</b>	<b>0.45</b>	<b>0.5</b>	<b>0.34</b>	<b>0.5</b>	<b>0.61</b>	<b>0.7</b>	<b>0.57</b>	0.12
in2	<b>0.73</b>	<b>0.38</b>	-0.36	<b>0.39</b>	<b>0.69</b>	<b>0.47</b>	<b>0.36</b>	<b>0.37</b>	<b>0.25</b>	<b>0.32</b>	<b>0.62</b>	<b>0.59</b>	<b>0.51</b>	0.11
in3	<b>0.54</b>	<b>0.07</b>	<b>-0.31</b>	<b>0.18</b>	<b>0.47</b>	<b>0.46</b>	<b>0.41</b>	<b>0.59</b>	<b>0.18</b>	<b>0.42</b>	<b>0.34</b>	<b>0.53</b>	<b>0.35</b>	0.06
in4	<b>0.41</b>	-0.13	-0.1	<b>0.12</b>	<b>0.34</b>	<b>0.5</b>	<b>0.45</b>	<b>0.79</b>	<b>0.37</b>	<b>0.57</b>	<b>0.23</b>	<b>0.42</b>	<b>0.28</b>	0.05
in5	<b>0.36</b>	<b>0.07</b>	-0.16	<b>0.16</b>	<b>0.36</b>	<b>0.45</b>	<b>0.47</b>	<b>0.71</b>	<b>0.37</b>	<b>0.55</b>	<b>0.31</b>	<b>0.47</b>	<b>0.34</b>	0.1
in6	<b>0.56</b>	-0.16	-0.21	<b>0.2</b>	<b>0.52</b>	<b>0.62</b>	<b>0.66</b>	<b>0.75</b>	<b>0.63</b>	<b>0.59</b>	<b>0.39</b>	<b>0.55</b>	<b>0.3</b>	-0.11
in7	<b>I</b>	<b>0.43</b>	-0.27	<b>0.34</b>	<b>0.79</b>	<b>0.79</b>	<b>0.7</b>	<b>0.47</b>	<b>0.42</b>	<b>0.61</b>	<b>0.77</b>	<b>0.65</b>	<b>0.47</b>	-0.02
in8	<b>0.43</b>	<b>I</b>	<b>-0.33</b>	<b>0.23</b>	<b>0.46</b>	<b>0.24</b>	<b>0.11</b>	<b>-0.22</b>	<b>-0.04</b>	<b>0.08</b>	<b>0.37</b>	<b>0.28</b>	<b>0.29</b>	0.04
nl1	-0.27	-0.33	<b>I</b>	0	-0.3	-0.18	-0.16	-0.04	-0.09	-0.04	-0.16	-0.25	-0.14	0.06
nl2	<b>0.34</b>	<b>0.23</b>	0	<b>I</b>	<b>0.39</b>	<b>0.25</b>	<b>0.23</b>	<b>0.17</b>	<b>0.25</b>	<b>0.18</b>	<b>0.24</b>	<b>0.19</b>	<b>0.41</b>	0.2
ou1	<b>0.79</b>	<b>0.46</b>	-0.3	<b>0.39</b>	<b>I</b>	<b>0.69</b>	<b>0.57</b>	<b>0.44</b>	<b>0.49</b>	<b>0.53</b>	<b>0.71</b>	<b>0.69</b>	<b>0.5</b>	0
ou2	<b>0.79</b>	<b>0.24</b>	-0.18	<b>0.25</b>	<b>0.69</b>	<b>I</b>	<b>0.82</b>	<b>0.69</b>	<b>0.56</b>	<b>0.73</b>	<b>0.68</b>	<b>0.57</b>	<b>0.38</b>	-0.01
ou3	<b>0.7</b>	<b>0.11</b>	-0.16	<b>0.23</b>	<b>0.57</b>	<b>0.82</b>	<b>I</b>	<b>0.69</b>	<b>0.5</b>	<b>0.77</b>	<b>0.53</b>	<b>0.51</b>	<b>0.34</b>	-0.06
ou4	<b>0.47</b>	-0.22	-0.04	0.17	<b>0.44</b>	<b>0.69</b>	<b>0.69</b>	<b>I</b>	<b>0.66</b>	<b>0.75</b>	<b>0.41</b>	<b>0.49</b>	<b>0.31</b>	-0.01
ou5	<b>0.42</b>	-0.04	-0.09	0.25	<b>0.49</b>	<b>0.56</b>	<b>0.5</b>	<b>0.66</b>	<b>I</b>	<b>0.56</b>	<b>0.39</b>	<b>0.29</b>	<b>0.21</b>	-0.12
ou6	<b>0.61</b>	0.08	-0.04	0.18	<b>0.53</b>	<b>0.73</b>	<b>0.7</b>	<b>0.75</b>	<b>0.56</b>	<b>I</b>	<b>0.54</b>	<b>0.51</b>	<b>0.25</b>	-0.06
ou7	<													

## Appendix D

# MVIV model time response

### D.1 1280mm wide slabs

**Table D.1** Comparison of  $V(\hat{\Theta})$  for different ARX structures for 1280mm wide slabs.

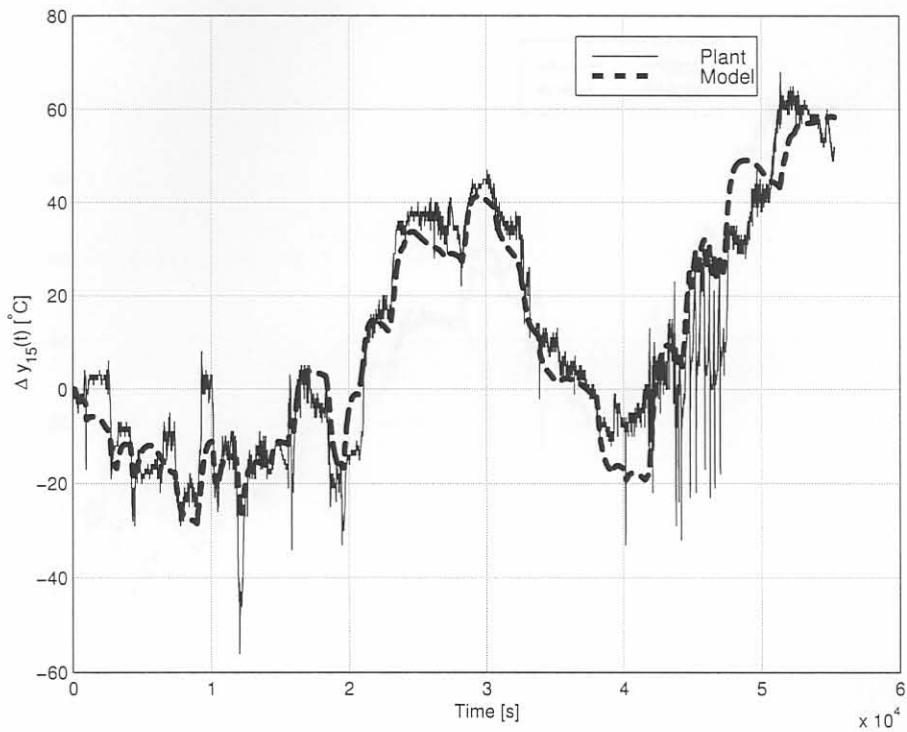
	$n_b=1$	2	3
$n_a=1$	12.8579		
2	12.7289	12.7664	
3	12.7073	12.7422	12.7469

