



Advanced Low Order Orthotropic Finite Element Formulations

by

Susanna Elizabeth Geyer

Title: Advanced Low Order Orthotropic Finite Element Formulations

Author: Susanna Elizabeth Geyer

Degree: A dissertation submitted in partial fulfillment
of the requirements for the degree of

Supervisor: **Master of Engineering**

Department: in the Department of Mechanical and Aeronautical Engineering,
University of Pretoria

December 2000

Supervisor:

Prof. Albert A. Groenwold



Abstract

Title: Advanced Low Order Orthotropic Finite Element Formulations

Author: Susanna Elizabeth Geyer

Degree: M.Eng (Mechanical)

Department: Mechanical Engineering

Supervisor: Prof. Albert A. Groenwold

Keywords: Drilling d.o.f., Assumed stress, Membrane, Flat shell, Finite element, Orthotropy

In this study advanced low order finite elements for the linear analysis and ultimately, the global optimization of orthotropic shells structures, are presented. Low order quadrilaterals are attractive in optimization, since they result in low connectivity of the structural stiffness matrix, and hence, reduced computational effort. However, standard 4-node quadrilaterals are notorious for their low accuracy.

Both drilling degrees of freedom and assumed stress interpolations have the potential to improve the modeling capabilities of low order quadrilateral finite elements. Therefore, it seems desirable to formulate low order elements with both an assumed stress interpolation field and drilling degrees of freedom, on condition that the elements are rank sufficient and invariant.

Firstly, a variational basis for the formulation of two families of assumed stress membrane finite elements with drilling degrees of freedom, is presented. This formulation depends on the formulation of Hughes and Brezzi, and is derived using the unified formulation presented by Di and Ramm. The recent stress mode classification method presented by Feng *et al.* is used to derive the stress interpolation matrices. The families, denoted $8\beta(M)$ and $8\beta(D)$, are rank sufficient, invariant, and free of locking. The membrane locking correction suggested by Taylor ensures that the consistent nodal loads of both families are identical to those of a quadrilateral 4-node membrane finite element with two translational degrees of freedom per node.

Secondly, the rectangular assumed strain plate element presented by Bathe and Dvorkin

is combined with the above mentioned membrane families to form flat shell finite elements. The strain-displacement measures of these elements are modified on the element level to incorporate the effect of element warp.

Thirdly, the constitutive relationship of the flat shell elements is extended to include symmetric orthotropy. In opposition to the general trend to employ quadratic or even cubic elements for orthotropic analyses, it is shown that the simpler 4-node assumed stress families with drilling degrees of freedom presented herein are highly accurate and effective.

Finally, the influence of the stability parameter γ , the integration scheme order and the effect of the membrane locking correction are evaluated. The numerical value of the parameter γ is shown to be irrelevant in the patch test. The effect of the previously proposed membrane-bending locking correction when included in in-plane analysis is demonstrated.

The elements have been incorporated in the EDSAP/CALSAP finite element infrastructure.

Opsomming

- Titel:** Gevorderde Lae-Orde Ortotropiese Eindige Element Formulerings
- Outeur:** Susanna Elizabeth Geyer
- Graad:** M.Ing (Meganië)
- Departement:** Meganiëse Ingenieurswese
- Sudieleier:** Prof. Albert A. Groenwold
- Sleutelwoorde:** Boor-vryheidsgraad, Aangenome-spanning, Membraan, Plat dop, Eindige-element, Ortotropie

In hierdie studie word gevorderde lae-orde eindige-elemente vir die lineêre analise van ortotropiese dop-strukture ontwikkel. Die uiteindelijke doel van hierdie elemente is die globale optimering van ortotropiese dop-strukture. Lae-orde vierhoekige elemente is aantreklik in optimering, omdat dit lei tot lae koppeling in die styfheidsmatriks. Dit lei weer tot verminderde berekeningstyd. Vier-node vierhoekige elemente is egter berug vanweë hulle lae akkuraatheid.

Beide boor-vryheidsgrade ('drilling degrees of freedom') en aangenome-spanningsinterpolasies ('assumed stress interpolations') het die potensiaal om die modelleringseienskappe van lae-orde vierhoekige elemente te verbeter. Daarom is dit wenslik om lae-orde elemente te formuleer met beide 'n aangenome-spanningsinterpolasieveld en boor-vryheidsgrade, op voorwaarde dat die elemente se rang voldoende is en dat die elemente invariant is.