### D.2 1575mm wide slabs

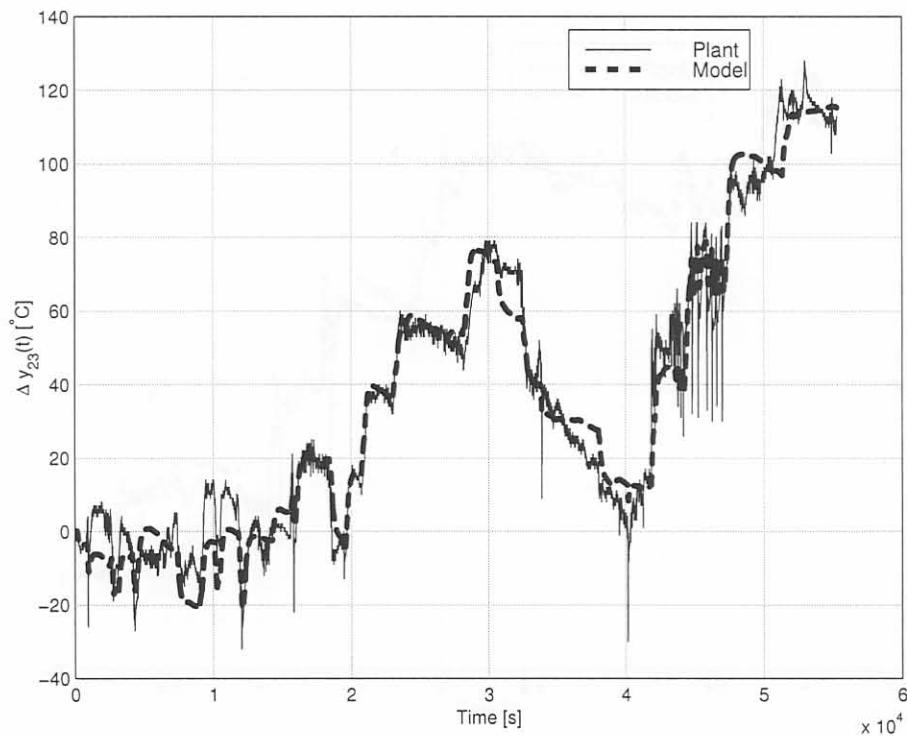
**Table D.2** Comparison of  $V(\hat{\Theta})$  for different ARX structures for 1575mm wide slabs.

	$n_b=1$	2	3
$n_a=1$	7.9015		
2	7.9207	7.9174	
3	7.8327	7.8285	7.8163

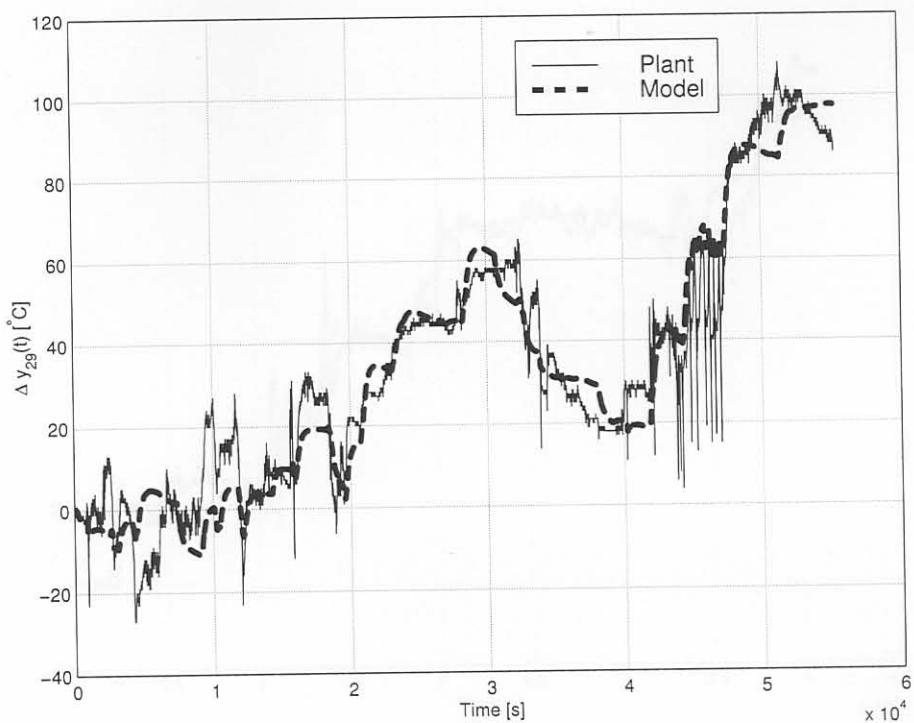
Figure D.1 Comparison of model output and ground truth for the two slab configurations along the width, including 1280 and 1575 mm widths.



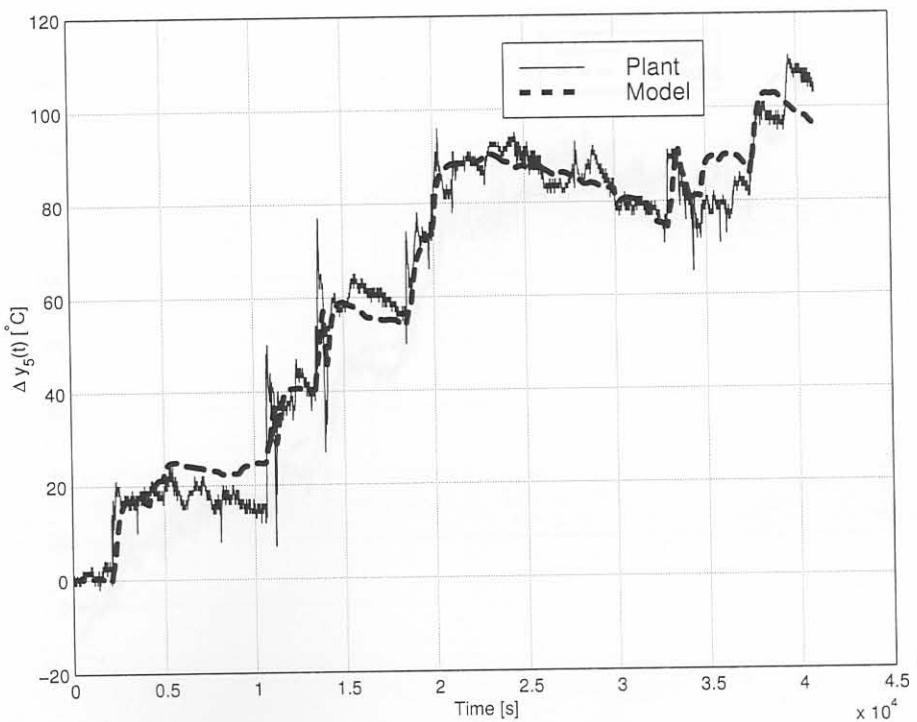
**Figure D.1** Comparison of model output and plant output for thermocouple (output) in8u ( $\Delta y_{15}(t)$ ) with  $n_a = 1$  and  $n_b = 1$  and 1280mm wide slabs.



**Figure D.2** Comparison of model output and plant output for thermocouple (output) ou2u ( $\Delta y_{23}(t)$ ) with  $n_a = 1$  and  $n_b = 1$  and 1280mm wide slabs.



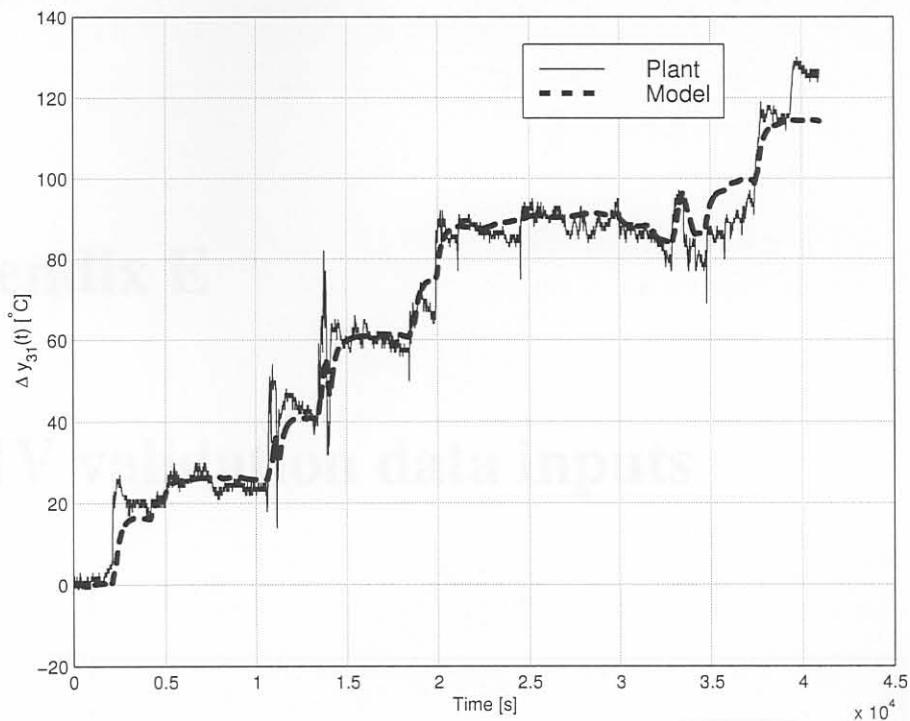
**Figure D.3** Comparison of model output and plant output for thermocouple (output) ou5u ( $\Delta y_{29}(t)$ ) with  $n_a = 1$  and  $n_b = 1$  and 1280mm wide slabs.



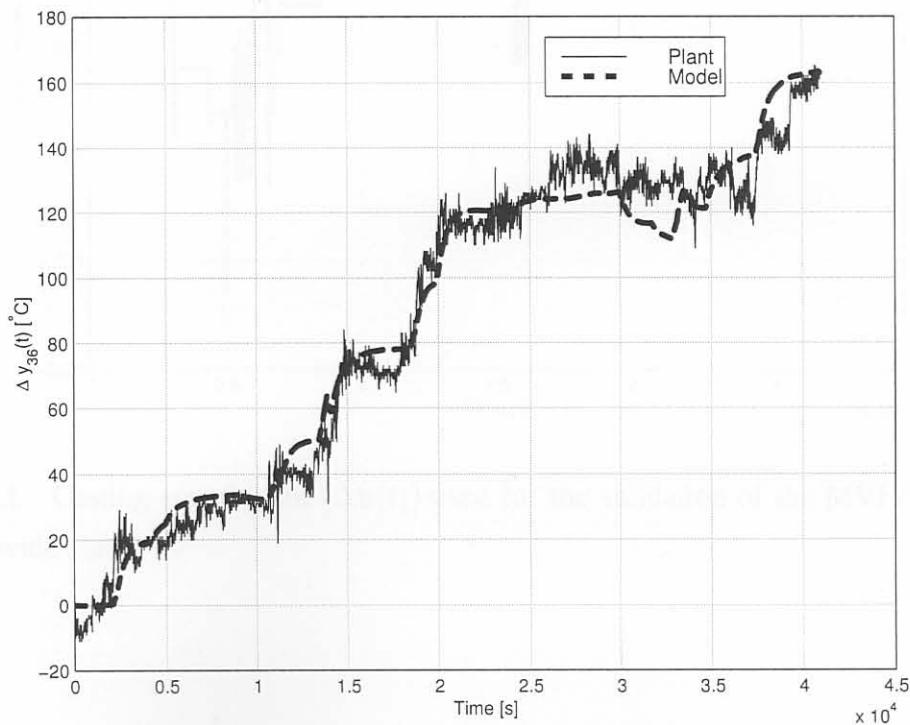
**Figure D.4** Comparison of model output and plant output for thermocouple (output) in3u ( $\Delta y_5(t)$ ) with  $n_a = 1$  and  $n_b = 1$  and 1575mm wide slabs.