Eerstens word 'n variasionele basis vir die formulering van twee aangenome-spanning membraan eindige-element families met boor-vryheidsgrade aangebied. Dit is gebaseer op die formulering van Hughes en Brezzi en is afgelei deur gebruik te maak van die genormaliseerde formulering van Di en Ramm. Die spanningsmode klassifikasie van Feng *et al.* is gebruik vir die afleiding van die spanningsinterpolasie-matrikse. Die families, genoem $8\beta(M)$ en $8\beta(D)$, se rang is voldoende en is invariant. Hierdie families toon ook geen sluitingsgedrag nie. Die membraan-sluitingskorreksie wat voorgestel is deur Taylor verseker dat die nodale kragte in dié families ooreenstem met 'n vier-node vierhoekige membraan eindige-element wat twee verplasings-vryheidsgrade per node besit.

Tweedens word die reghoekige aangenome-vervorming plaat element van Bathe en Dvorkin gekombineer met bogenoemde membraan element families om plat dop eindige-elemente te vorm. Die vervorming-verplasing verwantskap van hierdie elemente word op die element vlak gemanipuleer om die effek van element uit-vlak distorsie te akkomodeer.

Derdens word die materiaalverwantskap van die plat dop elemente uitgebrei om simmetriese ortotropie in te sluit. In teenstelling met die algemene gebruik om kwadratiese of kubiese elemente vir ortotropiese analyses te gebruik, word die eenvoudiger vier-node aangenome-spanning families met boor-vryheidsgrade hier voorgestel. Hierdie elemente lewer baie goeie resultate en is effektief.

Laastens word die invloed van die stabiliteitsparameter γ , die integrasieskema-orde en die effek van die membraan-sluitingskorreksie geëvalueer. Daar word getoon dat die numeriese waarde van die parameter γ irrelevant is in die laptoets ('patch test'). Die effek van die voorheen voorgestelde membraan-sluitingskorreksie wanneer dit ingesluit word in in-vlak analyses word gedemonstreer.

Die elemente is geakkomodeer in die EDSAP/CALSAP eindige-element infrastruktuur.

Acknowledgments

I would like to express my sincere gratitude towards the following persons:

- Dr. Albert Groenwold, for his support throughout this study. It was an honor to work with him. His availability and willingness to assist made this work a pleasure. Sincere thanks to his wife for always being friendly.
- Prof E.E. Rosinger of the Department of Mathematics at the University of Pretoria, for the opportunity for discussions.
- Willy Calder, for the time and effort he put into this work, in his holidays, to ensure that the language is acceptable.
- Detlef Grygier and Justin Mann of KENTRON, for financial support, information on composite materials and the interest they took in this study.
- SASOL, for the opportunity to complete this study.
- My family, for their support, encouragement and prayers that helped me through this study.
- Jana van Graan, my cousin, and her mother, for knowing that the only way they would be able to see me was by offering a free meal.
- Gerrie van der Westhuizen, for understanding even if he did not understand what I was talking about.
- Last but not least, our study group and in particular Michael Hindley (our social organizer), for ‘Let’s go and play pool’ when the office got to small.

Contents

Abstract	ii
Opsomming	iv
Acknowledgments	vi
List of figures	xi
List of tables	xiii
1 Introduction	1
1.1 Motivation	1
1.2 Objectives	2
1.3 Approach	3
1.4 Thesis overview	3
2 Assumed stress membranes with drilling d.o.f.	4
2.1 Introduction	4
2.1.1 Summary of recent research	4
2.1.2 This study	6
2.2 A framework for independently interpolated rotation fields	6
2.2.1 Variational formulation	6
2.2.2 Finite element interpolations by Ibrahimbegovic <i>et al.</i>	13
2.2.3 On the numerical value of γ	14
2.3 Assumed stress membrane element with drilling degrees of freedom formulation	14
2.3.1 Variational formulation	14
2.3.2 Finite element interpolation	15
2.3.3 Developing and constraining the assumed stress field	18