## Appendix D

## MVIV model time response



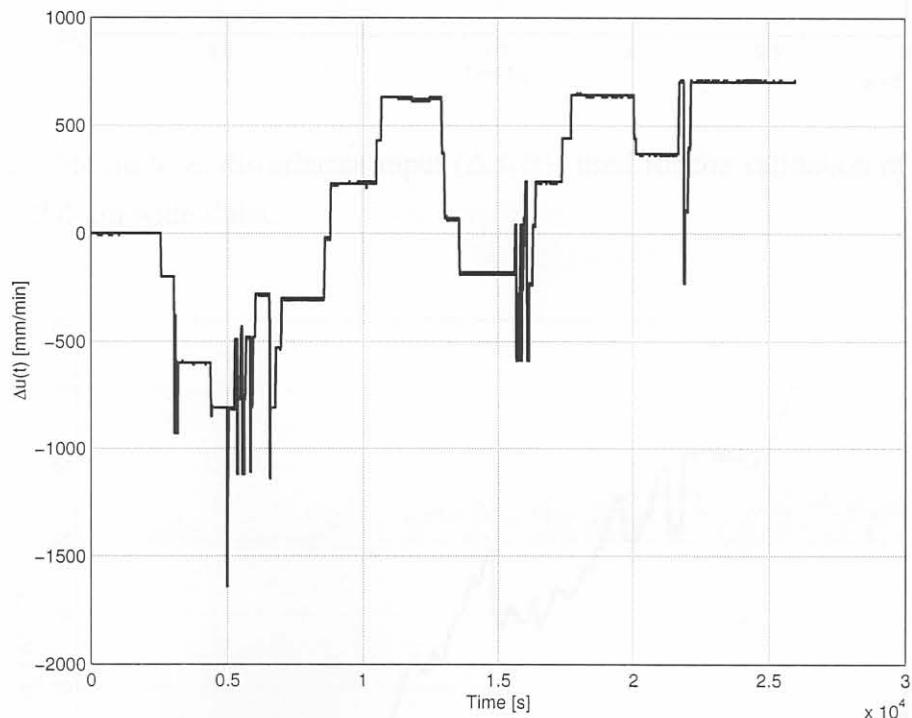
**Figure D.5** Comparison of model output and plant output for thermocouple (output) ou7u ( $\Delta y_{31}(t)$ ) with  $n_a = 1$  and  $n_b = 1$  and 1575mm wide slabs.



**Figure D.6** Comparison of model output and plant output for thermocouple (output) nr11 ( $\Delta y_{36}(t)$ ) with  $n_a = 1$  and  $n_b = 1$  and 1575mm wide slabs.

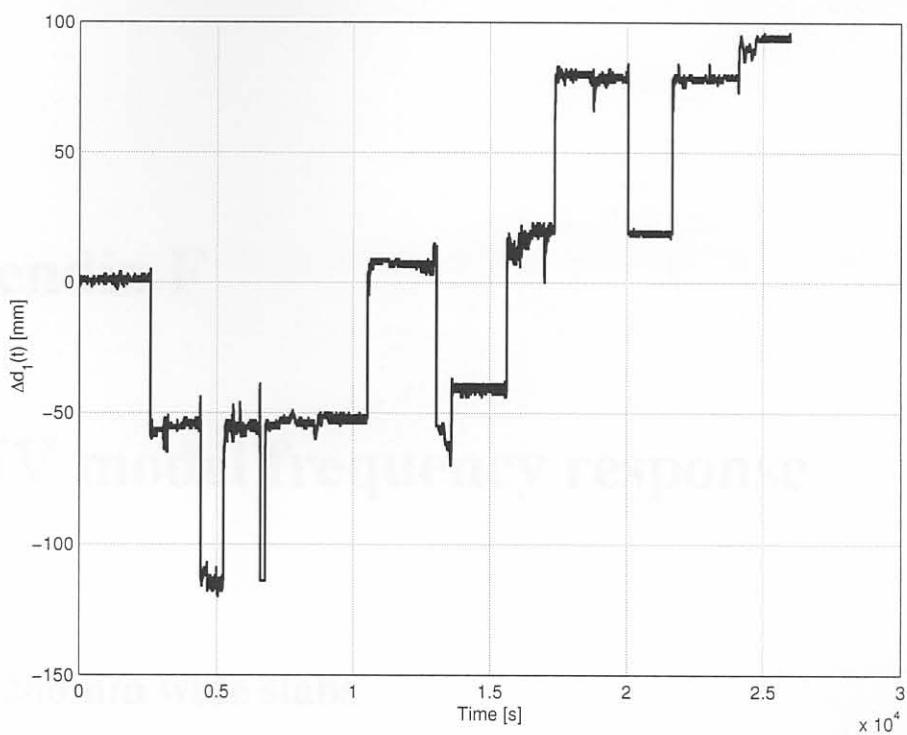
## Appendix E

### MVIV validation data inputs

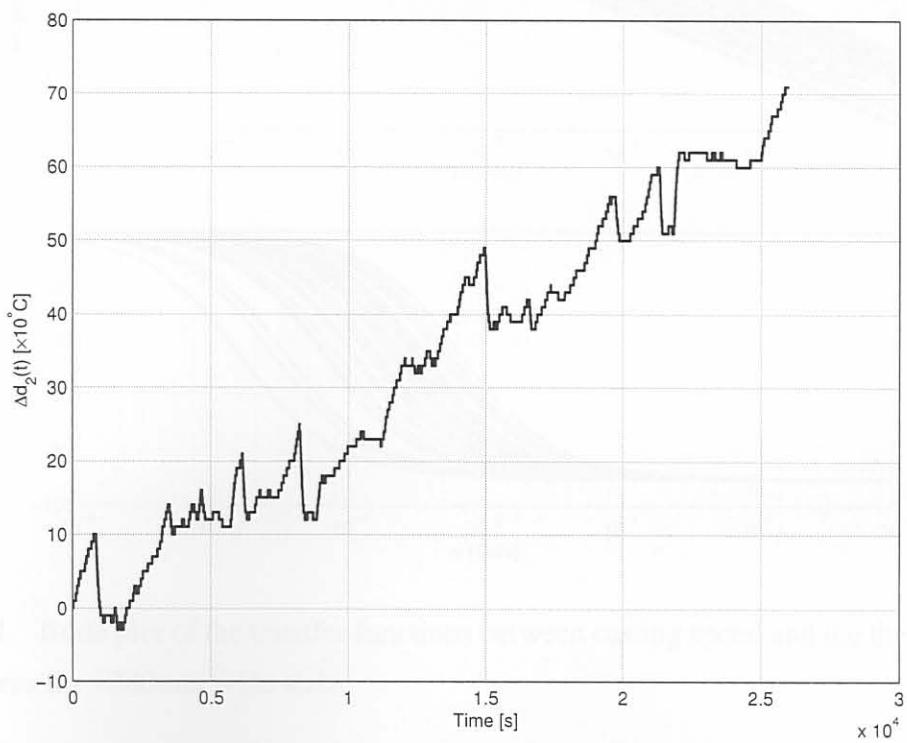


**Figure E.1** Casting speed input ( $\Delta u(t)$ ) used for the validation of the MVIV model for 1280mm wide slabs.

Figure E.2 Water temperature disturbance input ( $\Delta T_w(t)$ ) used for the validation of the MVIV model for 1280mm wide slabs.



**Figure E.2** Mould level disturbance input ( $\Delta d_1(t)$ ) used for the validation of the MVIV model for 1280mm wide slabs.

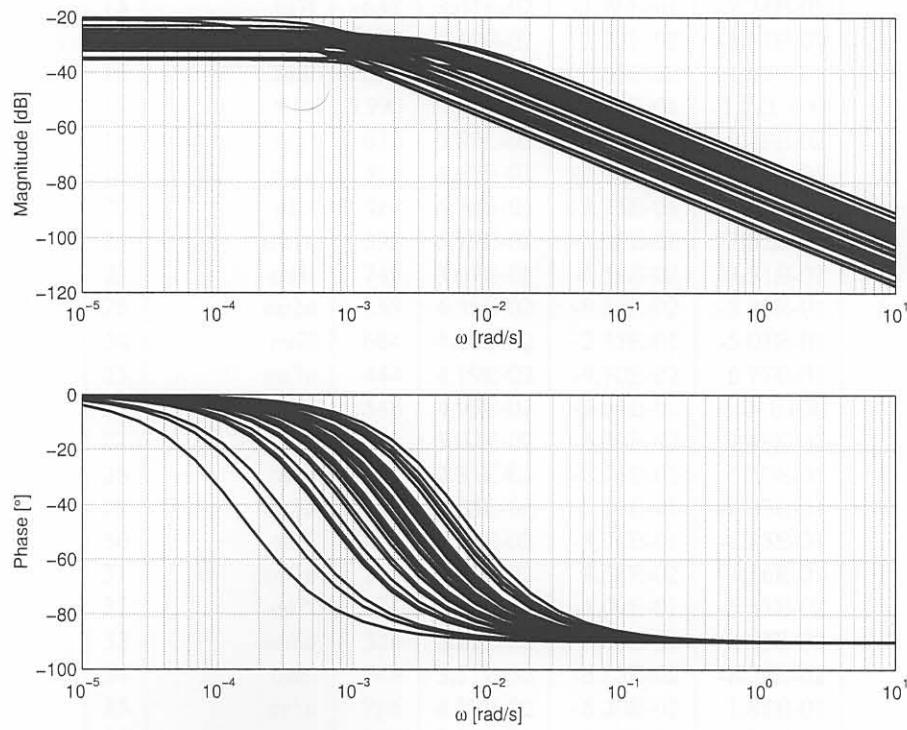


**Figure E.3** Water temperature disturbance input ( $\Delta d_2(t)$ ) used for the validation of the MVIV model for 1280mm wide slabs.

## Appendix F

### MVIV model frequency response

#### F.1 1280mm wide slabs

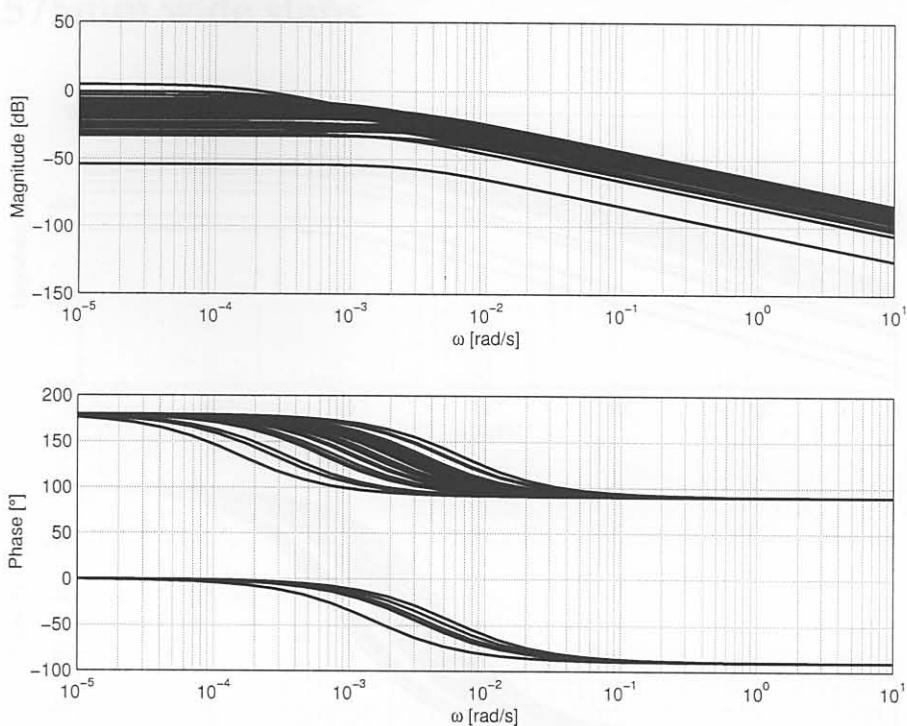


**Figure F.1** Bode plot of the transfer functions between casting speed and the thermocouple temperatures for 1280mm wide slabs.