2.4	Membrane locking correction	20
3	Numerical results: Isotropic membrane elements	23
3.1	Element rank	24
3.2	Membrane patch tests	25
3.2.1	Constant extension and constant shear patch tests	25
3.2.2	Modified shear patch test	25
3.3	Taylor's patch test and Ramm's cantilever beam	26
3.4	Cook's membrane	27
3.5	Thick walled cylinder	28
3.6	Cook's beam	29
3.7	Higher order patch test	30
4	Isotropic flat shell elements	43
4.1	Plate formulation	43
4.1.1	Mindlin plates: Bending theory and variational formulation	43
4.1.2	Finite element interpolation	48
4.1.3	Assumed strain interpolations	49
4.2	Shell formulation	51
4.2.1	Element formulation	51
4.2.2	A general warped configuration	52
5	Numerical results: Isotropic plates and shells	54
5.1	Plate patch tests	55
5.2	Cantilever under transverse tip loading	56
5.3	Thin simply supported plate under uniformly distributed load	56
5.4	Pinched hemispherical shell with 18° hole	56
5.5	Warped pinched hemisphere	57
5.6	Thick pinched cylinder with open ends	58
5.7	Thin pinched cylinder with open ends	58
5.8	Pinched cylinder with end membranes	59
5.9	Thick pre-twisted beam	59
5.10	Thin pre-twisted beam	60
5.11	Scordelis-Lo roof	60
5.12	Slender cantilever	60

6	Orthotropic flat shell elements	71
6.1	Constitutive relationship	71
6.2	Compliance matrix	73
7	Numerical results: Orthotropic problems	75
7.1	Plane stress membrane cantilever under transverse tip loading	75
7.1.1	Stacking sequence [0]	75
7.1.2	Stacking sequence [30]	76
7.1.3	Stacking sequence [0/90] _s	76
7.1.4	Stacking sequence [30/ − 30] _s	76
7.1.5	Stacking sequence [0/45/ − 45/90] _s	76
7.2	Clamped cylinder under internal pressure	77
7.2.1	Stacking sequence [90]	77
7.2.2	Stacking sequence [−45/45] _s	77
7.2.3	Stacking sequence [90/0] _s	77
7.2.4	Stacking sequence [0/90] _s	77
7.2.5	Stacking sequence [0]	78
7.3	Clamped hemisphere with 30° hole	78
7.3.1	Ply orientation $E_\theta = E_{11}$	78
7.3.2	Ply orientation $E_\phi = E_{11}$	78
7.4	Pre-twisted beam	80
7.4.1	Stacking sequence [0/90] _s	80
7.4.2	Stacking sequence [−45/45] _s	80
7.4.3	Stacking sequence [30/60] _s	80
8	Conclusions and recommendations	93
8.1	Isotropic membrane elements	93
8.2	Isotropic plate elements	94
8.3	Isotropic shell elements	94
8.4	Orthotropic formulation	94
8.5	Recommendations	95
	Bibliography	96
A	Element operators	101
A.1	Membrane element operators	101



A.2 Plate element operators	102
B Classification of stress modes	103
C Constraining the assumed stress field	104
D Reduced integration	105
D.1 Derivation of numerical integration schemes[1]	105
D.2 A 5-point integration scheme	106
D.3 An 8-point integration scheme	108
E Code	110
E.1 Subroutines for the isotropic 8β element	110
F List of definitions	129

List of Figures

2.1	Membrane finite element	16
3.1	Regular and distorted element geometries for eigenvalue analysis	24
3.2	Mesh used in patch tests	25
3.3	Constant extension patch test and constant shear patch test	26
3.4	Modified constant shear patch test	26
3.5	Taylor's patch test and Ramm's cantilever beam	27
3.6	Cook's membrane	28
3.7	Thick walled cylinder	29
3.8	Cook's beam	29
3.9	Higher order patch test	30
4.1	Four-node shell element	44
4.2	Mindlin theory	45
4.3	Interpolation functions for the transverse shear strains	50
4.4	Warped and projected quadrilateral shell element	53
5.1	Constant curvature patch test and constant shear patch test with zero rotations	55
5.2	Constant twist patch test	55
5.3	Cantilever under transverse tip loading	56
5.4	Thin simply supported plate under uniformly distributed load	57
5.5	Pinched hemisphere	58
5.6	Warped pinched hemisphere	59
5.7	Pinched cylinder with open ends	60
5.8	Pinched cylinder with end membranes	61
5.9	Pre-twisted beam	62
5.10	Scordelis-Lo roof	62
5.11	Slender cantilever	63



6.1	Laminate stacking convention	72
6.2	Local coordinate system for laminated structures	72
7.1	Cantilever under transverse tip loading and irregular mesh	75
7.2	Clamped cylinder under internal pressure	77
7.3	Clamped hemisphere with 30° hole	79
D.1	5-point integration scheme	107
D.2	8-point integration scheme	108