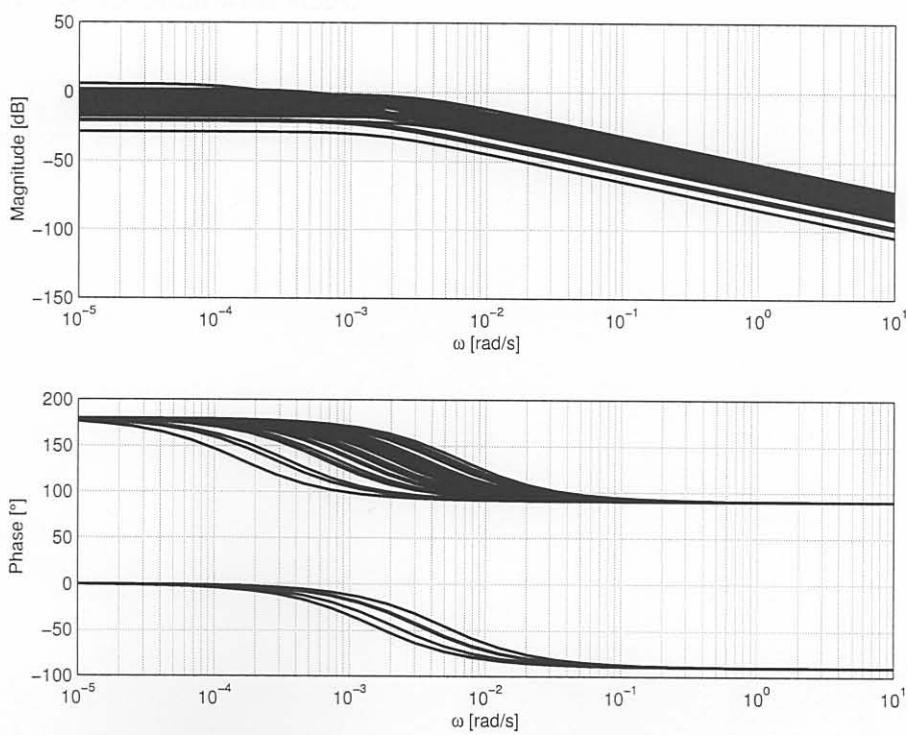
**Table F.1** Transfer functions of the MV to IV model for 1280mm wide slabs.

$i$	Thermocouple	$\tau$	$k_u$	$k_{d_1}$	$k_{d_2}$
1	in1u	180	3.33E-02	3.25E-02	-2.88E-01
2	in1l	512	2.47E-02	-2.55E-02	-2.48E-01
3	in2u	324	5.21E-02	-2.05E-01	-8.31E-01
4	in2l	1265	4.67E-02	-3.03E-01	-9.70E-01
5	in3u	348	3.11E-02	-1.97E-03	-5.43E-01
6	in3l	3721	6.06E-02	-9.04E-01	-1.17E+00
7	in4u	420	4.03E-02	-2.01E-01	-4.04E-01
8	in4l	6598	8.93E-02	-1.67E+00	-1.92E+00
9	in5u	197	1.81E-02	-5.74E-02	-1.57E-01
10	in5l	2991	4.81E-02	-6.79E-01	-1.06E+00
11	in6u	447	4.11E-02	-2.15E-01	-6.33E-01
12	in6l	1484	4.23E-02	-4.70E-01	-7.67E-01
13	in7u	302	3.32E-02	-4.18E-02	-4.69E-01
14	in7l	638	3.07E-02	-1.76E-01	-7.74E-01
15	in8u	279	3.10E-02	2.22E-02	-3.67E-01
16	in8l	672	1.70E-02	7.05E-02	1.69E-01
17	nl1u	1590	9.26E-02	-5.07E-01	-1.22E+00
18	nl1l	672	5.82E-02	-1.38E-01	-9.49E-02
19	nl2u	313	4.67E-02	-2.30E-02	4.53E-01
20	nl2l	484	4.78E-02	-1.75E-01	1.97E-01
21	ou1u	395	5.19E-02	-1.08E-01	-7.52E-01
22	ou1l	745	3.67E-02	-6.54E-02	-4.51E-01
23	ou2u	153	4.35E-02	-9.33E-02	-3.28E-01
24	ou2l	684	4.18E-02	-2.35E-01	-5.01E-01
25	ou3u	444	4.19E-02	-9.70E-02	-6.77E-01
26	ou3l	1548	4.95E-02	-2.64E-01	-1.01E+00
27	ou4u	321	3.07E-02	-6.30E-02	-1.49E-01
28	ou4l	981	2.81E-02	-2.76E-01	-5.37E-01
29	ou5u	286	3.35E-02	-1.06E-01	-2.03E-01
30	ou5l	1563	3.38E-02	-3.76E-01	-4.85E-01
31	ou7u	226	3.65E-02	4.58E-02	-1.26E-01
32	ou7l	611	3.65E-02	-1.09E-01	-3.53E-02
33	ou8u	324	3.28E-02	2.00E-01	-8.93E-02
34	ou8l	748	3.51E-02	-6.25E-02	-8.55E-02
35	nr1u	206	4.79E-02	-6.20E-02	1.88E-01
36	nr1l	297	3.67E-02	-1.43E-01	2.98E-01
37	nr2u	904	6.97E-02	-4.15E-01	-7.08E-01
38	nr2l	435	5.08E-02	-2.52E-01	-2.15E-01

Figure F.3 shows plots of the transfer functions between bulk temperature and the various probe temperatures for the 1280mm wide slabs.

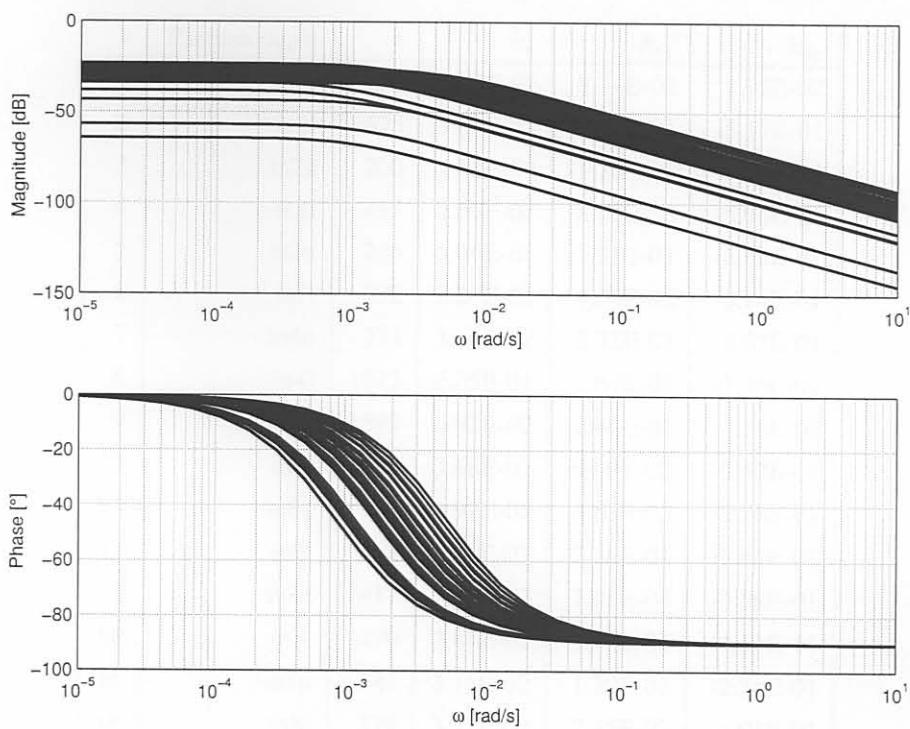


**Figure F.2** Bode plot of the transfer functions between mould level and the thermocouple temperatures for 1280mm wide slabs.



**Figure F.3** Bode plot of the transfer functions between inlet temperature and the thermocouple temperatures for 1280mm wide slabs.

## F.2 1575mm wide slabs



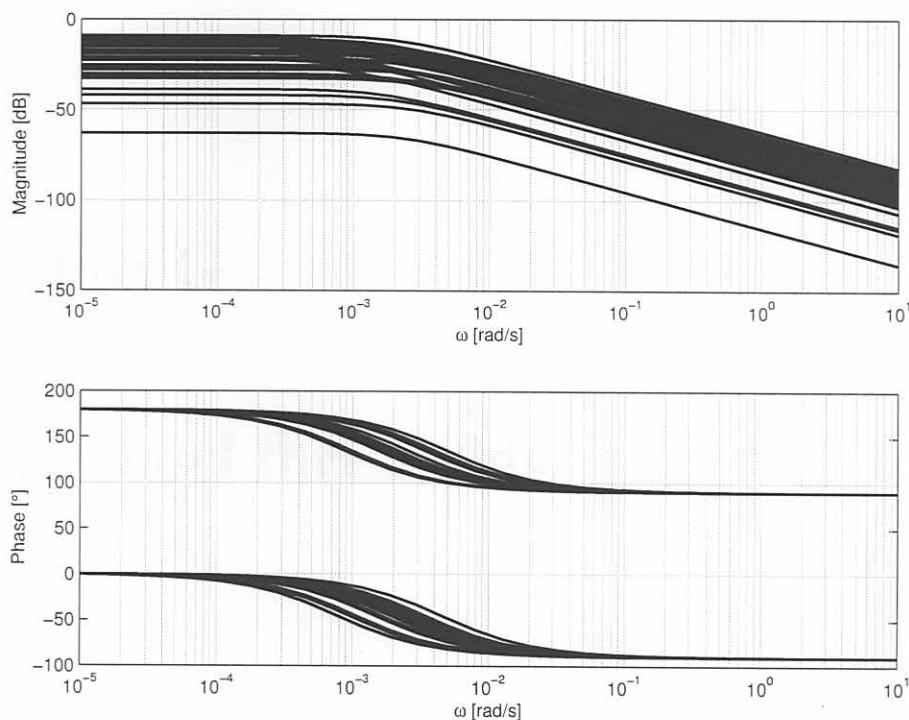
**Figure F.4** Bode plot of the transfer functions between casting speed and the thermocouple temperatures for 1575mm wide slabs.