List of Tables

2.1	Unified formulation for the 5β , 8β and 9β families	20
3.1	Eigenvalues of square $8\beta(M)$ -NT and $9\beta(M)$ -NT elements	24
3.2	Taylor's patch test and Ramm's cantilever beam: Numerical results	31
3.2	Taylor's patch test and Ramm's cantilever beam: Numerical results (continued)	32
3.3	Cook's membrane: Center displacement u_{2C}	32
3.3	Cook's membrane: Center displacement u_{2C} (continued)	33
3.4	Cook's membrane: Stress analysis	33
3.4	Cook's membrane: Stress analysis (continued)	34
3.5	Cook's membrane: Influence of γ for the 2×2 mesh	35
3.6	Cook's membrane: Effect of integration scheme order	36
3.7	Thick-walled cylinder: Radial displacement	37
3.7	Thick-walled cylinder: Radial displacement (continued)	38
3.8	Cook's beam: Tip displacement u_{2A}	38
3.8	Cook's beam: Tip displacement u_{2A} (continued)	39
3.9	Cook's beam: Stress analysis	39
3.9	Cook's beam: Stress analysis (continued)	40
3.10	Higher order patch test: Numerical results	41
3.10	Higher order patch test: Numerical results (continued)	42
5.1	Cantilever under transverse tip loading: Tip displacement u_{3A}	62
5.2	Thin simply supported plate under uniformly distributed load: Hard supported	63
5.3	Thin simply supported plate under uniformly distributed load: Soft supported	63
5.4	Pinched Hemisphere with 18° Hole: Radial displacement u_{1A}	64
5.5	Pinched Hemisphere with 18° Hole: Influence of γ for the 2×2 mesh	64
5.6	Pinched Hemisphere with 18° Hole: Effect of integration scheme order	65

5.7	Warped pinched hemisphere: Radial displacement u_{1_A}	66
5.8	Thick pinched cylinder with open ends: Radial displacement $-u_{3_A}$	66
5.9	Thin pinched cylinder with open ends: Radial displacement $-u_{3_A}$	67
5.10	Pinched cylinder with end membranes: Radial displacement $-u_{3_A}$	67
5.11	Thick pre-twisted beam: Numerical results	68
5.12	Thin pre-twisted beam: Numerical results	69
5.13	Scordelis-Lo roof: Center displacement u_{3_A}	69
5.14	Slender cantilever: Numerical results	70
7.1	Plane stress membrane cantilever: Stacking sequence $[0]$	80
7.2	Plane stress membrane cantilever ($[0]$): Influence of γ on irregular mesh . . .	81
7.3	Plane stress membrane cantilever ($[0]$): Effect of integration scheme order . .	81
7.4	Plane stress membrane cantilever: Stacking sequence $[30]$	81
7.5	Plane stress membrane cantilever ($[30]$): Influence of γ on irregular mesh . .	82
7.6	Plane stress membrane cantilever ($[30]$): Effect of integration scheme order .	82
7.7	Plane stress membrane cantilever: Stacking sequence $[0/90]_s$	82
7.8	Plane stress membrane cantilever: Stacking sequence $[30/-30]_s$	83
7.9	Plane stress membrane cantilever: Stacking sequence $[0/45/-45/90]_s$	83
7.10	Clamped cylinder under internal pressure: Stacking sequence $[90]$	83
7.11	Clamped cylinder under internal pressure: Stacking sequence $[-45/45]_s$	84
7.12	Clamped cylinder under internal pressure: Stacking sequence $[90/0]_s$	84
7.13	Clamped cylinder under internal pressure: Stacking sequence $[0/90]_s$	85
7.14	Clamped cylinder under internal pressure: Stacking sequence $[0]$	85
7.15	Clamped hemisphere with 30° hole: Ply orientation $E_\theta = E_{11}$	86
7.16	Clamped hemisphere with 30° hole ($E_\theta = E_{11}$): Influence of γ on 4×4 mesh	87
7.17	Clamped hemisphere with 30° hole ($E_\theta = E_{11}$): Effect of integration scheme order	88
7.18	Clamped hemisphere with 30° hole: Ply orientation $E_\phi = E_{11}$	89
7.19	Clamped hemisphere with 30° hole ($E_\phi = E_{11}$): Influence of γ on 4×4 mesh	90
7.20	Clamped hemisphere with 30° hole ($E_\phi = E_{11}$): Effect of integration scheme order	91
7.21	Pre-twisted beam: Stacking sequence $[0/90]_s$	92
7.22	Pre-twisted beam: Stacking sequence $[-45/45]_s$	92
7.23	Pre-twisted beam: Stacking sequence $[30/60]_s$	92