**Table F.2** Transfer functions of the MV to IV model for 1575mm wide slabs.

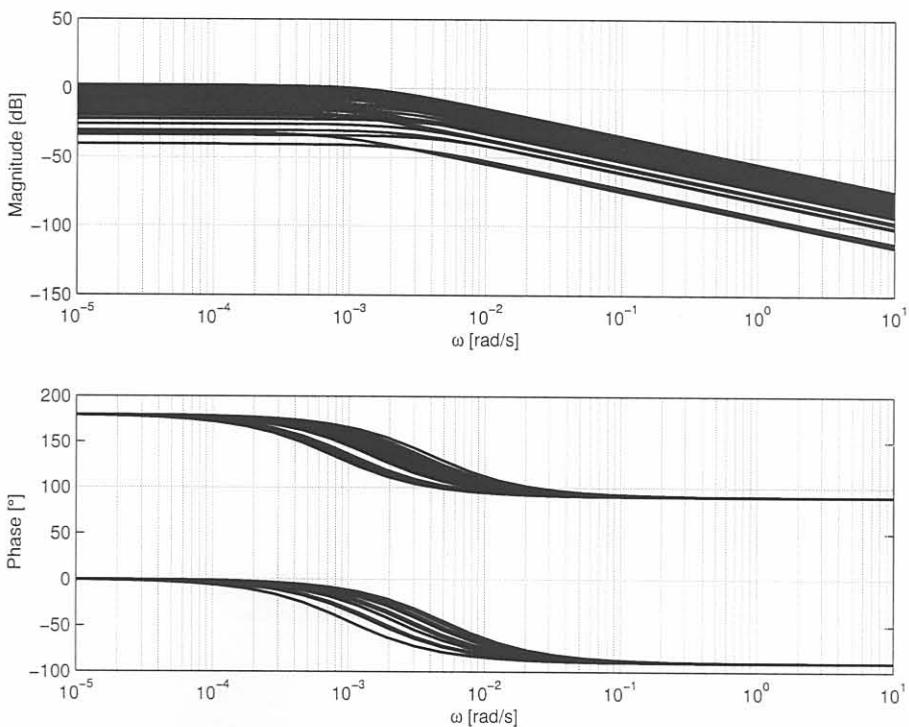
<i>i</i>	Thermocouple	$\tau$	$k_u$	$k_{d_1}$	$k_{d_2}$
1	in1u	221	3.55E-02	7.74E-02	1.95E-02
2	in1l	675	3.64E-02	1.77E-01	-5.57E-01
3	in2u	200	4.64E-02	-1.26E-01	7.54E-02
4	in2l	497	2.59E-02	-8.03E-03	-5.96E-01
5	in3u	245	5.06E-02	-1.31E-01	-2.62E-01
6	in3l	292	3.24E-02	4.04E-02	-5.14E-01
7	in4u	333	3.64E-02	2.32E-02	-1.07E-01
8	in4l	1073	6.05E-04	2.64E-01	-1.35E-01
9	in5u	598	6.92E-02	-2.88E-01	-7.56E-01
10	in5l	539	3.68E-02	-9.09E-02	-5.47E-01
11	in6u	389	3.92E-02	-4.63E-03	-2.26E-01
12	in6l	668	6.74E-03	2.36E-01	-1.61E-01
13	in7u	417	4.95E-02	7.06E-04	-3.78E-01
14	in7l	470	2.44E-02	1.44E-01	-4.13E-01
15	in8u	347	3.75E-02	1.20E-01	-2.56E-01
16	in8l	329	3.72E-02	7.35E-02	-5.91E-01
17	nl1u	285	2.00E-02	-1.31E-01	3.77E-01
18	nl1l	613	3.34E-02	-2.60E-01	4.70E-01
19	nl2u	463	6.03E-02	-3.59E-01	2.71E-01
20	nl2l	385	3.15E-02	-1.78E-01	2.17E-01
21	ou1u	379	2.30E-02	2.10E-01	-4.92E-02
22	ou1l	1316	2.10E-02	2.64E-01	-2.89E-01
23	ou2u	290	4.68E-02	-2.60E-02	-4.14E-01
24	ou2l	1145	5.56E-02	-5.22E-02	-1.02E+00
25	ou3u	380	3.66E-02	5.19E-02	-9.08E-03
26	ou3l	686	2.88E-02	1.86E-01	-3.27E-01
27	ou4u	348	3.55E-02	4.75E-02	2.92E-02
28	ou4l	945	1.44E-03	3.13E-01	-1.35E-01
29	ou5u	498	4.99E-02	-1.11E-01	-3.98E-01
30	ou5l	1305	1.24E-02	1.25E-01	-2.34E-02
31	ou7u	256	4.38E-02	-1.23E-01	7.27E-02
32	ou7l	647	4.37E-02	-1.31E-01	-5.69E-01
33	ou8u	406	3.59E-02	4.96E-02	-9.96E-02
34	ou8l	532	4.26E-02	5.63E-02	-8.63E-01
35	nr1u	619	3.81E-02	1.16E-02	6.97E-01
36	nr1l	459	4.91E-02	-3.13E-02	1.78E-01
37	nr2u	675	2.65E-02	7.52E-02	1.23E+00
38	nr2l	1013	4.19E-02	-7.61E-02	1.25E+00

## Appendix F

## MVIV model frequency response



**Figure F.5** Bode plot of the transfer functions between mould level and the thermocouple temperatures for 1575mm wide slabs.



**Figure F.6** Bode plot of the transfer functions between inlet temperature and the thermocouple temperatures for 1575mm wide slabs.

## Appendix G

IVOV model thresholds

**Table G.1** Thresholds for the IVOV predictor for 1060mm wide slabs

	1a	1b	2a	2b	4	5a	5b	6	8
TBL	0	0	0	0	0.3241	0.3249	0	0	0.3204
TBC	0	0	0	0.2131	0	0.2223	0	0	0.1249
TBR	0	0	0	0	0	0.2174	0	0	0.2553
BBL	0	0	0	0.06797	0	0.2734	0	0	0.2433
BBC	0	0	0	0.1323	0	0.2734	0	0	0.04449
BBR	0	0	0	0	0	0.2734	0	0	0.2383
TAL	0	0	0	0.3255	0	0	0	0	0.1257
TAC	0	0	0	0.8919	0	0	0	0	0.4165
TAR	0	0	0	0.2991	0	0	0	0	0.1628
BAL	0	0	0	0.06184	0	0	0	0	0.1337
BAC	0	0	0.09355	0.9357	0	0	0	0	0.317
BAR	0	0	0	0.0474	0	0	0	0	0.1357

**Table G.2** Thresholds for the IVOV predictor for 1320mm wide slabs

	1a	1b	2a	2b	4	5a	5b	6	8
TBL	0	0	0	0.03973	0.5165	0.2003	0	0.4401	0.1701
TBC	0	0	0	0.1984	0	0.1933	0	0.4401	0.0766
TBR	0	0	0	0.02151	0	0.1852	0	0.4401	0.1539
BBL	0	0	0	0.05918	0	0	0	0.2846	0.07791
BBC	0	0	0	0.2291	0	0	0	0.2846	0.025
BBR	0	0	0	0.01764	0	0	0	0.2846	0.1551
TAL	0	0	0	0.2232	0	0	0.09609	0.1803	0.1555
TAC	0	0.5323	0	0.6739	0	0	0	0.1803	0.1997
TAR	0	0	0	0.2567	0	0	0.1095	0.1803	0.141
BAL	0	0	0	0.1073	0	0	0	0.1203	0.09857
BAC	0	0	0	0.5426	0	0	0	0.1213	0.1414
BAR	0	0	0	0.0547	0	0	0	0.1213	0.1138

**Table G.3** Thresholds for the IVOV predictor for 1575mm wide slabs

	1a	1b	2a	2b	4	5a	5b	6	8
TBL	0	0	0	0	0	0	0	0.1996	0
TBC	0	0	0	0.1067	0	0	0	0.1996	0
TBR	0	0	0	0	0	0	0	0.1996	0
BBL	0	0	0	0	0	0	0	0.1597	0.09185
BBC	0	0	0	0.1127	0	0	0	0.1597	0
BBR	0	0	0	0	0	0	0	0.1597	0.08158
TAL	0	0	0	0.1385	0	0	0	0.06923	0.09947
TAC	0	0	0	0.3336	0	0	0	0.06923	0.1165
TAR	0	0	0	0.149	0	0	0	0.06923	0.1191
BAL	0	0	0	0.04642	0	0	0	0.06108	0.07018
BAC	0	0	0	0.2952	0	0	0	0.05896	0.1117
BAR	0	0	0	0.03535	0	0	0	0.05896	0.08297